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LAUNCH VEHICLE ERROR ANALYSIS
FOR APOLLO/SATURN 501 (U)

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Prepared by Bell Telephone Laboratories, Incorporated
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I. INTRODUCTION

This study evaluates and explains the effects of launch vehicle platform and performance errors on the Apollo/Saturn 501 unmanned test mission. AS501 is the first flight test of a Saturn V launch vehicle consisting of an S-IC first stage, an S-II second stage, and an S-IVB third stage.

The mission profile for AS501 is illustrated in Figure 9. The vehicle is launched along a 72 degree azimuth into a 100 nautical mile circular earth orbit. After two revolutions, the S-IVB is reignited for a non-optimum burn into a waiting orbit with a 9000 nautical mile apogee. A variable reignition criterion is employed which attempts to hold the total S-IVB consumed fuel constant by compensating for non-nominal S-IVB burn time during boost to earth parking orbit.

The SM is ignited twice on the waiting orbit. The first burn, which is approximately 27 seconds long, is performed shortly after waiting orbit injection. The second burn, which is approximately 265 seconds long, is performed before entry to increase the velocity to that of a lunar return. In this launch vehicle study, perfect updates and no platform or performance errors were considered for the SM burns.

The effects of launch vehicle platform and performance errors were determined by simulating perturbed trajectories for \pm three-sigma magnitudes of each independent error source. The following resulting three-sigma errors and fuel reserve deviations* at earth orbit injection (EOI) and waiting orbit injection (WOI) were obtained:

| | <u>EOI</u> | <u>WOI</u> |
|-----------------------------|------------|------------|
| Radius (ft) | 1314. | 5640. |
| Velocity magnitude (ft/sec) | 2.92 | 41.7 |
| Flight path angle (deg) | .0094 | .057 |
| Inclination (deg) | .0066 | .027 |
| Descending node (deg) | .0247 | .141 |
| Fuel reserve (lbs) | 5173. | 4350. |

The three-sigma actual deviations at entry are as follows:

| | <u>Without SM Burns</u> | <u>With Perfect SM Burns</u> |
|-----------------------------|-----------------------------|----------------------------------|
| Velocity magnitude (ft/sec) | 38.7 | .06 |
| Flight path angle (deg) | .119 | .0005 |
| Flight path azimuth (deg) | .220 | .080 |
| Latitude (deg) | .258 | .058 |
| Longitude (deg) | .468 | .185 |

* In this report, an error is defined as desired minus actual. An actual deviation is defined as actual minus actual nominal, and an uncertainty is defined as estimate minus actual.

The three sigma spacecraft ΔV penalty due to launch vehicle errors is 52.8 ft/sec.

As a result of this analysis, the following conclusions have been reached:

1. The errors at waiting orbit injection are almost entirely due to range angle uncertainty* at S-IVB reignition and gyro drift. The range angle uncertainty is due to the propagation of errors from earth orbit injection and uncertainty in venting thrust.
2. The sensitivities of velocity error at waiting orbit injection to range angle uncertainty and gyro drift are a function of the plane change and change in flight path angle made during this burn. Since both the plane and the flight path are changed appreciably, the sensitivities are large in comparison to those for a burn made along the velocity vector.
3. The perfect SM burns effectively reduce velocity and flight path angle deviations at entry. However, for the error sources considered in this study, the actual deviations at entry due to launch vehicle errors are small, even without the SM burns.

* The range angle is defined as the central angle to the instantaneous position measured in the plane of the orbit from the inertial position at launch. In the case of range angle uncertainty only, the shape and orientation of the orbit are known.

4. The variable ignition criterion for the S-IVB stage second burn effectively compensates for non-nominal performance during the boost to earth orbit. The three-sigma fuel deviation at waiting orbit injection is due to deviations in specific impulse, weight rate, and mixture ratio during the S-IVB second burn.

This study was performed by the Control Systems Analysis Department on behalf of Bellcomm, Inc.

II. Reference Trajectory Description

The nominal closed loop trajectory used for this study is a match of the Saturn V AS-501 Launch Vehicle Trajectory.¹ To develop this nominal trajectory, an open loop trajectory was first generated which matches significant parameters on the reference (cf. Table A).

The pitch profile of the open loop trajectory consists of a 12 second vertical rise followed by an instantaneous change in pitch (kick angle) to initiate a gravity turn. The gravity turn is flown until 144.846 seconds (from launch) at which time the attitude is fixed. At 183.846 seconds, the vehicle is given a second instantaneous pitch change followed by a constant pitch rate until S-IVB cutoff.

The kick angle at 12 seconds was selected to match the reference altitude at 183.846 seconds (288,983 ft). The pitch rate and S-IVB cutoff time were chosen to satisfy the radius (21,533,354 ft), velocity (25,567.705 ft/sec), and inertial flight path angle (0.0 deg) at S-IVB cutoff. In addition, the above scheme is nested in a procedure that finds a value for the thrust chamber area of the S-IC to match the time of S-IVB cutoff (687.542 seconds). The thrust chamber area A_T for the S-IC is used in the thrust formula found in Section IV.A, "Missile Dynamics", of this report. The value selected for A_T is 75844.533 in.²

The above constraints together with a launch azimuth of 72 degrees and no roll or yaw maneuvers, yield an orbital plane with an inclination of 32.557 degrees and an angle from the launch meridian to the descending node of 123.190 degrees.

The S-IVB remains in the parking orbit approximately three hours during which time the vehicle longitudinal axis is maintained along the velocity vector. Ullage and venting thrust with resulting mass losses are simulated in parking orbit. The ullage and venting thrust characteristics and time sequence were obtained from Reference 1.

The S-IVB is reignited when the vehicle's longitude matches the longitude in Reference 1 (81.4931 degrees west longitude). The time of reignition is at 11486.008 seconds compared with the reference value of 11486.034 seconds. Furthermore, the vehicle altitude and inertial velocity match the reference to within 700 ft and 3.6 ft/sec, respectively.

The S-IVB second burn uses a constant small pitch-rate attitude (measured in the launch plane from the x platform axis) with a constant yaw attitude (measured from the vehicle axis to the projection on the launch plane).

The four parameters of initial pitch angle, pitch rate, constant yaw angle, and the length of the second S-IVB burn, are selected to match the conditions of inertial velocity

(32067.974 ft/sec), inertial flight path angle (-9.1888 degrees), geodetic latitude (21.2845 degrees North), and longitude (156.7013 degrees east) at reentry (400,000 ft altitude) without SM burns. The selected parameters are 64.26 degrees for initial pitch angle, -.305 degrees/sec constant pitch rate, -20.60 degrees constant yaw angle, and 336.458 seconds burn time.

The resulting open loop reference trajectory was then processed to calculate all required guidance constants for the launch vehicle. The guidance constants of interest are listed below.

1. Parking Orbit Parameters

| | | |
|-----|--|------------------|
| (a) | Geocentric radius | 21,533,279.7 ft. |
| (b) | Inertial velocity | 25,567.77 ft/sec |
| (c) | Inertial flight path angle | 0.0 deg |
| (d) | Angle to descending node (from launch meridian) | 123.190 deg |
| (e) | Inclination | 32.55723 deg |

2. Waiting Orbit Parameters

| | | |
|-----|--|---|
| (a) | Energy | $-292,569,740. \text{ ft}^2/\text{sec}^2$ |
| (b) | Eccentricity | .57250593 |
| (c) | Angle between target vector and perigee vector | 0.0 deg |
| (d) | Angle to descending node (from launch meridian) | 135.490 deg |
| (e) | Inclination | 30.15168 deg |

The angle between the target vector and the perigee vector above corresponds to the angle specified in "AS-501/AFRM 017 Joint Launch Vehicle Targeting Requirements", September 1, 1965, (Reference 18).

A complete closed loop simulation of the launch vehicle was then performed, using the IGM equations planned for mission AS-501.⁴ The closed loop reference was generated in two modes starting at waiting orbit injection. The first is simply a match of the open loop reference without SM (Service Module) burns. The second incorporates two SM burns. The closed loop reference with SM burns uses the cross-product guidance law from Section 5.1 of Reference 14, including the revision of Reference 15. The values for eccentricity and semilatus rectum for these burns were obtained from Reference 17. The spacecraft burns are performed assuming a perfect update for each burn and no errors in the vehicle platform or in accelerometer measurements. The errors at reentry, therefore, using this reference, reflect errors that could not be eliminated by the spacecraft under ideal conditions. Table A summarizes the closed loop reference trajectory with and without SM burns.

TABLE A
Closed Loop Reference Trajectory

| Event | From Lift-off (Sec) | Weight (lbs) | Altitude (ft) | Geodetic Latitude (deg) | Longitude (deg) | Inertial Velocity (ft/sec) | Inertial Flight Path Angle (deg) | Inertial Azimuth (deg) |
|----------------------------------|------------------------|-----------------|------------------|-------------------------------|--------------------|----------------------------------|--|------------------------------|
| | | | | | | | | |
| Liftoff | 0.0 | 6,089,286 | 83.96 | 28.608 | -80.604 | 1,340.67 | 0.0 | 90.00 |
| S-IC Inboard Engine Cut-off | 144.846 | 1,890,087 | 181,765.22 | 28.804 | -79.911 | 8,326.17 | 20.923 | 75.469 |
| S-IC Outboard Engine Cut-off | 148.846 | 1,797,318 | 193,788.79 | 28.825 | -79.832 | 8,767.12 | 20.306 | 75.356 |
| S-II Engine Ignition | 152.156 | 1,410,795 | 203,722.93 | 28.844 | -79.764 | 8,731.00 | 19.736 | 75.336 |
| S-IC Interstage Jettison | 178.846 | 1,330,752 | 276,230.00 | 28.999 | -79.196 | 9,161.53 | 15.728 | 75.529 |
| LES Jettison | 183.846 | 1,309,194 | 288,474.43 | 29.029 | -79.084 | 9,254.67 | 15.035 | 75.558 |
| S-II Engine Cut-off | 511.526 | 459,835 | 611,442.87 | 31.627 | -66.219 | 22,067.25 | 0.930 | 81.255 |
| S-IVB Engine Ignition | 515.286 | 355,738 | 612,771.63 | 31.661 | -65.979 | 22,065.45 | 0.854 | 81.389 |
| S-IVB Engine Cut-off | 687.957 | 274,671 | 627,994.63 | 32.675 | -53.891 | 25,567.78 | 0.000 | 88.122 |
| <hr/> | | | | | | | | |
| EARTH PARKING ORBIT | | | | | | | | |
| Fixed Time 1 | 800.000 | 274,585 | 627,920.24 | 32.609 | -45.321 | 25,568.74 | 0.000 | 93.066 |
| Fixed Time 2 | 11,100.000 | 272,836 | 644,804.06 | 31.692 | -110.814 | 25,559.37 | 0.006 | 81.442 |
| Start S-IVB Preignition Sequence | 11,156.139 | 272,825 | 645,486.13 | 32.187 | -106.599 | 25,558.96 | 0.005 | 83.800 |
| <hr/> | | | | | | | | |
| SECOND S-IV BURN | | | | | | | | |
| S-IVB Engine Ignition | 11,486.113 | 271,954 | 646,512.41 | 31.855 | -81.515 | 25,562.78 | 0.016 | 97.987 |
| S-IVB Engine Cut-off | 11,814.134 | 128,492 | 1,893,306.88 | 27.445 | -57.052 | 30,695.23 | 15.411 | 103.439 |

TABLE A (cont'd)

| Event WAITING ORBIT WITHOUT SM BURNS | Time From Lift-off (Sec) | Weight (lbs) | Altitude (ft) | Geodetic Latitude (deg) | Longitude (deg) | Inertial Velocity (ft/sec.) | Inertial Path Angle (deg) | Inertial Azimuth (deg) |
|--|--------------------------------|-----------------|------------------|-------------------------------|--------------------|-----------------------------------|------------------------------|------------------------------|
| | | | | | | | | |
| Fixed Time 3 | 11,900.000 | 128,432 | 2,631,603.66 | 25.849 | -50.727 | 30,056.20 | 17.522 | 106.431 |
| Apogee | 20,145.297 | 51,759 | 54,742,382.0 | -28.431 | 39.155 | 8,720.74 | 0.000 | 100.614 |
| Reentry | 28,697.928 | 11,250 | 400,000.01 | 21.252 | 156.630 | 32,071.29 | -7.192 | 67.390 |
| WAITING ORBIT WITH SM BURNS | | | | | | | | |
| Fixed Time 3 | 11,900.000 | 128,432 | 2,631,603.66 | 25.849 | -50.727 | 30,056.20 | 17.522 | 106.431 |
| First SPS Engine Ignition | 12,514.134 | 51,735 | 9,302,875.38 | 12.775 | -20.185 | 25,280.16 | 27.960 | 117.677 |
| First SPS Engine Cut-off | 12,541.503 | 49,847 | 9,631,908.75 | 12.237 | -19.256 | 25,386.65 | 28.763 | 117.202 |
| Apogee | 20,921.553 | 49,847 | 60,083,785.5 | -28.663 | 37.384 | 8,395.00 | 0.000 | 79.908 |
| Second SPS Engine Ignition | 29,663.841 | 49,922 | 5,351,623.06 | 3.676 | 117.260 | 28,189.20 | -23.360 | 59.970 |
| Second SPS Engine Cut-off | 29,929.086 | 31,620 | 2,339,661.00 | 12.449 | 132.011 | 34,780.31 | -18.189 | 62.221 |
| Reentry | 30,176.269 | 11,250 | 400,000.16 | 21.891 | 152.155 | 36,334.06 | -7.05 | 68.560 |

III. Vehicle Data

Table B presents the vehicle data used to generate the closed loop reference trajectory. The weight used for each stage is illustrated in Table A and corresponds to the Saturn V AS-501 Launch Vehicle Reference Trajectory.¹

TABLE B

Engine Performance DataS-IC Engine Performance Data
(five engines burning)

| | |
|---------------------|---------------------------|
| Sea Level Thrust | 7,610,000 lbs |
| Weight Rate | 28,990.79 lbs/sec |
| Thrust Chamber Area | 75,844.53 in ² |
| Drag Area | 855.30 ft ² |

S-IC Engine Performance Data
(four engines burning)

| | |
|---------------------|----------------------------|
| Sea Level Thrust | 6,088,000 lbs |
| Weight Rate | 23,192.632 lbs/sec |
| Thrust Chamber Area | 60,675.624 in ² |

S-II Engine Performance Data5.0:1 Mixture Ratio

| | |
|---------------|--------------------|
| Vacuum Thrust | 1,000,000 lbs |
| Weight Rate | 2,358.4279 lbs/sec |

5.5:1 Mixture Ratio

| | |
|---------------|-------------------|
| Vacuum Thrust | 1,125,000 lbs |
| Weight Rate | 2,671.576 lbs/sec |

Table R - 2

4.7:1 Mixture Ratio

| | |
|---------------|-------------------|
| Vacuum Thrust | 925,000 lbs |
| Weight Rate | 2,172.766 lbs/sec |

S-IVB Engine Performance Data

5.0:1 Mixture Ratio

| | |
|---------------|----------------|
| Vacuum Thrust | 200,000 lbs |
| Weight Rate | 469.48 lbs/sec |

4.5:1 Mixture Ratio

| | |
|---------------|-----------------|
| Vacuum Thrust | 175,000 lbs |
| Weight Rate | 408.688 lbs/sec |

Spacecraft Engine Performance Data

| | |
|---------------|--------------|
| Vacuum Thrust | 21,460 lbs |
| Weight Rate | 69.0 lbs/sec |

IV. Simulation Description

The simulation required for the error analysis was performed using the Bellcomm Apollo Simulation Program (BCMASP). This program is a three degree of freedom simulator which generates the trajectory by numerical integration of all significant accelerations acting on the vehicle. Since BCMASP is described elsewhere in detail,¹⁰ only those aspects of the program that relate directly to the error analysis will be discussed in this report.

A functional diagram of the calculations performed in each guidance cycle by the simulation program is given in Figure 1. As illustrated in this diagram, the missile dynamics are simulated to obtain the actual position, velocity, and the integral of the nongravity acceleration. The accelerometer measurements are simulated by converting the integral of nongravity acceleration to platform coordinates and adding errors associated with the platform gyros and accelerometers. The accelerometer processing, navigation, and guidance equations are equivalent to those specified in the Launch Vehicle Digital Computer (LVDC) Equation Defining Document for AS-501.⁴ The pertinent details of these functions will now be discussed.

A. Missile Dynamics

In simulating the missile dynamics, the accelerations due to thrust, drag, and gravity were considered.

Thrust for the S-IC stage is computed by the following equation:

$$T = T_{sl} + A_T (14.696 - p)$$

where

T = thrust

T_{sl} = constant sea level thrust

A_T = thrust chamber area

p = atmospheric pressure (lbs/sq. in)

All other burns are assumed to have constant thrusts. Also, constant weight rates were assigned to all burns.

The S-IC burns at full thrust until either fuel remaining reaches 28445 lbs or oxidizer remaining reaches 64324 lbs, at which time the center engine is shut down, resulting in a 20% decrease in weight rate, T_{sl} , and A_T . Upon total depletion of either fuel or oxidizer, the remaining engines are shut down and a 3.31 second coast is initiated. The S-II is then ignited at a mixture ratio 5.0:1 and held there for 3.613 seconds at which time the propellant utilization (PU) system is released and the mixture ratio is stepped to 5.5:1. When the ratio of LOX to hydrogen reaches 4.7:1, the mixture ratio is stepped to 4.7:1 and held there until

shutdown is forced by depletion of either LOX or hydrogen. On the nominal, these occur simultaneously. Following a fixed time coast of 3.76 sec, the S-IVB is ignited at a mixture ratio of 5.0:1, which is held until parking orbit conditions have been attained. The S-IVB second burn is initiated at a mixture ratio of 4.5:1, which is changed to 5.0:1 by the PU system when the ratio of LOX to hydrogen reaches 5.0:1, and is then held constant until shutdown is executed.

Venting is simulated by applying a small thrust along the instantaneous velocity vector throughout parking orbit. The magnitude of this thrust is a function of time as tabulated in the Boeing reference trajectory.¹

Drag force was computed using the drag coefficient curve given in Reference 1 and the Patrick Reference Atmosphere.⁹ The gravitational force is computed from the standard Fisher Ellipsoid model of the Earth as defined in Reference 16.

The attitude of the vehicle is determined by integrating constant attitude rates. These rates are recomputed each guidance cycle and ordered to accomplish the required change in attitude as determined by the guidance equations. Although angular dynamics and autopilot response are not simulated, rate limiting of 1 deg/sec is applied.

Uncertainties in specific impulse, weight rate, mixture ratio, fuel loading, and inert weight were considered for each stage. Deviations in these quantities are expressed as fractions of nominal and are implemented in the following way:

$$\begin{aligned} w_p &= w_{\text{nom}}(1+E_w) \\ F_p &= F_{\text{nom}}(1+E_F) \\ \dot{w}_p &= \dot{w}_{\text{nom}}(1+E_{\dot{w}}) + bM_{\text{nom}}E_m \\ T_p &= (T_{\text{nom}}(1+E_{\text{ISP}}) - cM_{\text{nom}}E_m)(1+E_{\dot{w}}) \\ \text{ISP}_p &= T_p / \dot{w}_p \end{aligned}$$

where

- w = inert weight
- \dot{w} = weight rate
- F = fuel loaded
- M = mixture ratio
- T = thrust
- ISP = specific impulse
- E_x = deviation associated with x
- nom = subscript denoting nominal value
- p = subscript denoting perturbed value

$$\left. \begin{array}{l} b = \frac{\partial \dot{W}}{\partial M} \\ c = \frac{\partial T}{\partial M} \end{array} \right|_{M = M_{nom}} \quad \left. \begin{array}{l} \text{from engine performance} \\ \text{curves} \end{array} \right\}$$

In addition, the effects of perturbations in weight rate, mixture ratio, and fuel loading are reflected in the times of S-IC inboard engine cutoff and outboard engine cutoff, S-II second mixture ratio shift and cutoff, and the S-IVB mixture ratio shift. An error in fuel loading is assumed to be distributed in the same proportion as oxidizer and fuel are nominally loaded. Errors in mixture ratio are carried through an entire stage, causing the same percent error at all mixture ratio levels. During those burns for which the PU system is active and not in saturation, errors in mixture ratio are assumed to be zero.

Errors in drag coefficient, atmospheric density, ullage and venting thrust are also expressed as fractions of the nominal value. Perturbations of ullage and venting thrust are assumed to be caused by proportional variations in weight rate.

Cutoff execution uncertainties are simulated for both S-IVB shutdowns. These uncertainties are represented by an equivalent time increment at full thrust.

B. Inertial Platform Simulation

The accelerometer measurements are simulated by integrating the actual sensed acceleration due to thrust and aerodynamic forces, and adding errors associated with the platform gyros and accelerometers. The error sources considered include the following:

- (1) initial platform misalignment
- (2) gyro drift
- (3) gyro mass unbalance
- (4) gyro anisoelastic effects
- (5) accelerometer misalignment
- (6) accelerometer bias
- (7) accelerometer scale factor error

The inertial platform alignment and the orientation of the gyro axes are illustrated in Figure 2. As shown in Figure 3, the operations performed to simulate this platform proceed by first forming the increment in velocity gained during the last guidance cycle due to thrust and aerodynamic forces. This velocity increment ($\Delta\bar{V}_a$) is expressed in the platform coordinate system which is defined by the nominal platform alignment at guidance reference release.

The effects of initial misalignment and platform drift are simulated by the A matrix. This matrix relates

the actual instantaneous platform orientation to the nominal alignment. The initial misalignment is described by three Euler angles taken about the pitch, yaw, and roll axes. The drift rate about each platform axis is given by

$$\omega_j = GD_j + U_{sj}a_{1j} + U_{1j}a_{sj} + U_{oj}a_{oj} + S_ja_{1j}a_{sj}$$

where

GD_j = the fixed gyro drift rate of the j^{th} axis gyro

U_{sj}, U_{1j}, U_{oj} = the mass unbalance about the spin, input, and output axes of the j^{th} axis gyro

S_j = the anisoelastic constant of the j^{th} axis gyro, and

a_{1j}, a_{sj}, a_{oj} = the sensed acceleration along the input, spin, and output axes of the j^{th} axis gyro.

The total drift rate is calculated and used to update the A matrix each computation cycle.

With reference to Figure 3, the B matrix simulates accelerometer misalignment. Since this matrix is not time dependent, it need only be calculated once and is given by

$$[B] = \begin{bmatrix} \cos \epsilon_{yx} \cos \epsilon_{xz} & -\sin \epsilon_{xy} \cos \epsilon_{yz} & \sin \epsilon_{xz} \cos \epsilon_{xy} \\ \sin \epsilon_{yx} \cos \epsilon_{yz} & \cos \epsilon_{yx} \cos \epsilon_{yz} & -\sin \epsilon_{yz} \cos \epsilon_{yx} \\ -\sin \epsilon_{zx} \cos \epsilon_{zy} & \sin \epsilon_{zy} \cos \epsilon_{zx} & \cos \epsilon_{zx} \cos \epsilon_{zy} \end{bmatrix}$$

where the ϵ 's are the angles by which the accelerometer axes deviate from the platform axes as illustrated in Figure 4. Accelerometer bias and scale factor error are introduced by the vector \bar{a}_b and the matrix $[1 + SF]$ respectively. The scale factor matrix is of the form

$$\begin{bmatrix} (1 + SF_x) & 0 & 0 \\ 0 & (1 + SF_y) & 0 \\ 0 & 0 & (1 + SF_z) \end{bmatrix}$$

where SF_i represents the scale factor error of the accelerometer along the i^{th} axis.

ΔV_m , the output of the platform simulation, now represents the change in the accelerometer measurements that has occurred during the last computation cycle. This quantity is used by the navigation equations, the M/F filter⁸, and the mixture ratio shift sensor.

C. Navigation Equations

The onboard navigation equations consists of two sections: boost navigation and orbital navigation. The boost navigation (as specified in the LVDC Equation Defining Document⁴) is simulated during powered flight and during ullage burns. At ullage cutoff, after parking orbit insertion, the boost navigation state vector is used as the initial state for the orbital navigation equation.

The orbital navigation scheme uses a venting model where the thrust acceleration is the nominal value (derived from nominal values for venting thrust, weight rate, and weight-into-orbit). The direction of the thrust acceleration for this model is maintained along the navigation velocity vector and the equations of motion are integrated with the fourth order Runge-Kutta scheme in BCMASP.¹¹ The direction of the thrust acceleration for the actual vehicle is derived from this model knowing the orientation of the actual platform with respect to the inertial navigation coordinates. In addition to platform errors, deviations in weight-into-orbit and venting thrust (assumed to be a deviation in weight rate) will, in this model, cause uncertainties in the vehicle state vector.

When ullage thrust is again applied, prior to the S-IVB reignition, the orbital navigation state vector is used as the initial state for the boost navigation equations which are used until S-IVB waiting orbit insertion. The boost navigation state vector is then integrated (using fourth order Runge-Kutta and no thrust acceleration) until 86 seconds from nominal S-IVB cutoff. The two spacecraft burns are both simulated assuming a perfect navigation model.

D. Guidance Equations

Steering commands are generated in the following manner: from tower clearance to S-IC center engine cutoff, a fourth degree polynomial provides pitch commands as a function of time. The polynomial is a least-squares fit to the zero lift open loop trajectory. The attitude of the vehicle is then held constant until the launch escape system has been jettisoned. From this point until earth orbit insertion, pitch and yaw steering orders are generated by the 3-stage Iterative Guidance Mode (IGM).

The out-of-orbit burn is also guided by IGM (2-stage). This burn is intentionally non-optimum in order to deplete the S-IVB fuel supply. A variable reignition criterion corrects for dispersions in the first S-IVB burn time. The following formula redefines α_{TS} , the angle between the target vector and the intersection of the parking orbit and waiting orbit planes:

$$\alpha_{TS} = \alpha_N + K_1 \Delta t_4 + K_2 \Delta t_4^2$$

where

$$\alpha_N = 147.56356 \text{ deg}$$

$$K_1 = .56338027 \times 10^{-2} \text{ deg/sec}$$

$$K_2 = .20939407 \times 10^{-3} \text{ deg/sec}^2$$

Δt_4 = actual S-IVB burn time for
earth orbit injection minus
nominal burn time.

Adjusting α_{TS} causes a slight reorientation of the waiting orbit plane, and hence, the use of more or less fuel as desired.

Cross-product steering is employed during both spacecraft burns. The guidance objectives are to control the eccentricity and semilatus rectum of the orbit, and to maintain the vehicle in the present waiting orbit plane.

V. Results

The effects of platform errors¹⁹ and performance errors² were determined by simulating perturbed trajectories for \pm three-sigma magnitudes of each error source. The resulting variations in significant parameters at earth orbit injection, S-IVB reignition, waiting orbit injection, entry, and three fixed times are listed in Appendix C. The variations at entry are examined both with and without (perfect) SM burns. The fixed times occur after earth orbit injection (800 sec), before S-IVB reignition (11,100 sec), and after waiting orbit injection (11,900 sec). The coordinate systems and symbols used in Appendix C are defined in Appendices A and B respectively.

In addition to listing variations due to individual sources, Appendix C contains covariance matrices of these variations due to all platform and performance errors considered. These matrices list the standard deviations (one-sigma) down the main diagonal, correlation coefficients above the diagonal, and covariances below the diagonal.

The remainder of this section describes the significant results in two parts: guidance and navigation error analysis, and performance analysis.

A. Guidance and Navigation Error Analysis

The significant guidance and navigation errors at earth orbit injection, waiting orbit injection, and entry are discussed.

1. Earth Orbit Injection

The three-sigma actual deviations at earth orbit injection are as follows:

| | |
|--------------------|-------------|
| Radius | 1314. ft |
| Velocity magnitude | 2.92 ft/sec |
| Flight path angle | .0094 deg |
| Inclination | .0066 deg |
| Descending node | .0247 deg |

Since the guidance and navigation system can sense and correct for non-nominal performance, the above deviations are caused almost entirely by uncertainties due to platform anomalies and cutoff execution error.

Table 1 in Appendix C lists the actual deviations at earth orbit injection due to the individual platform errors. The results in this table indicate that the platform errors fall into three categories: those that cause in-plane deviations (radius, velocity, and flight path angle); those that cause out-of-plane deviations (inclination and node); and those that cause no significant deviations. This behavior is explained by the orientation of the platform relative to the trajectory.

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As illustrated in Figure 2, the flight to earth orbit lies nearly in the xy platform plane. The x component of thrust acceleration is dominant, and the z component is near zero. Although the y component of thrust acceleration is significant, it experiences a sign change such that the integrated effect is small. Thus, rotations about the x axis cause no significant deviations. Rotations about the y axis cause out-of-plane deviations, and rotations about the z axis cause in-plane deviations.

Platform rotations about the y and z axes are caused by initial platform misalignment (CHI_{1Y} and CHI_{1Z}) and platform drift. With reference to Section IV.B and Figure 2, the drift rates about these axes are given by the following:

$$\omega_y = GDSVY + (\ddot{z})UISVY + (\ddot{y})USSVY + (\ddot{x})UOSVY + (\ddot{y})(\ddot{z})SSVY$$

$$\omega_z = GDSVZ + (\ddot{x})UISVZ + (\ddot{z})USSVZ + (\ddot{y})UOSVZ + (\ddot{z})(\ddot{x})SSVZ$$

where

GDSVY and GDSVZ are the constant drift terms;

UISVY and UISVZ represent mass unbalance about the input axes;

USSVY and USSVZ represent mass unbalance about the spin axes;

UOSVY and UOSVZ represent mass unbalance about the output axis;

SSVY and SSVZ represent anisoelastic constants; and \ddot{x} , \ddot{y} , and \ddot{z} are the thrust acceleration components. Since \ddot{z} is near zero, only GDSVY, USSVY, and UOSVY contribute significantly to drift about the y axis. Similarly, only GDSVZ, UISVZ, and UOSVZ contribute significantly to drift about the z axis.

Similar arguments can be made for the accelerometer errors. Bias and scale factor error in the x and y accelerometers contribute to in-plane deviations. Although bias in the z accelerometer contributes to the out-of-plane deviations, z scale factor error does not contribute significantly because of the small acceleration in this direction. If the x and y accelerometers are misaligned in the xy plane, in-plane deviations result. If the z accelerometer is misaligned, it senses accelerations in the xy plane resulting in out-of-plane deviations.

2. Waiting Orbit Injection

The three-sigma errors at waiting orbit injection are as follows:

| | |
|--------------------|-------------|
| Radius | 5640. ft |
| Velocity magnitude | 41.7 ft/sec |
| Flight path angle | .057 deg |
| Inclination | .027 deg |
| Node angle | .141 deg |

The above errors are differences between the desired values as computed by the guidance equations and the actual values (see Table 39), and should not be confused with actual deviations (Table 40). The desired values can change due to a change in the injection point on the ellipse or because the ellipse itself has changed due to the variable ignition criterion.

Errors at waiting orbit insertion are due to uncertainties at S-IVB reignition, platform errors that affect the sensed acceleration during the burn, and cutoff execution errors. Since non-nominal performance during the burn can be sensed, it does not appreciably affect guidance accuracy.

Although uncertainties in the shape and orientation of the orbit at S-IVB reignition are small, a significant range angle uncertainty exists. The range angle uncertainty is due to deviations in the orbital period that are not sensed by the on-board navigation system. The deviations in period are caused by deviations in energy at earth orbit injection due to platform errors and uncertainties in venting thrust. As described in Section IV.C, the actual venting thrust is not sensed by the navigation system.

To illustrate the propagation of errors from earth orbit injection, consider the energy relationship.

$$E = V^2/2 - \mu/R$$

Differentiating and using the relationship that V on a circular orbit is equal to $\sqrt{\mu/R}$, we obtain

$$\frac{\delta E}{E} = -2 \left[\frac{\delta V}{V} + \frac{\delta R}{R} \right] \quad (1)$$

This change in energy in turn affects the orbital period. The period is given by

$$\tau = 2\pi \sqrt{a^3/\mu}$$

where a is the semi major axis given by

$$a = -\mu/2E$$

Thus,

$$\frac{\delta \tau}{\tau} = -\frac{3}{2} \frac{\delta E}{E} \quad (2)$$

When the change in period is not sensed by the navigation system, it causes a range angle uncertainty at S-IVB reignition. The range angle ϕ_T (PHIT) is the central angle measured in the plane of the orbit from the inertial position at launch. At S-IVB reignition, the range angle is approximately given by

$$\Phi_T = \Phi_{T0} + 2\pi T/\tau \quad (3)$$

where Φ_{T0} is the range angle at earth orbit injection and T is the flight time from earth orbit injection to S-IVB reignition.

The deviation in Φ_T at S-IVB reignition is given by

$$\delta\Phi_T = \delta\Phi_{T0} - \left(\frac{2\pi T}{\tau}\right)\frac{\delta\tau}{\tau} + \left(\frac{2\pi}{\tau}\right)\delta T$$

If we consider only deviations that are not sensed, δT is equal to zero. Also, since $\delta\Phi_{T0}$ is near zero for these error sources (PHIT column in Table 1), the Φ_T deviation is approximated by the following.

$$\delta\Phi_T = -\left(\frac{2\pi T}{\tau}\right)\frac{\delta\tau}{\tau} \quad (4)$$

From Eqs. 1 through 4, we obtain

$$\delta\Phi_T = -3(\Phi_T - \Phi_{T0}) \left[\frac{\delta V}{V} + \frac{\delta R}{R} \right] \quad (5)$$

where Φ_T is evaluated at S-IVB reignition on the nominal trajectory. For AS501,

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$$\Phi_T - \Phi_{TO} = 735 \text{ deg}$$

$$V = 25,567 \text{ ft/sec}$$

and

$$R = 21,533,280 \text{ ft.}$$

Table C illustrates Eq. (5) by listing Φ_T deviations ($\delta\hat{\Phi}_T$) at S-IVB reignition computed from radius and velocity deviations at earth orbit injection. The ΔV used to compute $\delta\hat{\Phi}_T$ for non-nominal venting thrust is the average velocity change attributed to this source. As illustrated, the computed values agree closely with the actual deviations ($\delta\Phi_T$) listed from Table 22.

Since the platform has been released for over 3.3 hours, the platform errors that affect the sensed acceleration during the waiting orbit injection burn are dominated by the constant gyro drift terms.

The simple model shown in Figure 8 was developed to explain the affects of gyro drift and range angle uncertainty on the velocity errors at waiting orbit injection. In this model, the burn is represented by an instantaneous ΔV applied up from the local horizontal by an angle α , and out of the initial plane by an angle γ . V_0 , V , and β represent the

Table C
 Φ_T Errors at S-IVB Reignition

| <u>Error Source</u> | <u>δR^* (ft)</u> | <u>δV (ft/sec)</u> | <u>$\delta \hat{\Phi}_T$ (deg)</u> | <u>$\delta \Phi_T$ (deg)</u> |
|---------------------|---|---|---|---|
| CH11Z | 224. | -.60 | .029 | .027 |
| GDSVZ | 667. | -1.49 | .060 | .056 |
| UISVZ | 786. | -1.69 | .065 | .061 |
| UOSVZ | 525. | -1.17 | .047 | .044 |
| SFSVX | -117. | -.59 | .063 | .061 |
| SFSVY | -189. | .14 | .007 | .007 |
| ABSVX | -101. | -.53 | .056 | .058 |
| ABSVY | -233. | .30 | -.002 | -.003 |
| EPSVXY | 176. | .44 | -.056 | -.055 |
| EPSVYX | -440. | .54 | -.002 | .000 |
| EVENTR | 0. | 1. | <u>-.086</u> | <u>-.094</u> |
| RSS | | | .169 | .169 |

* δR and δV are from Table 1 in Appendix C. $\delta \hat{\Phi}_T$ is computed from Eq. (5), and $\delta \Phi_T$ is from Table 22.

initial velocity, the final velocity, and the final flight path angle respectively. The initial flight path angle is assumed to be zero.

Using this model, the final velocity magnitude is given by

$$V = \left\{ (V_0 + \Delta V \cos \gamma \cos \alpha)^2 + (\Delta V \cos \gamma \sin \alpha)^2 + (\Delta V \sin \gamma)^2 \right\}^{1/2}$$

The deviation in velocity magnitude due to deviations in V_0 , α , and γ which are not sensed by the navigation system is given by

$$\begin{aligned} \delta V &= \left\{ \frac{-V_0 \Delta V \cos \gamma \sin \alpha}{V} \right\} \delta \alpha \\ &+ \left\{ \frac{-V_0 \Delta V \sin \gamma \cos \alpha}{V} \right\} \delta \gamma \\ &+ \left\{ \frac{V_0 + \Delta V \cos \gamma \cos \alpha}{V} \right\} \delta V_0 \end{aligned} \quad (6)$$

For AS501, the following values approximate the waiting orbit injection burn:

$$V_0 = 25562 \text{ ft/sec}$$

$$\Delta V = 9095 \text{ ft/sec}$$

$$\alpha = 60.4 \text{ deg}$$

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$$\gamma = 25 \text{ deg}$$

$$\beta = 15.4 \text{ deg}$$

$$V = 30695 \text{ ft/sec}$$

Substituting these values into Eq. (6) we obtain

$$\delta V \approx -108\delta\alpha - 24.8\delta\gamma + \delta V_0 \quad (7)$$

where the velocity and angle deviations are expressed in feet/second and degrees respectively.

Note from Eq. (6) that the sensitivities of δV to errors in the direction of ΔV depend strongly upon the nominal orientation. If the ΔV could be applied along the initial velocity vector, the sensitivities would be greatly reduced. For AS501, α is large to obtain the desired velocity and flight path angle at entry. The large γ is required to perform the plane change.

Deviations in φ_T that are not sensed by the navigation system result in an error in α . In this case,

$$\delta\alpha = \delta\varphi_T. \quad (8)$$

Gyro drift can be related to deviations in α and γ by noting the platform orientation relative to the nominal ΔV vector.

Since φ_T is approximately 60 degrees at waiting orbit injection

(note that α is also 60 degrees), the ΔV is applied almost directly along the x axis. The z axis is normal to the plane, and the y axis completes the right handed set as illustrated in Figure 8. Thus, y and z gyro drift cause deviations in γ and α respectively. A drift about the x axis rotates the out-of-plane ΔV component ($\Delta V \sin \gamma$) toward the initial plane resulting in a change in α given by

$$\delta\alpha = \frac{(\Delta V \sin \gamma)(GDSVX)T}{\Delta V \cos \gamma}$$

or

$$\delta\alpha = (\tan \gamma)(GDSVX)T \quad (9)$$

where GDSVX is the x gyro drift (.1 deg/hr) and T is the time from launch to waiting orbit injection (3.3 hr). Since the total rotation is small, $\delta\gamma$ can be assumed zero.

Table D illustrates the effectiveness of Eq. (7) in explaining the velocity errors at waiting orbit injection. In the case of x gyro drift, the velocity deviation was derived by assuming that Eq. (9) describes the only contribution to Eq. (7). Similarly, the y gyro drift was derived assuming that the only contribution to Eq. (7) is given by

$$\delta\gamma = (GDSVY)T$$

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Table DVelocity Errors at Waiting Orbit Injection

| Error Source | $\hat{\delta}V^*$ | δV |
|--------------|-------------------|------------|
| GDSVX | -16.6 | -15.2 |
| GDSVY | -6.1 | -6.7 |
| GDSVZ | -34.2 | -33.3 |
| UISVZ | -8.3 | -10.4 |
| UOSVZ | -5.9 | -6.5 |
| SFSVX | -6.6 | -6.9 |
| ABSVX | -6.8 | -6.7 |
| ABSVY | .6 | 1.2 |
| CH11Z | -3.5 | -3.6 |
| EPSWXY | 6.4 | 5.9 |
| EVENTR | 10.2 | 8.3 |
| RSS | 42.8 | 41.8 |

* $\hat{\delta}V$ is computed from Eq. (7), and δV is obtained from simulations as given in Table 31.

where GDSVY is the y gyro drift (.075 deg/hr). In the case of z gyro drift, Eq. (7) was evaluated as

$$\delta V = -108[(GDSVZ)(T) + \delta\varphi_T] + \delta V_0$$

where $\delta\varphi_T$ was computed from Eq. (5), and δV_0 is the deviation at S-IVB reignition due to the z gyro drift ($GDSVZ = .075$ deg/hr) as given in Table 22. Since earth orbit injection and S-IVB reignition occur at almost the same point on the orbit, δV_0 is nearly equal to the velocity deviation at earth orbit injection.

In the case of all other error sources, the velocity deviations were computed from the following:

$$\delta V = -108\delta\varphi_T + \delta V_0$$

In these cases, the velocity deviation is almost entirely due to the propagation of errors from earth orbit injection. It should also be noted that δV_0 is usually small as compared to the $\delta\varphi_T$ contribution.

It is concluded that the errors at waiting orbit injection are due to range angle uncertainty at S-IVB reignition and gyro drift. The range angle uncertainty is due to

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venting model uncertainties and platform errors which contribute to in-plane errors at earth orbit injection. Other sources, including cutoff execution errors, contribute negligible errors to this burn.

3. Entry

The three-sigma actual deviations at entry due to the launch vehicle platform and performance errors considered in this study are given as follows:

| | <u>Without SM Burns</u> | <u>With Perfect SM Burns</u> |
|-----------------------------|-----------------------------|----------------------------------|
| Velocity magnitude (ft/sec) | 38.7 | .06 |
| Flight path angle (deg) | .119 | .0005 |
| Flight path azimuth (deg) | .220 | .080 |
| Latitude (deg) | .258 | .058 |
| Longitude (deg) | .468 | .185 |

The first spacecraft burn has a three-sigma ΔV penalty (DELV1) of 52.8 ft/sec. Since, in this analysis, the first burn corrects the in-plane velocity error, the ΔV penalty for the second SM burn (DELV2) is not significant.

The velocity and flight path angle deviations at entry are effectively reduced by the perfect spacecraft burns. Other deviations are not completely removed since the SM burns do not correct position deviations or out-of-plane velocity errors at waiting orbit injection. However, even without SM burns, the deviations at entry are small.

B. Performance Analysis

Performance uncertainties determine the fuel reserve requirements for the S-IVB. Tables 4 and 36 list fuel deviations at first and second S-IVB cutoff caused by performance perturbations. As shown by Table 36, the variable ignition criterion for the S-IVB stage second burn effectively compensates for non-nominal performance in the first two stages, and the only significant contributors to fuel deviations are those error sources affecting the S-IVB stage. The total three-sigma fuel uncertainty of 4350 lbs is due primarily to deviations in specific impulse, weight rate, inert weight, and mixture ratio in the S-IVB stage.

Figures 5 through 7 are plots of fuel penalties caused by perturbations of engine mixture ratios. The discontinuous slope exhibited in Figure 5 is due to the fact that an off nominal mixture ratio in the first stage causes early depletion of either fuel or oxidizer. The S-II and S-IVB stages do not demonstrate this characteristic since the PU system is assumed to guarantee simultaneous depletion of fuel and oxidizer. The slopes on these curves are due to the variation of specific impulse with mixture ratio.

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APPENDIX A

COORDINATE SYSTEMS

Platform Coordinates

The platform coordinate system is a geocentric inertial system defined as follows: The y axis is upward along the local vertical at launch. The x axis is orthogonal to the y axis and points down-range in the launch plane. The z axis completes the right-handed orthogonal system.

Local Vertical Coordinates

The local vertical coordinate system is a geocentric inertial system defined relative to the state vector at a specific time. The "cross-range" axis is directed opposite to the angular momentum vector; the "up" axis is defined as upward along the position vector; and the "down-range" axis is parallel to the projection of the velocity vector into a plane perpendicular to the "up" axis.

APPENDIX B

DEFINITION OF SYMBOLS

Trajectory Parameters

| <u>Symbol</u> | <u>Units</u> | <u>Definition</u> |
|---------------|--------------|--|
| R | ft | position magnitude |
| V | ft/sec | velocity magnitude |
| BETA | deg | inertial flight path angle |
| INCL | deg | orbit inclination |
| NODE | deg | angle from launch meridian to descending node |
| PHT | deg | central angle from inertial launch site |
| FUEL | lbs-m | S-IVB fuel reserve |
| RPX | ft | position in platform coordinates |
| RPY | ft | |
| RPZ | ft | |
| VPX | ft/sec | velocity in platform coordinates |
| VPY | ft/sec | |
| VPZ | ft/sec | |
| TIME | sec | time measured from midnight of launch date |
| ERNX | ft | position uncertainties, navigation minus actual, in platform coordinates |
| ERNY | ft | |
| ERNZ | ft | |
| EVNX | ft/sec | velocity uncertainties, navigation minus actual, in platform coordinates |
| EVNY | ft/sec | |
| EVNZ | ft/sec | |

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| <u>Symbol</u> | <u>Units</u> | <u>Definition</u> |
|---------------|--------------|--|
| ERCR | ft | |
| ERDR | ft | |
| ERUP | ft | |
| EVCR | ft/sec | |
| EVDR | ft/sec | |
| EVUP | ft/sec | |
| ERNCR | ft | |
| ERNDR | ft | |
| ERNUP | ft | |
| EVNCR | ft/sec | |
| EVNDR | ft/sec | |
| EVNUP | ft/sec | |
| ER | ft | |
| EV | ft/sec | |
| EBETA | deg | |
| EINCL | deg | |
| ENODE | deg | |
| LAT | deg | geodetic latitude |
| LON | deg | longitude |
| ALFA | deg | inertial flight path azimuth |
| CRMN | naut miles | cross range ground distance to landing site at reentry |
| DRNM | naut miles | down range ground distance to landing site at reentry |
| DELV1 | ft/sec | delta-V at first SM burn |
| DELV2 | ft/sec | delta-V at second SM burn |

Appendix B - 3

Platform Perturbations

| <u>Symbol</u> | <u>Units</u> | <u>Definition</u> |
|---------------|-----------------------|---|
| GDSVX | deg/hr | |
| GDSVY | deg/hr | |
| GDSVZ | deg/hr | |
| USSVX | deg/hr/g | |
| USSVY | deg/hr/g | |
| USSVZ | deg/hr/g | |
| UISVX | deg/hr/g | |
| UISVY | deg/hr/g | |
| UISVZ | deg/hr/g | |
| UOSVX | deg/hr/g | |
| UOSVY | deg/hr/g | |
| UOSVZ | deg/hr/g | |
| SSVX | deg/hr/g ² | |
| SSVY | deg/hr/g ² | |
| SSVZ | deg/hr/g ² | |
| SFSVX | - | |
| SFSVY | - | |
| SFSVZ | - | accelerometer scale factors |
| ABSVX | g | |
| ABSVY | g | |
| ABSVZ | g | accelerometer bias |
| CHI1X | deg | |
| CHI1Y | deg | |
| CHI1Z | deg | initial platform misalignment |
| EPSVXY | deg | |
| EPSVXZ | deg | |
| EPSVYX | deg | |
| EPSVYZ | deg | |
| EPSVZX | deg | |
| EPSVZY | deg | accelerometer misalignment coefficients |

Performance Perturbations

| <u>Symbol</u> | <u>Units</u> | <u>Definition</u> |
|---------------|--------------|--|
| EISPl | % | uncertainty in specific impulse, S-IC |
| EDWGT1 | % | uncertainty in weight rate, S-IC |
| EM1 | % | uncertainty in mixture ratio, S-IC |
| EFUELL | % | uncertainty in fuel loading, S-IC |
| EWGT1 | % | uncertainty in inert weight, S-IC |
| ECD | % | uncertainty in axial force coefficient |
| ERHOA | % | uncertainty in atmospheric density |
| EISP2 | % | uncertainty in specific impulse, S-II |
| EDWGT2 | % | uncertainty in weight rate, S-II |
| EM2 | % | uncertainty in mixture ratio, S-II |
| EFUEL2 | % | uncertainty in fuel loading, S-II |
| EWGT2 | % | uncertainty in inert weight, S-II |
| EISP3 | % | uncertainty in specific impulse, S-IVB |
| EDWGT3 | % | uncertainty in weight rate, S-IVB |

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| <u>Symbol</u> | <u>Units</u> | <u>Definition</u> |
|---------------|--------------|--|
| EM3 | % | uncertainty in mixture ratio, S-IVB |
| EFUEL3 | % | uncertainty in fuel loading, S-IVB |
| EWGT3 | % | uncertainty in inert weight, S-IVB |
| E4OFF1 | sec | uncertainty in S-IVB cutoff, parking orbit insertion |
| E4OFF2 | sec | uncertainty in S-IVB cutoff, waiting orbit insertion |
| EULAGE | % | uncertainty in ullage thrust |
| EVENTR | % | uncertainty in venting thrust |

APPENDIX C

ERROR ANALYSIS SIMULATION RESULTS

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TABLE I
ACTUAL DEVIATIONS AT PARKING ORBIT INSERTION
DUE TO PLATFORM ERRORS

| | R FT | V FT/SEC | BETA E-3 DEG | INCL E-3 DEG | NODE E-3 DEG | PHIT E-3 DEG | FUFL LBS |
|-------|---------|-------------|-----------------|-----------------|-----------------|-----------------|-------------|
| GDSVX | .100 | 5° | 0.00 | -0.8 | -1.2 | 0.0 | -0.0 |
| GDSVY | -.100 | -5° | -0.00 | 0.8 | 1.2 | -0.0 | -0.0 |
| GDSVZ | -.075 | -12° | -0.03 | -0.1 | 2.4 | -0.1 | -0.0 |
| GDSVZ | -.075 | 11° | 0.03 | 0.1 | -2.4 | 0.1 | 0.0 |
| GDSVZ | -.075 | 667° | -1.49 | 5.0 | 0.0 | 0.1 | 0.3 |
| GDSVZ | -.075 | -668° | 1.49 | -5.0 | -0.0 | -0.1 | -0.4 |
| USSVX | .100 | 4° | 0.00 | 0.0 | -0.8 | -1.1 | 0.0 |
| USSVY | -.100 | -4° | -0.00 | -0.0 | 0.8 | 1.1 | 0.0 |
| USSVZ | -.075 | -12° | -0.02 | -0.1 | 2.3 | 9.2 | 0.0 |
| USSVZ | -.075 | 11° | 0.02 | 0.1 | -2.3 | -9.2 | 0.0 |
| USSVZ | -.100 | 0° | 0.00 | 0.0 | -0.0 | -0.1 | 0.1 |
| UISVX | .100 | 0° | 0.00 | 0.0 | 0.0 | -0.0 | -0.0 |
| UISVY | -.100 | 0° | 0.00 | 0.0 | 0.0 | -0.0 | -0.0 |
| UISVZ | -.075 | 0° | 0.00 | 0.0 | -0.0 | -0.0 | -0.0 |
| UISVZ | -.075 | -786° | -1.69 | 6.2 | 0.0 | 0.1 | -1.6 |
| UISVZ | -.075 | -787° | 1.69 | -6.2 | -0.0 | -0.1 | -1.6 |
| UOSVX | .060 | 4° | 0.00 | 0.0 | -0.7 | -1.4 | 0.0 |
| UOSVY | -.060 | -6° | -0.00 | -0.0 | 0.7 | 1.4 | 0.0 |
| UOSVZ | -.060 | -3° | -0.00 | -0.1 | 2.2 | 10.7 | 0.0 |
| UOSVZ | -.060 | 10° | 0.00 | 0.1 | -2.2 | -10.7 | 0.1 |
| UOSVZ | -.060 | 525° | -1.17 | 3.0 | 0.0 | 0.0 | 0.5 |
| UOSVZ | -.060 | -525° | 1.17 | -3.0 | -0.0 | -0.0 | -1.4 |
| SSVX | .050 | -0° | 0.00 | 0.0 | 0.0 | 0.0 | -0.3 |
| SSVY | -.050 | 1° | 0.00 | 0.0 | 0.0 | 0.0 | -0.1 |
| SSVZ | -.050 | 0° | 0.00 | 0.0 | 0.0 | 0.0 | -0.0 |
| SSVZ | -.050 | 0° | 0.00 | 0.0 | 0.0 | 0.0 | -0.0 |
| SSVZ | -.050 | 0° | 0.00 | 0.0 | 0.0 | 0.0 | -0.0 |

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| | R | FT | V | FT/SFC | BETA | INCI | N0 DF | PHIT | E-3 DFG | E-3 DEG | |
|--------|----------|---------|---------|--------|-------|-------|-------|--------|---------|---------|--|
| SFSVX | • 00002 | -117° | -0° 59' | -1° 4 | -1° 4 | -0° 0 | -0° 0 | -2° 2 | -2° 2 | -0° 0 | |
| SFSVY | • 00002 | 123° | 0° 59' | 0° 4 | 0° 4 | 0° 0 | 0° 0 | 1° 7° | 1° 7° | 0° 0 | |
| SFSVZ | • 00002 | -189° | 0° 4 | -0° 7 | -0° 7 | -0° 0 | -0° 0 | -5° 5 | -5° 5 | -0° 4 | |
| ABSVX | • 00002 | -189° | -0° 4 | -0° 7 | -0° 7 | 0° 0 | 0° 0 | 0° 4 | 0° 4 | 0° 0 | |
| ABSVY | • 00002 | 0° | 0° 0 | 0° 0 | 0° 0 | 0° 0 | 0° 0 | -0° 0 | -0° 0 | -0° 0 | |
| ABSVZ | • 00002 | 0° | 0° 0 | -0° 0 | -0° 0 | -0° 0 | -0° 0 | -1° 5° | -1° 5° | -0° 0 | |
| CHI'X | • 001 95 | 2° | 2° | 2° | 2° | 0° 0 | 0° 0 | -1° 4° | -1° 4° | -0° 0 | |
| CHI'Y | • 005 73 | 2° | 2° | 2° | 2° | 0° 0 | 0° 0 | 1° 5° | 1° 5° | -0° 0 | |
| CHI'Z | • 005 72 | 224° | -0° 60 | 1° 0 | 1° 0 | 0° 1 | 0° 1 | 2° 4 | 2° 4 | -0° 0 | |
| FPSVXZ | • 00824 | -293° | 0° 60 | -1° 0 | -1° 0 | 0° 0 | 0° 0 | -0° 6 | -0° 6 | -0° 0 | |
| FPSVYX | • 00824 | 0° | 0° 0 | 0° 0 | 0° 0 | 0° 0 | 0° 0 | -0° 6 | -0° 6 | -0° 0 | |
| FPSVZY | • 00824 | -0° 924 | -2° 0 | 0° 0 | 0° 0 | 0° 0 | 0° 0 | -1° 6° | -1° 6° | -0° 0 | |
| FPSVXY | • 003 93 | 176° | 0° 44° | 1° 4 | 1° 4 | 0° 0 | 0° 0 | -1° 6° | -1° 6° | -0° 0 | |
| FPSVYX | • 002 93 | -75° | -0° 44° | -1° 6 | -1° 6 | 0° 0 | 0° 0 | -1° 5° | -1° 5° | -0° 0 | |
| FPSVYZ | • 00824 | 0° | 0° 0 | 0° 0 | 0° 0 | 0° 0 | 0° 0 | -0° 0 | -0° 0 | -0° 0 | |
| FPSVZY | • 00824 | -0° 834 | 0° | -0° 0 | -0° 0 | -0° 0 | -0° 0 | -0° 0 | -0° 0 | -0° 0 | |
| FPSVZX | • 002 79 | -440° | 0° 54° | -2° 5 | -2° 5 | 0° 0 | 0° 0 | -0° 4 | -0° 4 | 0° 0 | |
| FPSVZY | • 002 79 | 442° | -0° 53° | 2° 5 | 2° 5 | 0° 0 | 0° 0 | 0° 4 | 0° 4 | 0° 0 | |
| FPSVZY | • 00879 | -14° | -0° 0° | -0° 1 | -0° 1 | 2° 3 | 2° 3 | -4° 5 | -4° 5 | 0° 0 | |
| FPSVZX | • 00879 | 17° | 0° 0° | 0° 1 | 0° 1 | -2° 3 | -2° 3 | -4° 6 | -4° 6 | 0° 0 | |
| FPSVZY | • 00824 | 20° | 0° 0° | 0° 1 | 0° 1 | -3° 7 | -3° 7 | -12° 0 | -12° 0 | -0° 1 | |
| PSS | | 13950 | 2° 94° | 9° 4 | 9° 4 | 6° 6 | 6° 6 | 30° 7 | 30° 7 | 30° 8 | |

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TABLE 2

ACTUAL DEVIATIONS AT PARKING ORBIT INSERTION
DUE TO PLATFORM ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SEC | TIMF SEC |
|-------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| GDSVX | -100 | 0° | 293° | 0.00 | 0.00 | 0.37 | 0. |
| GDSVY | -100 | 0° | -293° | -0.00 | -0.00 | -0.37 | 0. |
| GDSVZ | 0.075 | 2° | -755° | -0.00 | -0.01 | -2.76 | 0. |
| GDSVZ | -0.075 | -1° | 765° | 0.00 | 0.01 | 2.77 | 0. |
| USSVX | 0.075 | -212° | 84° | -0.08 | 2.27 | 0.01 | -0.001 |
| USSVY | -0.075 | 213° | -842° | -1° | 0.08 | -3.27 | -0.001 |
| USSVZ | 0.075 | -0° | 0° | 274° | 0.00 | 0.00 | 0.00 |
| USSVY | -0.075 | -2° | -274° | -0.00 | -0.00 | -0.28 | 0. |
| USSVZ | 0.075 | -1° | -768° | -0.00 | -0.00 | -0.28 | 0. |
| USSVZ | -0.075 | 1° | 758° | 0.00 | 0.00 | -2.26 | -0.000 |
| USSVY | 0.075 | -3° | -0° | -0° | 0.00 | 2.26 | 0. |
| USSVZ | -0.075 | 2° | 0° | 0° | 0.00 | -0. | 0. |
| UISVX | 0.075 | -10° | -10° | 0° | 0.00 | 0.00 | 0. |
| UISVY | -0.075 | 10° | 10° | 0° | 0.00 | 0.00 | 0. |
| UISVZ | 0.075 | -17° | -17° | 0° | 0.00 | 0.00 | 0. |
| UISVY | -0.075 | 187° | 187° | -0° | 0.00 | 0.00 | 0. |
| UISVZ | 0.075 | -962° | 962° | 1° | -0.02 | 3.84 | 0.01 |
| UISVY | -0.075 | -963° | -963° | -1° | 0.03 | -3.84 | -0.01 |
| UISVZ | 0.075 | 0° | -0° | 0° | 0.00 | 0.00 | 0.34 |
| UISVY | -0.075 | 0° | 0° | 0° | 0.00 | -0.00 | -0.000 |
| UISVZ | 0.075 | -1° | -1° | -1° | -0.02 | -0.00 | -0.00 |
| UISVY | -0.075 | 1° | 1° | 1° | 0.03 | -0.00 | -0.00 |
| UISVZ | 0.075 | 0° | 0° | 0° | 0.00 | 0.00 | 0. |
| SSSVX | 0.050 | 0° | -707° | -707° | 0.00 | 0.00 | 0. |
| SSSVY | -0.060 | 0° | 707° | 707° | 0.00 | 0.00 | 0. |
| SSSVZ | 0.050 | -0.2° | -0.2° | -0.2° | -0.21 | 2.27 | 0.00 |
| SSSVY | 0.050 | 0.2° | 0.2° | 0.2° | 0.20 | -2.26 | -0.00 |
| SSSVZ | -0.050 | 0.0° | 0.0° | 0.0° | 0.00 | 0.00 | 0. |
| SSSVY | 0.050 | 0.0° | 0.0° | 0.0° | 0.00 | 0.00 | 0. |
| SSSVZ | -0.050 | 0.0° | 0.0° | 0.0° | 0.00 | 0.00 | 0. |
| SSSVY | 0.050 | 0.0° | 0.0° | 0.0° | 0.00 | 0.00 | 0. |
| SSSVZ | -0.050 | 0.0° | 0.0° | 0.0° | 0.00 | 0.00 | 0. |

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| | RDX FT | OPY FT | VPX FT/SFC | VPY FT/SFC | VPZ FT/SFC | TIMF SEC |
|-------|-----------|-----------|---------------|---------------|---------------|-------------|
| FSVX | -0.00002 | 767. | -7. | -0.36 | 0.51 | -0.037 |
| FSVY | -0.00003 | 84. | -7. | 0.26 | -0.52 | 0.037 |
| FSVZ | -0.00002 | -204. | -1. | 0.05 | -0.30 | -0.012 |
| BSVX | -0.00002 | 205. | -110. | -0.06 | 0.20 | -0.013 |
| BSVY | -0.00002 | -1. | -0. | -0.06 | -0.00 | 0.013 |
| BSVZ | -0.00003 | -779. | 0. | 0.00 | -0.00 | 0. |
| H11X | -0.00003 | -739. | -737. | -0.32 | -0.56 | -0.037 |
| H11Y | -0.00003 | -184. | -154. | 0. | -0.63 | 0.037 |
| H11Z | -0.00003 | 156. | 182. | -0.02 | 0.62 | -0.006 |
| PSVXZ | -0.00003 | 1. | -2. | 0. | -0.00 | 0.006 |
| PSVYX | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| PSVYZ | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| PSVXY | -0.00003 | 792. | -185. | 0. | -0.38 | -0.036 |
| PSVYX | -0.00003 | -790. | -186. | -0.21 | 0.38 | -0.036 |
| PSVYY | -0.00003 | 1. | -1. | 0. | -0.00 | 0. |
| PSVZZ | -0.00003 | -1. | 0. | -0.00 | 0. | 0. |
| SVYX | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| SVYY | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| SVZZ | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| SVZX | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| SVZY | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| SVZZ | -0.00003 | 0. | -1. | 0. | -0.00 | 0. |
| RSS | 1491. | 2223. | 2223. | 0.655 | 5.84 | 0.065 |

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TABLE 3
**UNCERTAINTIES AT PARKING ORBIT INSERTION
 DUE TO PLATFORM ERRORS**

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| | FRNX FT | FRNY FT | FRNZ FT | EVNX FT/SEC | EVNY FT/SFC | FVNZ FT/SEC | FVNZ FT |
|--------|------------|------------|------------|----------------|----------------|----------------|------------|
| SFSVX | • 000003 | 756• | 8• | 0• 60 | 0• 07 | 0• 00 | 0• 00 |
| SFSVY | -• 000003 | -262• | -71• | -0• 69 | -0• 07 | -0• 00 | -0• 00 |
| SFSVZ | • 000002 | 9• | 206• | 0• 05 | 0• 43 | 0• 00 | 0• 00 |
| SFSV2 | -• 000003 | -11• | -704• | -0• 05 | -0• 42 | -0• 00 | -0• 00 |
| ABSVX | • 000003 | 1• | 0• | -0• 00 | 0• 00 | -0• 00 | -0• 00 |
| ABSVY | -• 000002 | 218• | -0• | 0• 00 | 0• 00 | 0• 00 | 0• 00 |
| ABSVZ | • 000003 | 5• | -221• | -0• 61 | -0• 06 | -0• 00 | -0• 00 |
| CH1IX | • 00196 | 6• | -254• | -0• 06 | -0• 80 | -0• 00 | -0• 00 |
| CH1IY | • 000573 | 1• | 256• | 0• 06 | 0• 81 | 0• 00 | 0• 00 |
| CH1IZ | • 00196 | 2• | -216• | 0• 00 | 0• 00 | 0• 59 | 0• 59 |
| EPSSVX | -• 00196 | -174• | -184• | -0• 00 | 0• 00 | -0• 50 | -0• 50 |
| EPSSVY | -• 00196 | -178• | -194• | -0• 00 | 0• 00 | -0• 26 | -0• 26 |
| EPSSVZ | -• 00196 | -323• | -216• | -0• 00 | 0• 00 | -0• 00 | -0• 00 |
| EPSVXZ | -• 000834 | 0• | 216• | -0• 00 | 0• 00 | 0• 26 | 0• 26 |
| EPSVYX | -• 000834 | -1• | -178• | -0• 00 | 0• 00 | -0• 00 | -0• 00 |
| EPSVYZ | -• 000834 | -1• | -376• | -0• 00 | 0• 00 | -0• 00 | -0• 00 |
| EPSVZX | -• 000834 | -1• | -374• | -0• 00 | 0• 00 | -0• 00 | -0• 00 |
| EPSVZY | -• 000834 | -1• | -374• | -0• 00 | 0• 00 | -0• 00 | -0• 00 |
| FPSVYX | -• 00278 | 12• | 492• | 1• | 0• 11 | 1• 47 | 0• 00 |
| FPSVZY | -• 00278 | -14• | -484• | -1• | -0• 12 | -1• 47 | 0• 00 |
| FPSVZX | -• 00879 | 3• | -1• | -826• | 0• 00 | 0• 01 | 1• 15 |
| FPSVZY | -• 00879 | -3• | -484• | -1• | -1247• | -0• 01 | -1• 15 |
| FPSVZX | -• 00834 | -4• | -826• | -1• | -1247• | 0• 00 | -2• 22 |
| FPSVZY | -• 00834 | -1• | -484• | -1• | -1247• | 0• 00 | -2• 22 |
| RSS | | | | 1600• | 1.13 | 5.87 | 6.08 |

TABLE 4

ACTUAL DEVIATIONS AT PARKING ORBIT INSERTION
DUE TO PERFORMANCE ERRORS

| | R FT | V FT/SEC | BETA F-2 DFG | INCL. F-2 DFG | NODE F-2 DFG | PHIT F-2 DFG | FUFL LBS |
|--------|---------|-------------|-----------------|------------------|-----------------|-----------------|-------------|
| F1ISP* | 0.415 | 0. | 0. | 0. | -0.0 | -26.6 | 575.8 |
| ENWGT1 | -0.419 | -1. | 0.00 | 0.0 | 0.0 | 37.0 | 555.2 |
| ENWGT1 | 0.715 | -18. | 0.07 | -0.0 | 0.0 | 82.7 | 526.5 |
| F1M* | -0.716 | -6. | 0.07 | 0.0 | 0.1 | 44.6 | 44.6 |
| F1M* | 0.895 | 2. | -C.C0 | C.C | C.C | 183.6 | 214.5 |
| F1UFL* | -0.895 | -6. | C.C1 | -0.C | 0.1 | 235.1 | -330.1 |
| F1UFL* | 0.5 | -25. | 0.07 | -0.1 | 0.0 | 38.1 | 34.6 |
| F1UGT1 | -0.5 | -12. | 0.07 | -0.0 | 0.0 | 39.6 | 72.1 |
| F1UGT1 | 2.946 | 1. | -0.00 | 0.0 | 0.0 | 09.8 | 125.9 |
| FCD | -1.0 | 946 | 1. | 0.00 | 0.0 | -1.0. | 1261.0 |
| FRHMA | -1.0 | 0.0 | -1. | -0.00 | 0.0 | 52.0 | 594.0 |
| F1ISP? | 0.427 | 4. | 0.00 | 0.0 | 0.0 | 52.5 | 598.2 |
| ENWGT2 | -0.427 | -1. | 0.00 | 0.0 | 0.0 | 42.5 | 49.5 |
| F1ISP? | 0.427 | -1. | 0.00 | 0.0 | 0.0 | 44.2 | 49.1 |
| F1UFL? | 0.5 | -1. | 0.00 | 0.0 | 0.0 | 45.9 | 154.0 |
| F1UGT2 | 1.34 | -1. | 0.00 | 0.0 | 0.0 | 57.4 | -152.8 |
| FMD | -1.0 | 26 | -1. | 0.00 | 0.0 | 75.5 | 4 |
| F1UGT2 | 0.895 | -1. | C.CU | -C.C | C.1 | 24.2 | 50C.6 |
| F1UFL? | 0.5 | -1. | -C.C0 | C.C | C.0 | -15.8 | -681.1 |
| F1ISP? | 0.5 | -4. | 0.00 | -0.0 | 0.0 | 71.5 | 99.5 |
| F1UGT2 | 2.0 | 2. | -0.00 | 0.0 | 0.0 | 29.2 | -79.8 |
| F1ISP? | 2.0 | -2. | 0. | 0.0 | 0.0 | 14.6 | -63.4 |
| ENWGT3 | 2.0 | 0.020 | -1. | 0.00 | 0.0 | 48.6 | 444.7 |
| ENWGT3 | -0.020 | -1. | 0.00 | 0.0 | 0.0 | -50.5 | 676.5 |
| F1M? | 2.0 | -2. | 0.00 | -0.0 | 0.0 | 92.1 | -598.1 |
| F1M? | 2.0 | -2. | 0.00 | -0.0 | 0.0 | -222.7 | 49.0 |
| F1M? | 2.0 | -2. | -C.C0 | C.C | C.1 | 244.7 | -55.0 |
| F1M? | -2.0 | -2. | -C.C0 | C.C | C.0 | -272.8 | -43.7 |
| | | | | | | 287.5 | 43.1 |

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| | R | FT | V FT/SFC | BETA F-3 DFG | INCL F-2 DFG | NODE F-2 DFG | PHIT E-2 DFG | FUR LRG |
|---------|--------|------|-------------|-----------------|-----------------|-----------------|-----------------|------------|
| FFFLFL1 | 1.0 | 2. | -0.00 | 0.0 | 0.0 | 0.1 | 209.7 | 430. |
| FWGT2 | -1.0 | 1. | -0.00 | 0.0 | 0.0 | 0.0 | -200.0 | -440.0 |
| | 1.536 | 2. | -0.00 | 0.0 | 0.0 | 0.1 | 217.0 | -1945.1 |
| | -1.430 | -2. | -0.00 | 0.0 | 0.0 | 0.1 | -216.3 | 1934.6 |
| F40FF1 | 0.02 | 0. | -0.70 | 0.1 | 0.0 | 0.0 | -2.0 | -1.6. |
| F40FF2 | 0.02 | 0. | -0.70 | -0.1 | -0.0 | 0.0 | 0.0 | 0.0 |
| FULAGE | 5.0 | 0. | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | -5.0 | 0. | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| FVNTR | 20.0 | 0. | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | -20.0 | 0. | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| RSS | 34. | 0.7C | 0.2 | 0.0 | 0.3 | 724.5 | 5172.8 | |

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TABLE 5

**ACTUAL DEVIATIONS AT PARKING MILE INSERTION
DUE TO PERFORMANCE ERRORS**

| | RPX FT | RPY FT | RPZ FT | Vpx FT/SEC | Vpy FT/SEC | Vpz FT/SEC | TIME SEC |
|--------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| FISP1 | 0. 419 | -45275. | 22191. | -518. | 25.34 | 54.95 | -3. 271 |
| FNWGT1 | -0. 410 | 45551. | -22514. | 521. | -26.72 | -55.40 | 2. 212 |
| FM | 0. 714 | -28372. | 13601. | -318. | 16.17 | 23.65 | -2. 186 |
| EM | -0. 715 | 22656. | -15748. | 365. | -18.68 | -28.78 | -0. 450 |
| FUFL1 | 0. 895 | 62137. | -30009. | 694. | -35.62 | -73.77 | 4. 466 |
| EM | -0. 895 | 75533. | -38463. | 888. | -45.64 | -94.45 | 5. 8C8 |
| FUFL1 | 0. 5 | -9531. | 4554. | -107. | 5.44 | 11.27 | -0. 617 |
| EM | -0. 5 | 13406. | -6468. | 150. | -7.65 | -15.94 | 0. 798 |
| FWGTT1 | 2. 846 | 37171. | -17923. | 415. | -21.27 | -44.13 | -0. 70 |
| ECN | -2. 846 | -7380. | 7926. | -419. | 21.29 | 44.39 | -2. 688 |
| FRHQA | 1.00 | -17933. | -9537. | 200. | -10.25 | -21.20 | -0. 24 |
| FRHQA | -1.00 | -17782. | 8545. | -199. | 10.14 | 21.12 | -1. 252 |
| ECN | 1.00 | 14765. | -7106. | 165. | -8.42 | -17.53 | -0. 67 |
| FISP2 | 0. 477 | -14958. | 7185. | -168. | 8.53 | 17.76 | -1. 034 |
| FNWGT2 | -0. 427 | -53764. | 25769. | -602. | 30.59 | 62.84 | -1. 034 |
| EM | -0. 427 | 53299. | -55720. | 595. | -20.52 | -62.27 | -3. 280 |
| FUFL2 | 1. 34 | -92544. | 20063. | -936. | 47.44 | 90.20 | 2. 775 |
| EM | -1. 34 | 9141. | -44275. | 1020. | -52.49 | -108.57 | -6. 261 |
| EM? | 0. 895 | 8197. | -3546. | 92. | -4.68 | -9.74 | 6. 875 |
| FUFL2 | 0. 5 | -5334. | 2574. | -60. | 3. C5 | 6.36 | -C. 772 |
| EM? | -0. 895 | 10655. | -5172. | 119. | -6.09 | -12.64 | -C. 772 |
| FWGTT2 | 2. 402 | -9579. | 4606. | -108. | 5.47 | 11.29 | -1. 211 |
| EM | -2. 402 | 49623. | -23046. | 554. | -28.42 | -58.97 | -C. 02 |
| FISP2 | 0. 920 | -50249. | 2134. | -554. | 29.65 | 50.78 | C. CS |
| FNWGT3 | 2. 0 | -10585. | 4729. | -243. | 17.48 | 26.44 | -1. 054 |
| EM | -2. 0 | 4605. | 21186. | -15032. | -17.94 | -27.02 | -2. 077 |
| FUFL2 | 2. 0 | -109774. | 52418. | -1231. | 62.22 | 130.24 | 1. 0465 |
| EM | -2. 0 | 115560. | -56496. | 1300. | -67.06 | -128.39 | -5. 171 |
| FNWGT3 | 2. 0 | -92480. | 44211. | -1C37. | 52.48 | 1C9.81 | 5. 464 |
| EM | -2. 0 | 97248. | -47C75. | 1C85. | -55.88 | -115.47 | -4. 323 |
| | | | | | | | 4. 557 |

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| | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SFC | TIME SEC |
|--------|-----------------|-------------------|-------------------|------------------|-----------------|-----------------|
| FFUEL3 | 1.0 -1.0 | 70942. -70844. | -34280. 792. | -40.69 -84.23 | -84.23 -1.29 | 4.002 -3.991 |
| FWGCT3 | 1.936 -1.936 | 73435. -73338. | -35492. 35103. | 40.26 -42.13 | 84.17 -87.19 | 1.037 -1.37 |
| F4AFF1 | 0.01 6.9° | 6.91. -691. | -333. 332. | 41.67 0.26 | 67.08 -1.08 | 4.143 -4.121 |
| F4AFF2 | 0.03 0.02 | 0. 0. | 0. 0. | -0.26 0. | 1.08 0. | 0.010 0.030 |
| FULAGE | 5.0 -5.0 | 0. 0. | 0. 0. | 0. 0. | 0. 0. | 0. 0. |
| FVENTR | 20.0 -20.0 | 0. 0. | 0. 0. | 0. 0. | 0. 0. | 0. 0. |
| RSS | 257532. | 118478. | 2737. | 140.62 | 291.07 | 4.56 |
| | | | | | | 14.762 |

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TABLE 6
**'UNCERTAINTIES AT PARKING ORBIT INSERTION
 DUE TO PERFORMANCE ERRORS**

| | FRNX FT | FRNY FT | FRNZ FT | EVNX FT/SEC | EVNY FT/SEC | EVNZ FT/SEC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| FISP1 | 0.419 | -2. | 1. | 0. | 0.00 | 0.00 |
| FDWGT1 | 0.716 | -3. | 3. | -0. | 0.00 | 0.00 |
| FM1 | -0.716 | 21. | 16. | -0. | -0.01 | 0.02 |
| EM1 | 0.895 | -5. | 8. | -0. | -0.01 | 0.01 |
| EFUEL1 | -0.895 | 8. | 1. | -0. | -0.00 | -0.00 |
| ECD | 0.5 | 15. | 3. | -0. | -0.01 | 0.01 |
| FWGTC1 | -0.5 | 14. | 21. | -0. | -0.01 | 0.01 |
| FWGTC2 | 2.846 | 0. | -0. | -0. | 0.02 | 0.00 |
| FRHQA | 1.0 | -3. | 2. | -0. | 0.00 | 0.00 |
| FISP2 | -1.0 | 2. | -2. | -0. | -0.00 | -0.00 |
| EDWGT2 | -1.0 | 0. | -0. | -0. | -0.00 | -0.00 |
| EM2 | 0.427 | -2. | 4. | -0. | -0.00 | 0.00 |
| EFUEL2 | -0.427 | -3. | -7. | -0. | -0.00 | 0.00 |
| ECD | 1.34 | 5. | -1. | -0. | -0.00 | 0.00 |
| FWGTC1 | -1.34 | -16. | -1. | -0. | -0.00 | -0.00 |
| EM3 | 0.895 | 6. | -2. | -0. | -0.00 | -0.00 |
| EFUEL3 | -0.895 | -13. | -1. | -0. | -0.00 | -0.01 |
| ECD | 0.5 | 7. | 2. | -0. | -0.00 | 0.00 |
| FWGTC2 | -0.5 | -16. | -1. | -0. | -0.00 | -0.00 |
| EM4 | 0.402 | 5. | -3. | -1. | -0.00 | -0.00 |
| EDWGT3 | -0.402 | -2. | 1. | -2. | -0.00 | -0.00 |
| EFUEL4 | 0.929 | 3. | -1. | 4. | -0.00 | 0.01 |
| ECD | -0.929 | 3. | -1. | 1. | 0.00 | 0.00 |
| FWGTC3 | 3.0 | 0. | -1. | 2. | -0.00 | 0.00 |
| EM5 | -3.0 | 0. | -1. | 0. | -0.00 | -0.01 |
| EFUEL5 | 2.0 | -3. | 4. | -2. | 0.00 | 0.00 |
| ECD | -2.0 | -C. | -C. | -2. | 0.00 | -0.00 |

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| | ERNX FT | ERNY FT | ERNZ FT | EVNX FT/SEC | EVNY FT/SEC | FVNZ FT/SEC | FVNZ FT/SEC |
|---------|------------|------------|------------|----------------|----------------|----------------|----------------|
| EFFUEL3 | 1.0 | -2. | -2. | -0.00 | -0.00 | 0.00 | 0.00 |
| EWG T? | 1.936 | -1.936 | 1. | 0.00 | 0.00 | 0.00 | 0.00 |
| E40FFF1 | 0.02 | -0.02 | 3. | -0.00 | -0.00 | -C.CC | -C.CC |
| E40FFF2 | 0.02 | -0.02 | -1. | 0.00 | 0.00 | 0.00 | 0.00 |
| FULAGE | -0.03 | -0.03 | -0. | -0.00 | -0.00 | 0.00 | 0.00 |
| EVENTR | 20.0 | -20.0 | 0 | -0.00 | -0.00 | -0.00 | -0.00 |
| RSS | | | | 0.02 | 0.04 | 0.00 | 0.00 |

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TABLE 7

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT PARKING ORBIT INSERTION

| | R | V | BETA | INCL | NODE | PHIT | FUEL |
|------|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| R | 4.38E 02 | -0.8 | 1.0 | -0.0 | -0.0 | 0.0 | -0.0 |
| V | -3.55E 02 | 9.72E-01 | -0.8 | -0.0 | -0.0 | 0.0 | -0.0 |
| BETA | 1.35E 00 | -2.40E-03 | 3.14E-03 | -0.0 | -0.0 | 0.0 | -0.0 |
| INCL | -2.18E-02 | -4.61E-05 | -1.89E-07 | 2.20E-03 | 1.0 | 0.0 | -0.0 |
| NODE | -6.88E-02 | -2.00E-04 | -6.43E-07 | 1.75E-05 | 8.23E-03 | 0.0 | -0.0 |
| PHIT | 1.49E-01 | 1.06E-03 | 3.22E-07 | 1.22E-07 | 2.26E-06 | 2.20E-01 | -0.5 |
| FUEL | -3.62E 03 | -1.36E 00 | -2.41E-02 | -1.13E-03 | -1.65E-02 | -1.39E 02 | 1.29E 03 |

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TABLE 8

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT PARKING ORBIT INSERTION

| | RPX | RPY | RPZ | VPX | VPY | VPZ | TIME |
|------|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| RPX | 7.45E 04 | -1.0 | 0.7 | -1.0 | -1.0 | -0.6 | 1.0 |
| RPY | -2.65E 09 | 3.56E 04 | -0.7 | 1.0 | 1.0 | 0.6 | -1.0 |
| RPZ | 6.22E 07 | -2.97E 07 | 1.12E 03 | -0.7 | -0.7 | 0.1 | 0.7 |
| VPX | -3.14E 06 | 1.50E 06 | -3.52E 04 | 4.22E 01 | 1.0 | 0.6 | -1.0 |
| VPY | -5.59E 06 | 3.15E 06 | -7.38E 04 | 3.73E 03 | 8.85E 01 | 0.6 | -1.0 |
| VPZ | -1.02E 05 | 4.86E 04 | 3.01E 02 | 5.77E 01 | 1.21E 02 | 2.44E 00 | -0.5 |
| TIME | 3.23E 05 | -1.54E 05 | 3.62E 03 | -1.83E 02 | -3.84E 02 | -5.93E 00 | 4.44E 00 |

TABLE 9

COVARIANCE MATRIX OF UNCERTAINTIES
AT PARKING ORBIT INSERTION

| | ERNX | ERNY | ERNZ | EVNX | EVNY | EVNZ |
|------|-----------|-----------|----------|-----------|----------|----------|
| ERNX | 2.14E 02 | -0.5 | 0.0 | 0.9 | -0.5 | 0.0 |
| ERNY | -6.02E 04 | 5.33E 02 | 0.0 | -0.1 | 1.0 | 0.0 |
| ERNZ | 4.97E 02 | 9.77E 02 | 7.41E 02 | 0.0 | 0.0 | 1.0 |
| EVNX | 6.89E 01 | -2.40E 01 | 2.09E 00 | 3.73E-01 | -0.1 | 0.0 |
| EVNY | -2.16E 02 | 1.03E 03 | 5.91E 00 | -7.68E-02 | 1.95E 00 | 0.0 |
| EVNZ | 4.45E-01 | 4.02E 00 | 1.44E 03 | 5.78E-03 | 2.04E-02 | 2.03E 00 |

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TABLE 10
ACTUAL DEVIATIONS AT FIXED TIME NO. 1
DUE TO PLATFORM ERRORS

| | ERCK FT | ERUR FT | ERUP FT | EVCK FT/SEC | EVUR FT/SEC | EVUP FT/SEC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| GDSVX | .100 | 326. | 1. | 6. | 0.27 | 0.00 |
| GDSVY | -.100 | -326. | -4. | -6. | -0.27 | -0.00 |
| GDSVZ | .075 | -1067. | -9. | -18. | -2.62 | -0.02 |
| GUSSVZ | -.075 | 1067. | 8. | 18. | 2.62 | 0.02 |
| USSVX | -.075 | -825. | 902. | -823. | -0.02 | -1.77 |
| USSVY | .100 | 302. | 2. | 5. | 0.02 | 1.77 |
| USSVZ | -.100 | -302. | -3. | -6. | 0.23 | 0.00 |
| UISVY | .075 | -1013. | -9. | -18. | -0.23 | -0.00 |
| UISVZ | -.075 | 1013. | 7. | 17. | -2.12 | -0.02 |
| UWSVX | .100 | -0. | -1. | 0. | 2.12 | 0.01 |
| UWSVY | -.100 | -0. | -1. | 0. | 0.00 | 0.00 |
| UWSVZ | .100 | -0. | -0. | 0. | 0.00 | 0.00 |
| UISVX | -.100 | -0. | -0. | 0. | 0.00 | 0.00 |
| UISVY | .075 | -0. | -1. | 0. | 0.00 | 0.00 |
| UISVZ | -.075 | 0. | -0. | 0. | 0.00 | 0.00 |
| UWSVX | -.075 | 7. | 914. | 271. | 1. | 1075. |
| UWSVY | -.075 | 7. | 914. | 271. | 1. | -915. |
| UWSVZ | .060 | 271. | 1. | 5. | -4. | -1076. |
| UWSVX | -.060 | -272. | -3. | -4. | -1. | -10.02 |
| UWSVY | .060 | -994. | -8. | -17. | -2.49 | -0.02 |
| UWSVZ | -.060 | 994. | 8. | 16. | 2.49 | 0.02 |
| SSVX | .050 | -705. | -3. | 663. | -0.01 | -664. |
| SSVY | -.050 | 703. | 3. | -703. | -1. | -703. |
| SSVZ | .050 | -0. | 0. | -1. | 1. | -0. |
| SSVX | -.050 | -0. | -0. | -1. | 0. | -0. |
| SSVY | .050 | -0. | -0. | -1. | 0. | -0. |
| SSVZ | -.050 | -0. | -0. | -0. | 0. | -0. |

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| | EKUR FT | ERUP FT | EVCR FT/SEC | EVDR FT/SEC | EVUP FT/SEC |
|---------|------------|------------|----------------|----------------|----------------|
| SFSVX | -0.0003 | 5. | 33. | 0.01 | -0.49 |
| SFSVY | -0.0003 | -5. | -36. | -0.01 | -0.84 |
| SFSVZ | -0.0003 | 2. | 212. | 0.00 | 0.85 |
| SFSVZ | -0.0003 | -2. | -211. | -0.00 | -0.56 |
| ABSVX | -0.0003 | -9. | -9. | -0.00 | 0.56 |
| ABSVY | -0.0003 | -7. | -7. | 0.00 | 0.00 |
| ABSVZ | -0.0003 | 4. | 27. | 0.01 | -0.00 |
| ABSVY | -0.0003 | -4. | -28. | -0.01 | -0.72 |
| ABSVZ | -0.0003 | 2. | 249. | 0.01 | -0.44 |
| ABSVZ | -0.0003 | -3. | -248. | -0.01 | -0.37 |
| CHLX | -0.0003 | -279. | -3. | -0.55 | -0.00 |
| CHLY | -0.0003 | 279. | 2. | 0.55 | -0.01 |
| CHLZ | -0.00196 | 211. | -1. | 0.22 | 0.01 |
| CHLY | -0.00196 | -211. | -3. | -0.22 | -0.00 |
| CHLZ | -0.00573 | -1090. | -9. | -19. | -0.00 |
| EP SVXZ | -0.00834 | 1040. | 8. | 14. | -0.01 |
| EP SVXY | -0.00393 | -0. | -381. | 265. | -0.02 |
| EP SVYX | -0.00393 | -0. | 376. | -265. | -0.05 |
| EP SVYZ | -0.00834 | -6. | -6. | 0.00 | 0.76 |
| EP SVYX | -0.00834 | -6. | -106. | 266. | -0.65 |
| EP SVYZ | -0.00834 | 7. | 105. | -266. | -0.75 |
| EP SVYX | -0.00278 | -0. | -0. | -0.00 | -0.00 |
| EP SVYZ | -0.00278 | 5. | 466. | -0.01 | 1.00 |
| EP SVYX | -0.00278 | -2. | -467. | 0.01 | -1.00 |
| EP SVYZ | -0.00834 | -2. | -948. | 563. | -0.34 |
| EP SVYX | -0.00834 | -0. | 947. | 0.01 | 0.00 |
| EP SVYZ | -0.00834 | 6. | 1594. | 0.01 | 0.01 |
| EP SVYX | -0.00834 | -1593. | -12. | 2.98 | 0.02 |
| RSS | | 2861. | 1581. | 1756. | 5.68 |
| | | | | | 3.27 |
| | | | | | 5.57 |

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TABLE I-1
UNCERTAINTIES AT FIXED TIME NO. 1
DUE TO PLATFORM ERRORS

| | EKNUK FT | EKNUP FT | EKNUR FT/SEC | EVNUP FT/SEC | EVNUR FT/SEC |
|-------|-------------|-------------|-----------------|-----------------|-----------------|
| USSVX | +100 | -326. | -3. | -6. | -0.27 |
| USSVY | -0.100 | 326. | 1. | 6. | 0.00 |
| USSVZ | -0.075 | 1667. | 6. | 18. | 2.62 |
| USSVX | -0.075 | -1067. | -8. | -18. | -2.62 |
| USSVY | -0.075 | 5. | 834. | -902. | 0.02 |
| USSVZ | -0.075 | -5. | -838. | -903. | -0.02 |
| USSVX | -0.100 | -302. | -2. | -5. | -0.23 |
| USSVY | -0.100 | 302. | 5. | 6. | 0.23 |
| USSVZ | -0.075 | 1013. | 5. | 18. | 2.12 |
| USSVX | -0.075 | -1013. | -10. | -16. | -2.12 |
| USSVY | -0.100 | 0. | -2. | 0. | -0.00 |
| USSVZ | -0.100 | -0. | -0. | 0. | -0.00 |
| U1SVX | -0.100 | -0. | 0. | 0. | -0.00 |
| U1SVY | -0.100 | 0. | 0. | 0. | -0.00 |
| U1SVZ | -0.075 | -0.075 | -3. | -2. | -0.00 |
| U1SVX | -0.075 | -0.075 | 0. | 0. | -0.00 |
| U1SVY | -0.075 | -0.075 | 0. | 0. | -0.00 |
| U1SVZ | -0.075 | -0.075 | -1. | -1. | -0.00 |
| U2SVX | -0.060 | -271. | -3. | -5. | -10.75. |
| U2SVY | -0.060 | 272. | -1. | -1. | 10.76. |
| U2SVZ | -0.060 | 994. | 7. | 917. | -920. |
| U3SVX | -0.060 | -994. | -8. | -7. | -920. |
| U3SVY | -0.060 | -994. | -8. | -7. | -920. |
| U3SVZ | -0.060 | 3. | -3. | -2. | -271. |
| U4SVX | -0.060 | -0.060 | -3. | -1. | -271. |
| U4SVY | -0.060 | -0.060 | 0. | -1. | -271. |
| U4SVZ | -0.060 | -0.060 | 0. | 0. | -271. |
| SSVX | -0.050 | -0.050 | 0. | -1. | -720. |
| SSVY | -0.050 | -0.050 | 0. | 2. | -720. |
| SSVZ | -0.050 | -0.050 | 0. | -1. | -720. |

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| | EKNUR FT | EKNUP FT | EVNCR FT/SEC | EVNDR FT/SEC | EVNUP FT/SEC |
|--------|-------------|-------------|-----------------|-----------------|-----------------|
| SFSVX | -0.00003 | -5. | 206. | 199. | 0.49 |
| SFSVY | -0.00003 | 5. | -272. | -203. | -0.48 |
| SFSVZ | -0.00003 | -2. | -127. | 225. | 0.40 |
| SFSVZ | -0.00003 | 2. | 124. | -223. | -0.45 |
| ABSVX | -0.00003 | 6. | -1. | 0. | 0.66 |
| ABSVY | -0.00003 | 0. | 1. | -0.01 | 0.30 |
| ABSVY | -0.00003 | -4. | 232. | 173. | 0.48 |
| ABSVZ | -0.00003 | 4. | -238. | -304. | 0.45 |
| ABSVZ | -0.00003 | 3. | 178. | -302. | -0.42 |
| ABSVZ | -0.00003 | 284. | 1. | 5. | 0.83 |
| CHILX | -0.00196 | -284. | -2. | -5. | -0.83 |
| CHILY | -0.00196 | -211. | -5. | -4. | -0.61 |
| CHILY | -0.00573 | 211. | 3. | 4. | 0.01 |
| CHILZ | -0.00196 | 1096. | 6. | 19. | 0.01 |
| CHILZ | -0.00196 | -1096. | -11. | -19. | -0.01 |
| EPSVXZ | -0.00834 | 0. | -1. | 0. | 0.01 |
| EPSVYX | -0.00834 | -0. | -2. | 0. | 0.01 |
| EPSVYX | -0.00393 | 7. | -348. | -266. | -0.02 |
| EPSVYX | -0.00393 | -6. | 345. | 266. | 0.01 |
| EPSVYX | -0.00834 | -0. | -1. | 0. | 0.01 |
| EPSVYX | -0.00834 | -0. | -334. | 266. | 0.01 |
| EPSVYX | -0.0278 | -4. | 334. | -563. | -0.01 |
| EPSVYX | -0.0278 | 5. | 330. | -563. | 0.01 |
| EPSVYX | -0.00834 | 947. | 10. | 18. | 0.01 |
| EPSVYX | -0.00834 | -947. | -10. | -17. | -0.01 |
| EPSVYX | -0.00834 | -1596. | -16. | -29. | -0.01 |
| KSS | -0.00834 | 1595. | 11. | 28. | 0.02 |
| | | 2862. | 1627. | 1758. | 0.07 |
| | | | | 5.69 | 5.28 |
| | | | | 5.36 | |

TABLE 12
ACTUAL DEVIATIONS AT FIXED TIME NO. 1
DUE TO PERFORMANCE ERRORS

| | ERCR FT | FRDR FT | ERUP FT | EVCR FT/SEC | EVDR FT/SEC | EVUP FT/SFC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| ETISP? | 0.49 | 10. | 22312. | -24. | 0.14 | -0.03 |
| FDWGT1 | -0.49 | -10. | -32884. | -25. | -0.14 | -0.02 |
| FM1 | 0.716 | 5. | 24438. | -33. | 0.08 | -0.00 |
| FM2 | -0.716 | -5. | -25372. | -23. | -0.12 | -0.01 |
| FM3 | 0.895 | -14. | -45193. | -44. | -0.20 | -0.05 |
| EFUEL1 | -0.895 | -18. | -6C153. | -89. | -0.26 | -0.09 |
| EFUEL2 | 0.5 | 10. | 5078. | -29. | 0.01 | 0.02 |
| FWGT1 | -0.5 | -5. | -5502. | -13. | -0.05 | -0.01 |
| FWGT2 | 0.866 | -9. | -27338. | -16. | -0.13 | -0.02 |
| ECD | -2.846 | 5. | 27262. | -16. | 0.09 | -0.02 |
| FP HMA | 1.00 | -5. | -2445. | -4. | -0.06 | -0.00 |
| ETISP2 | -1.00 | 10. | 12301. | -1. | 0.03 | -0.01 |
| EDWGT2 | 1.00 | -10. | -10046. | 2. | -0.06 | -0.00 |
| FM1 | 0.427 | 12. | 10172. | -4. | 0.02 | -0.00 |
| ETISP3 | -0.427 | 12. | 24244. | -15. | 0.14 | -0.02 |
| EDWGT3 | 1.24 | -11. | -24593. | -10. | -0.14 | -0.02 |
| FM2 | -1.24 | 15. | 70029. | -120. | 0.75 | -0.12 |
| FFUEL2 | 0.895 | -19. | -74238. | -112. | -0.29 | -0.17 |
| EWGT2 | -0.895 | -3. | 28849. | -23. | 0.02 | -0.01 |
| ETISP4 | 0.5 | -3. | -35239. | -16. | -0.06 | -0.05 |
| EDWGT4 | -0.5 | 2. | -21252. | -16. | -0.06 | -0.01 |
| FM2 | 2.402 | -2. | 22894. | -11. | 0.03 | -0.01 |
| EFUEL3 | -2.402 | -11. | -22992. | -10. | -0.13 | -0.01 |
| ETISP5 | 0.939 | 8. | 22840. | -16. | 0.10 | -0.02 |
| EDWGT5 | -0.939 | 2. | 2803. | -1. | 0.03 | -0.00 |
| FM2 | 2.0 | -7. | -2854. | 0. | -0.07 | 0.00 |
| FM2 | -2.0 | 23. | 9529. | -6. | 0.21 | -0.00 |
| FM2 | 2.0 | -27. | -10174. | 2. | -0.25 | -0.00 |
| FM2 | 2.0 | 17. | 8C17. | -4. | 0.16 | -0.00 |
| FM2 | -2.0 | -21. | -8468. | 2. | -0.20 | -0.00 |

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| | ERCR | ERDR | ERUP | EVCR | EVDR | EVUP |
|------------------------|--------|---------|------|--------|--------|--------|
| | FT | FT | FT | FT/SFC | FT/SEC | FT/SEC |
| FFI(FFL ²) | 1.0 | -23535. | -8. | -0.19 | -0.02 | 27.07 |
| FFI(FFL ²) | -1.0 | 23233. | -13. | 0.16 | -0.01 | -27.60 |
| FWGT ² | 1.936 | -24367. | -11. | -0.19 | -0.02 | 28.96 |
| FWGT ² | -1.936 | 24048. | -17. | 0.16 | -0.01 | -2E.58 |
| E40FF ¹ | 0.02 | 77. | 16. | -0.00 | 0.68 | 0.14 |
| E40FF ¹ | -0.02 | 0. | -16. | 0.00 | -0.68 | -0.14 |
| E40FF ² | 0.02 | 0. | 0. | 0. | 0. | -0. |
| E40FF ² | -0.02 | 0. | 0. | 0. | 0. | -0. |
| FULAGE | 5.0 | 4. | 1. | -0.00 | 0.04 | 0.01 |
| FULAGE | -5.0 | 0. | -1. | 0.00 | -0.04 | -0.01 |
| EVFNTR | 20.0 | 0. | 0. | -0.00 | 0.01 | 0.00 |
| EVFNTR | -20.0 | 0. | -1. | 0.00 | -0.01 | -0.00 |
| RSS | 55. | 127294. | 166. | 0.66 | 0.72 | 151.19 |

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TABLE F 1.3
UNCERTAINTIES AT FIXED TIME NO. 1
DUE TO PERFORMANCE ERRORS

| | ERNCR FT | ERNR FT | ERNUP FT | FVNCR FT/SEC | FVNR FT/SEC | FVNUP FT/SFC |
|--------|-------------|------------|-------------|-----------------|----------------|-----------------|
| EISP1 | 0.419 | 0. | -4. | 0.00 | 0.00 | -0.00 |
| EDWGT1 | -0.419 | -0. | -5. | 0.00 | -0.00 | 0.00 |
| FDWGT1 | 0.716 | -0. | -2. | 21. | -0.02 | 0.02 |
| FM1 | -0.716 | -0. | -6. | 8. | -0.01 | 0.00 |
| FFUEL1 | 0.895 | -0. | -6. | -1. | 0.00 | -C.C. |
| EWGT1 | -0.895 | -0. | -3. | 10. | -0.02 | C.C. |
| FCD | 0.5 | -0. | -3. | 30. | -0.02 | 0.03 |
| FRHQA | -0.5 | -0. | -6. | 15. | -0.01 | 0.01 |
| EISP2 | 2.846 | -0. | -1. | 2. | -0.00 | 0.00 |
| EDWGT2 | -2.846 | -0. | -4. | -7. | -0.00 | -0.00 |
| FDWGT2 | 1.000 | -0. | 0. | 2. | 0.00 | -0.01 |
| FM2 | -1.000 | -0. | 2. | -1. | 0.00 | -0.00 |
| FFUEL2 | 1.000 | -0. | 1. | -3. | 0.00 | -0.01 |
| FRHQA | -1.000 | -0. | -3. | 3. | -0.00 | -0.00 |
| EISP3 | 0.427 | -0. | -4. | -1. | 0.00 | 0.00 |
| EDWGT3 | -0.427 | -0. | -3. | -1. | 0.00 | -0.00 |
| FDWGT3 | 1.34 | -0. | -5. | -1. | 0.00 | -0.01 |
| FM3 | -1.34 | -0. | -14. | -9. | 0.00 | -0.00 |
| FFUEL3 | 0.895 | -0. | -5. | -1. | 0.00 | -C.C. |
| EWGT2 | -0.895 | -0. | -11. | -8. | 0.00 | -0.01 |
| FCD | 0.5 | -0. | -2. | -6. | 0.00 | -0.00 |
| FRHQA | -0.5 | -0. | -3. | -7. | 0.00 | -0.00 |
| EISP4 | 2.402 | -0. | -2. | -4. | 0.00 | -0.01 |
| EDWGT4 | -2.402 | -0. | -3. | -1. | 0.00 | 0.00 |
| FDWGT4 | 0.929 | -0. | 0. | 0. | 0.00 | 0.00 |
| FM4 | -0.929 | -0. | -1. | 2. | -0.00 | -0.00 |
| FFUEL4 | 2.0 | -0. | 0. | 0. | 0.00 | C.C. |
| EWGT3 | -2.0 | -0. | -5. | 1. | 0.00 | -0.00 |
| FCD | 2.0 | -0. | -2. | -1. | 0.00 | -C.C. |
| FRHQA | -2.0 | -0. | -0. | -0. | 0.00 | -0.00 |

| | FRNCR FT | ERNDR FT | ERNUP FT | EVNCR FT/SFC | EVNDR FT/SFC | EVNUP FT/SFC |
|---------------------|-------------|-------------|-------------|-----------------|-----------------|-----------------|
| EFFUFL ² | -1.0 | -1. | -1. | 0.00 | -0.00 | 0.00 |
| FWGTR ³ | 1.536 | -1.0 | -0.0 | 0.00 | -0.00 | 0.00 |
| E4AFF1 | -1.436 | -1.0 | -1. | 0.00 | -0.00 | -0.00 |
| E4AFF2 | 0.03 | 0.0 | -1. | 0.00 | -0.00 | -0.00 |
| FULAGE | 0.03 | 0.0 | -0. | 0.00 | -0.00 | -0.00 |
| EVENTR | 0.0 | 0.0 | -0. | 0.00 | 0.00 | 0.00 |
| RSS | -2C.0 | -2C.0 | -0. | 0.00 | -0.01 | 0.00 |
| | | | 41. | 0.00 | 0.04 | 0.05 |

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TABLE 14
COVARIANCE MATRIX OR ACTUAL DEVIATIONS
AT FIXED TIME No. 1

| EKCR | ERUR | ERUP | EVCR | EVUR | EVUP |
|-----------|-----------|-----------|-----------|-----------|----------|
| 9.54E 02 | 0.0 | 0.0 | 1.0 | 0.0 | -0.0 |
| 4.72E 02 | 3.74E 04 | -0.1 | 0.1 | -0.0 | -1.0 |
| 1.34E 04 | -1.28E 06 | 5.80E 02 | 0.0 | -0.9 | 0.1 |
| 1.76E 03 | 6.30E 03 | 2.04E 01 | 1.90E 00 | 0.0 | -0.1 |
| 1.57E 01 | -2.40E 02 | -5.65E 02 | 3.51E-02 | 1.11E 00 | -0.0 |
| -5.19E 02 | -1.66E 06 | 2.24E 03 | -1.41E 00 | -8.05E-01 | 4.45E 01 |

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TABLE I

COVARIANCE MATRIX OF UNCERTAINTIES
AT FIXED TIME N₀. 1

| EKNCK | EKNUR | EKNUP | EVNCK | EVNDK | EVNUP |
|----------|-----------|-----------|----------|-----------|----------|
| 9.54E 02 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 |
| 8.01E 03 | 5.40E 02 | -0.8 | 0.0 | 1.0 | -0.9 |
| 1.37E 04 | -2.67E 05 | 5.85E 02 | 0.0 | -0.9 | 1.0 |
| 1.76E 03 | 1.86E 01 | 2.37E 01 | 1.90E 00 | 0.0 | 0.0 |
| 1.59E 01 | 5.83E 02 | -5.08E 02 | 3.79E-02 | 1.09E 00 | -0.9 |
| 3.22E 01 | -8.52E 02 | 1.04E 03 | 5.68E-02 | -1.80E 00 | 1.79E 00 |

TABLE 16
ACTUAL DEVIATIONS AT FIXED TIME NO. 2
DUE TO PLATFORM ERRORS

| | EVRK FT | EVRK FT | EVUP FT | EVUP FT/SEC | EVRK FT/SEC | EVUP FT/SEC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| GU\$VX | .100 | -252. | -242. | 0.37 | 0.01 | 0.30 |
| GU\$VY | -.100 | -253. | 244. | -0.37 | -0.00 | -0.27 |
| GU\$VZ | .075 | -325. | 1163. | -2.90 | -0.03 | -1.42 |
| GU\$VZ | -.075 | 325. | -1191. | 2.90 | 0.04 | 1.45 |
| U\$SVX | -.075 | -5. | 21843. | 0.04 | -0.99 | -23.25 |
| U\$SVX | -.075 | 5. | -21883. | -0.04 | 0.97 | 23.30 |
| U\$SVX | -.100 | 227. | -212. | 0.33 | 0.00 | 0.26 |
| U\$SVY | -.100 | -227. | 264. | -0.33 | -0.01 | -0.32 |
| U\$SVY | -.075 | -403. | 1143. | -2.39 | -0.03 | -1.39 |
| U\$SVZ | -.075 | 403. | -959. | 4. | 2.39 | 1.17 |
| U\$SVZ | -.100 | -20. | -25. | -1. | 0.00 | 0.03 |
| U\$SVZ | -.100 | -20. | -1. | 0.00 | 0.00 | 0.00 |
| UISVX | -.100 | -0. | -0. | -1. | 0.00 | 0.00 |
| UISVY | -.100 | -67. | 0. | -0.00 | 0.00 | 0.08 |
| UISVY | -.075 | -0. | -32. | -1. | 0.00 | 0.04 |
| UISVZ | -.075 | -0. | -19. | -1. | 0.00 | 0.02 |
| UISVZ | -.075 | -6. | 23928. | 0.04 | -1.08 | -25.18 |
| U\$SVX | -.075 | 0. | -23954. | -270. | -0.04 | 1.06 |
| U\$SVX | -.060 | 178. | -212. | 1. | 0.39 | 0.01 |
| U\$SVY | -.060 | -178. | 155. | -2. | -0.39 | -0.00 |
| U\$SVY | -.060 | -287. | 1148. | -2. | 74. | -0.03 |
| U\$SVZ | -.060 | 286. | -1156. | 3. | 2. | 4.41 |
| U\$SVZ | -.060 | -4. | 17172. | 251. | 0.04 | -0.86 |
| U\$SVZ | -.060 | 4. | -16860. | -263. | -0.03 | 0.84 |
| SSVX | -.050 | -0. | -21. | -1. | 0.00 | 0.00 |
| SSVY | -.050 | -0. | -89. | 1. | -0.00 | 0.00 |
| SSVZ | -.050 | -0. | -31. | 0. | 0.00 | 0.00 |
| SSVZ | -.050 | -0. | -38. | 0. | 0.00 | 0.00 |
| SSVZ | -.050 | -0. | -15. | 0. | 0.00 | 0.02 |
| SSVZ | -.050 | -0. | -29. | 0. | 0.00 | 0.03 |

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| | EKUR FT | EKUR FT | EKUP FT | EKUP FT | EVUR FT/SEL | EVUR FT/SEL | EVUP FT/SEL | EVUP FT/SEL |
|--------|------------|------------|------------|------------|----------------|----------------|----------------|----------------|
| SFSVX | •UU003 | -3• | 23331• | -45• | •U07 | -U07 | -U08 | -28•01 |
| SFSVY | -•CC003 | 3• | -23709• | 25• | -U07 | U07 | U07 | 28•46 |
| SFSVZ | •UU003 | 0• | 2767• | -134• | U01 | U01 | U07 | -3•05 |
| SFSVZ | •UU003 | -1• | -2851• | 131• | -U01 | -U01 | 3•70 | |
| ABSVX | •UU003 | -U• | -22• | -0• | U00 | U00 | U00 | 0•03 |
| ABSVX | •UU003 | -0• | 18• | -1• | U00 | U0 | U0 | -0•02 |
| ABSVX | •UU003 | -3• | 2667• | -38• | U07 | -U07 | -U07 | -24•81 |
| ABSVY | •UU003 | 3• | -20894• | 18• | -U07 | U01 | U01 | 25•07 |
| ABSVY | •UU003 | 1• | -524• | -118• | U00 | U00 | U00 | -U05 |
| ABSVZ | •UU003 | -1• | 424• | 116• | -U00 | -U00 | -U00 | 0•17 |
| ABSVZ | •UU003 | -121• | 263• | -2• | -U062 | -U062 | -U062 | -U052 |
| ABSVZ | •UU003 | 121• | -296• | 1• | U062 | U062 | U062 | U036 |
| CHIAX | •CC196 | 141• | -153• | 2• | U029 | U029 | U029 | U019 |
| CHIAY | -•CC196 | -142• | 153• | -2• | -U029 | -U029 | -U029 | -U019 |
| CHIAY | •CC573 | -497• | 1084• | -6• | -2•37 | -2•37 | -2•37 | -1•32 |
| CHIAY | -•CC573 | 497• | -1137• | 6• | U037 | U037 | U037 | U039 |
| CHIZZ | •CC196 | -2• | 10410• | 127• | U03 | U03 | U03 | -11•73 |
| CHIZZ | -•CC196 | 2• | -10409• | -132• | -U03 | -U03 | -U03 | 11•62 |
| EPSVXZ | •UU834 | -U• | -23• | -1• | U00 | U00 | U00 | U00 |
| EPSVXY | -•CC834 | -D• | -41• | -1• | U00 | U00 | U00 | U00 |
| EPSVXY | •UU834 | 1• | -20982• | 57• | -U07 | U07 | U07 | 25•38 |
| EPSVYZ | -•CC834 | -1• | 20920• | -79• | U07 | U07 | U07 | -22•50 |
| EPSVYZ | •UU834 | -U• | -28• | -1• | -U09 | -U09 | -U09 | U09 |
| EPSVYY | -•CC834 | -U• | 16• | -1• | U00 | U00 | U00 | U00 |
| EPSVYY | •UU278 | 2• | -192• | 233• | U01 | U01 | U01 | -U02 |
| EPSVYY | -•CC278 | -2• | 5• | 233• | -U01 | -U01 | -U01 | 1•21 |
| EPSVYY | •UU679 | -033• | 778• | -6• | -1•32 | -1•32 | -1•32 | -U095 |
| EPSVYY | -•CC679 | 032• | -762• | 7• | 1•32 | 1•32 | 1•32 | 0•93 |
| EPSVZX | •UU834 | 722• | -1665• | 8• | 3•43 | 3•43 | 3•43 | 2•03 |
| EPSVZX | -•CC834 | -726• | 1578• | -9• | -3•43 | -3•43 | -3•43 | -1•92 |
| RSS | 13020. | 53981• | 501• | 6•45 | 2•12 | 2•12 | 2•12 | 01•47 |

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TABLE 17
UNCERTAINTIES AT FIXED TIME NO. 2
DUUE TO PLATFORM ERRORS

| ERNUX FT | ERNUY FT | ERNUZ FT | ERNUP FT | ERNUR FT/SEC | ERNUU FT/SEC |
|-------------|-------------|-------------|-------------|-----------------|-----------------|
| GUSSX .100 | -252. | 237. | -3. | -0.37 | -0.01 |
| GUSSY -.100 | 253. | -215. | 3. | 0.37 | 0.00 |
| GUSSY .075 | 326. | -1185. | 4. | 2.90 | 0.03 |
| GUSSY -.075 | -320. | 1220. | -3. | -2.90 | -0.04 |
| GUSSZ .075 | 5. | -21796. | -241. | -0.34 | 0.97 |
| GUSSZ -.075 | -5. | 21840. | 215. | 0.94 | -1.00 |
| GUSSX .100 | -227. | 194. | -2. | -0.33 | -0.00 |
| GUSSX -.100 | 228. | -258. | 2. | 0.33 | 0.01 |
| GUSSY .075 | 404. | -1103. | 5. | 2.39 | 0.03 |
| GUSSY -.075 | -404. | 942. | -4. | -2.39 | -0.03 |
| GUSSZ .100 | 0. | 27. | 0. | -0.00 | -0.00 |
| GUSSZ -.100 | 0. | 0. | 0. | -0.00 | -0.00 |
| GUSSX .100 | 0. | -10. | 0. | -0.00 | -0.00 |
| GUSSY .100 | -100. | 0. | 0. | -0.00 | -0.00 |
| GUSSZ .100 | 0. | 0. | 0. | -0.00 | -0.00 |
| UISVX .075 | 0. | 20. | -0. | -0.00 | -0.00 |
| UISVY .075 | 0. | 56. | 0. | 0.00 | -0.00 |
| UISVZ .075 | 0. | -10. | 1. | -0.00 | -0.00 |
| UISVX -.075 | -100. | 0. | 0. | -0.00 | -0.00 |
| UISVY -.075 | 0. | 0. | 0. | -0.00 | -0.00 |
| UISVZ -.075 | 0. | -10. | 1. | -0.00 | -0.00 |
| UWSVX .060 | 0. | 23915. | -206. | -0.04 | 1.07 |
| UWSVY .060 | -0. | 23936. | 235. | 0.04 | -1.09 |
| UWSVZ .060 | 0. | -178. | 209. | -2. | -0.01 |
| UWSVX -.060 | -0. | 178. | -161. | 2. | 0.00 |
| UWSVY -.060 | 0. | 178. | -160. | 3. | 2.74 |
| UWSVZ -.060 | 0. | -178. | 145. | -3. | -2.74 |
| SUVX .050 | 0. | 287. | -160. | 1. | -0.04 |
| SUVY .050 | -0. | 287. | 145. | -1. | 0.04 |
| SUVZ .050 | 0. | 4. | -17096. | -259. | -0.04 |
| SUVX -.050 | -0. | 4. | 16809. | 245. | 0.03 |
| SUVY -.050 | 0. | 0. | 0. | -0.00 | -0.00 |
| SUVZ -.050 | 0. | 0. | 0. | -0.00 | -0.00 |
| SSVX .050 | -0. | 80. | 80. | -1. | 0.00 |
| SSVY .050 | 0. | 26. | 26. | -2. | 0.00 |
| SSVZ .050 | -0. | 45. | 45. | -3. | 0.00 |
| SSVX -.050 | 0. | 10. | 10. | -4. | 0.00 |
| SSVY -.050 | -0. | 34. | 34. | -5. | 0.00 |
| SSVZ -.050 | 0. | -0. | -0. | -6. | 0.00 |

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| | EKNUR FT | EKNUR FT | EKNUP FT | EVNUR FT/SEC | EVNUP FT/SEC |
|--------|-------------|-------------|-------------|-----------------|-----------------|
| SFSVX | .00000 | .0. | -23060. | .29. | .0.09 |
| SFSVY | -.00003 | -.3. | 23490. | .0.07 | .0.73 |
| SFSVZ | .00003 | -.0. | -26240. | -.0.01 | -.0.08 |
| ABSVX | -.00003 | 1. | 21870. | 1.34. | .0.43 |
| ABSVY | -.00003 | 0. | 21. | 0. | -.0.02 |
| ABSVZ | -.00003 | 0. | -24. | 0. | .0.03 |
| ABSVX | -.00003 | 3. | -21780. | 23. | .0.05 |
| ABSVY | -.00003 | -.3. | 22036. | -.0.07 | -.0.09 |
| ABSVZ | -.00003 | 1. | 1350. | 108. | -.0.17 |
| ABSVX | -.00003 | 1. | -1201. | -105. | .0.16 |
| ABSVY | -.00003 | 112. | -280. | 2. | .0.01 |
| ABSVZ | -.00003 | 111. | 313. | -.1. | -.0.01 |
| CHLIX | .00196 | -141. | 153. | -.1. | -.0.07 |
| CHLIZ | -.00196 | 142. | -129. | 2. | .0.70 |
| CHLY | -.00573 | 498. | -1078. | 6. | .0.35 |
| CHLIZ | -.00573 | -497. | 1101. | -.6. | -.0.18 |
| CHLIZ | -.00196 | 2. | -10308. | -129. | -.0.00 |
| EPSVXZ | -.00196 | -2. | 10440. | 124. | .0.19 |
| EPSVYX | -.00834 | 0. | 23. | 0. | -.0.19 |
| EPSVYZ | -.00834 | 0. | 41. | 0. | -.0.19 |
| EPSVXY | -.00393 | 0. | 20548. | -84. | 0.06 |
| EPSVYX | -.00393 | 1. | -20409. | 67. | 0.06 |
| EPSVYZ | -.00834 | 0. | 39. | 0. | 0.00 |
| EPSVYX | -.00834 | 0. | 3. | 1. | 0.00 |
| EPSVYX | -.00278 | -2. | 382. | 231. | 0.01 |
| EPSVYZ | -.00278 | 2. | -148. | -230. | 0.01 |
| EPSVYX | -.00879 | 034. | -772. | 8. | 1.02 |
| EPSVYZ | -.00879 | -633. | 771. | -7. | -1.02 |
| EPSVYX | -.00834 | -724. | 1678. | -9. | -3.04 |
| EPSVYZ | -.00834 | 724. | -1589. | 9. | 3.04 |
| KSS | 1306. | 54128. | 555. | 0.46 | 2.010 |
| | | | | | 61.04 |

TABLE 18

ACTUAL DEVIATIONS AT FIXED TIME NO. 2
DUE TO PERFORMANCE ERRORS

| | ERCR FT | ERDP FT | ERUP FT | FVCR FT/SEC | FVDR FT/SEC | FVUP FT/SFC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| FISP1 | 0.419 | -13. | 33396. | 0.14 | 0.01 | -29.41 |
| FDWGT1 | -0.419 | 14. | -34016. | -0.14 | -0.07 | 40.35 |
| FM1 | 0.716 | -6. | 25007. | -0.08 | 0.01 | -29.66 |
| FFUFL1 | -0.716 | 12. | -26860. | -0.12 | -C.03 | 31.85 |
| FWGT1 | 0.895 | 2C. | -46792. | -0.20 | -0.11 | 55.51 |
| FCN | -0.895 | 26. | -62520. | -0.26 | -0.15 | 74.17 |
| FISP2 | 0.5 | -1. | 5792. | 0.02 | 0.02 | -6.61 |
| FRHNA | -0.5 | 5. | -5913. | -0.05 | -0.01 | 7.07 |
| FWGT2 | 2.846 | 13. | -28256. | -0.13 | -0.05 | 23.52 |
| FFUFL2 | -2.846 | -8. | 27993. | -0.09 | 0.02 | -33.70 |
| FCN | 10.0 | 6. | -12832. | -0.06 | -0.02 | 15.22 |
| FRHNA | -10.0 | -2. | -12659. | -0.03 | 0.01 | -15.01 |
| FISP2 | 0.427 | 5. | -10598. | -0.06 | -0.01 | 12.57 |
| FDWGT2 | -0.427 | 16. | 10542. | 0.02 | 0.01 | -12.50 |
| FWGT2 | 1.24 | -20. | 25288. | -106. | 0.07 | -20.01 |
| FFUFL2 | -1.24 | -15. | -25686. | 78. | -0.06 | 20.48 |
| EM2 | -1.34 | 27. | 70454. | -140. | -0.14 | -82.61 |
| FISP2 | 0.895 | 4. | -75073. | -93. | -0.15 | 89.11 |
| FDWGT3 | -0.895 | 4. | 29028. | -44. | -0.02 | -34.47 |
| FFUFL2 | 0.5 | 0. | -35792. | 9. | -0.06 | 42.51 |
| EM2 | -0.5 | 4. | -23065. | -35. | -0.06 | 27.76 |
| FWGT2 | 2.402 | 0. | 22766. | 9. | 0.00 | -27.01 |
| FFUFL2 | -2.402 | 15. | -24059. | 73. | -0.05 | 28.55 |
| FISP2 | 0.939 | -10. | 23909. | -102. | 0.02 | -23.37 |
| FDWGT3 | -0.939 | -4. | 3378. | -42. | 0.02 | -2.95 |
| FFUFL2 | 0.0 | 10. | -2300. | -39. | -0.07 | 2.97 |
| EM2 | -2.0 | -30. | 9685. | 8. | 0.21 | -11.50 |
| FISP2 | 2.0 | 37. | -10286. | -15. | -0.25 | 0.01 |
| FDWGT3 | -2.0 | -23. | 8085. | 13. | 0.16 | -0.02 |
| FFUFL2 | 2.0 | 29. | -8463. | -16. | -0.20 | -6.60 |

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| | ERCR FT | ERDR FT | ERUP FT | FVCR FT/SEC | FVDR FT/SFC | FVUP FT/SEC |
|---------|------------|------------|------------|----------------|----------------|----------------|
| FFUFL? | 1.0 | -23349. | -57. | -0.18 | 0.07 | 27.70 |
| FWGT? | -1.0 | 22948. | 30. | 0.15 | -0.05 | -27.22 |
| | 1.536 | -24075. | -55. | -0.19 | 0.01 | 26.57 |
| | -1.536 | -23845. | 28. | 0.16 | -0.05 | -26.29 |
| F40FF1 | • 02 | 6. | -22446. | 8. | -0.06 | 0.67 |
| F40FF2 | -• 03 | -5. | 22447. | -3. | 0.06 | -0.70 |
| | • 02 | -0. | 0. | 0. | 0. | -26.28 |
| | -• 02 | -0. | 0. | 0. | 0. | 0. |
| FULLAGE | 5.0 | 0. | -1394. | 1. | 0.00 | 0.04 |
| | -5.0 | -0. | 1395. | -7. | 0.00 | -0.04 |
| FVNTR | 20.0 | 5. | -32848. | 3609. | -0.09 | -0.06 |
| | -20.0 | -5. | 32817. | -3654. | 0.09 | 2.00 |
| RSS | | 76. | 135954. | 3667. | 0.67 | 2.19 |
| | | | | | | 161.34 |

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TABLE 10
UNCERTAINTIES AT FIXED TIME NO. 2
DUE TO PERFORMANCE ERRORS

| | FRNCR FT | FRNDR FT | ERNUP FT | EVNCR FT/SEC | EVNDR FT/SEC | EVNUP FT/SEC |
|--------------------|-------------|-------------|-------------|-----------------|-----------------|-----------------|
| FISP ¹ | 0. 419 | 0. | -989. | -0.00 | -0.06 | 1.17 |
| EDWGT ¹ | -0. 419 | -0. | 1013. | 0.00 | 0.05 | -1.21 |
| FM ¹ | 0. 716 | -0. | -595. | -0.00 | -0.02 | C.77 |
| FM ¹ | -0. 716 | -0. | 367. | -0.00 | 0.01 | -0.44 |
| FFUEL ¹ | 0. 895 | -C. | 1309. | -142. | 0.08 | -1.57 |
| FFUEL ¹ | -0. 895 | -1. | 2143. | -216. | 0.11 | -2.54 |
| FCD | 0.5 | -0. | -723. | 65. | -0.00 | -0.04 |
| FWGT ¹ | 2. 846 | -0. | 243. | -34. | 0.02 | -0.28 |
| FRH0A | 1.0 | -0. | 747. | -87. | 0.04 | -0.89 |
| FISP ² | 10.0 | 0. | -652. | 85. | -0.05 | 0.77 |
| FCD | -10.0 | -0. | 229. | -35. | 0.02 | -0.28 |
| FRH0A | 1.0 | -0. | -317. | 38. | -0.02 | C.28 |
| FISP ² | -10.0 | -0. | 405. | -32. | 0.01 | -0.49 |
| EDWGT ² | 1.24 | -0. | -236. | 37. | -0.02 | 0.40 |
| FCD | 0.427 | -0. | -872. | 102. | -0.06 | 1.04 |
| EDWGT ² | -0.427 | -0. | 892. | -102. | 0.06 | -1.07 |
| FISP ² | 1.24 | -0. | -471. | 51. | -0.02 | 0.56 |
| FM ² | -1.24 | -0. | 925. | -65. | 0.03 | -1.12 |
| FWGT ² | 0.895 | -C. | -180. | 33. | -0.02 | C.22 |
| FFUEL ² | -0.895 | -0. | 551. | -48. | 0.02 | -C.68 |
| FCD | 0.5 | -0. | -192. | 19. | -0.01 | 0.32 |
| EDWGT ² | 2.402 | -0. | -0. | -14. | 0.01 | -0.02 |
| EDWGT ² | -2.402 | 0. | 873. | -95. | 0.05 | -1.04 |
| FISP ² | 0.929 | -0. | -952. | 99. | -0.05 | 1.15 |
| FM ² | -0.929 | -0. | -376. | 45. | -0.03 | C.45 |
| EDWGT ² | 3.0 | -0. | 293. | -41. | 0.02 | -C.26 |
| FM ² | -2.0 | -0. | -82. | 5. | 0.00 | C.10 |
| FM ² | 2.0 | -0. | 55. | -2. | 0.00 | -0.07 |
| FM ² | -2.0 | -C. | -5. | -2. | 0.00 | C.01 |
| FM ² | 2.0 | -C. | -58. | 3. | -0.00 | C.07 |

| | FRNCR FT | FRNNR FT | FRNUP FT | EVNCR FT / SEC | EVNNR FT / SEC | EVNUP FT / SFC |
|--------------------|-------------|-------------|-------------|-------------------|-------------------|-------------------|
| FFUFL ² | 1.0 | -0. | 29. | -0.00 | -0.02 | C. 74 |
| FWGT ² | -1.0 | 294. | -30. | 0.00 | 0.02 | -C. 75 |
| -1.936 | -0. | -238. | 31. | -C.00 | -0.02 | C. 28 |
| F4FFF ¹ | -1.936 | 207. | -29. | 0.00 | 0.02 | -C.25 |
| • 03 | 0. | 7. | 1. | 0.00 | -0.00 | -C.25 |
| F4FFF ² | -• 03 | -0. | -2. | 0.00 | -0.00 | -0.01 |
| • 03 | -0. | -0. | 0. | 0.00 | -0.00 | 0.07 |
| FULAGF | -• 03 | -0. | 0. | -0. | -0. | -0. |
| 5.0 | -0. | -0. | -0. | -0. | -0. | -0. |
| FULAGF | 5.0 | -0. | -79. | 1.0 | 0.00 | 0.00 |
| -5.0 | -0. | -0. | -172. | 2. | -0.00 | 0.00 |
| EVFNTR | 20.0 | -5. | 37843. | -1670. | 0.09 | 1.98 |
| -20.0 | 4. | -32822. | 3615. | -0.09 | -2.04 | -39.19 |
| RSS | 5. | 33CC3. | 3684. | 0.09 | 2.05 | 29.16 |
| | | | | | | 39.38 |

TABLE 20

COVARIANCE MATRIX FOR ACTUAL DEVIATIONS
AT FIXED TIME NO. 2

| | ERCR | ERDR | ERUP | EVCR | EVDR | EVUP |
|------|-----------|-----------|-----------|-----------|----------|----------|
| ERCR | 4.36E 02 | -0.1 | 0.0 | 0.9 | 0.0 | 0.1 |
| ERDR | -1.11E 06 | 4.41E 04 | -0.3 | 0.1 | -0.2 | -1.0 |
| ERUP | 4.40E 03 | -1.43E 07 | 1.22E 03 | -0.0 | -0.7 | 0.3 |
| EVCR | 8.34E 02 | 5.52E 03 | -3.30E 01 | 2.16E 00 | 0.0 | -0.1 |
| EVDR | 1.25E 01 | -6.75E 03 | -9.11E 02 | 4.50E-02 | 1.01E 00 | 0.1 |
| EVUP | 1.33E 03 | -2.29E 06 | 1.73E 04 | -6.46E 00 | 7.10E 00 | 5.19E 01 |

TABLE 21

COVARIANCE MATRIX OF UNCERTAINTIES
AT FIXED TIME NO. 2

| ERNUK | ERNUK | ERNUP | EVNUK | EVNUK | EVNUP |
|-----------|-----------|-----------|----------|----------|----------|
| 4.35E 02 | -0.1 | 0.0 | 0.9 | 0.0 | 0.1 |
| -4.73E 05 | 2.10E 04 | -0.5 | -0.0 | -0.2 | -1.0 |
| 3.73E 03 | -1.19E 07 | 1.24E 03 | -0.0 | -0.8 | 0.5 |
| 8.39E 02 | -1.01E 03 | -2.35E 01 | 2.15E 00 | 0.0 | 0.0 |
| 1.23E 01 | -4.84E 03 | -9.04E 02 | 5.16E-02 | 9.65E-01 | 0.2 |
| 5.70E 02 | -5.09E 05 | 1.45E 04 | 1.29E 00 | 4.85E 00 | 2.42E 01 |

TABLE ??

ACTUAL DEVIATIONS AT S-IVB REIGNITION
DUE TO PLATFORM ERRORS

| R | V | BETA | INCL | NODF | PHT | FUFL |
|-------|--------|---------|---------|---------|---------|-------|
| FT | FT/SEC | F-3 DEG | E-3 DEG | E-3 DEG | E-3 DEG | LBS |
| GDSVX | • 100 | 0.00 | -0.9 | -1.2 | -0.6 | -0.0 |
| GDSVY | -• 100 | 0.00 | 0.9 | 1.2 | 0.6 | -0.0 |
| GDSVZ | • 075 | -0.01 | -0.1 | 2.4 | 3.1 | -0.0 |
| GDSVZ | -• 075 | 24.0 | 0.01 | -2.4 | -3.2 | 0.0 |
| GDSVZ | • 075 | 1.084 | -1.09 | 3.7 | -0.2 | 0.3 |
| GDSVZ | -• 075 | -1.081 | 1.09 | -3.7 | 55.6 | -0.4 |
| USSVX | • 100 | 6.0 | 0.00 | 0.0 | 0.7 | -0.0 |
| USSVY | -• 100 | -7.0 | -0.00 | -0.8 | -1.1 | -0.5 |
| USSVY | • 075 | -2.1 | -0.01 | 0.8 | 1.1 | 0.7 |
| USSVZ | -• 075 | 22.0 | 0.01 | -0.1 | 2.3 | 3.1 |
| USSVZ | • 100 | 1.0 | 0.00 | 0.0 | -2.3 | -2.5 |
| USSVZ | -• 100 | -0.0 | 0.00 | 0.0 | -0.1 | -0.1 |
| UISVX | • 100 | -1.0 | 0.00 | 0.0 | 0.0 | 0.0 |
| UISVY | -• 100 | 1.0 | 0.00 | 0.0 | -0.1 | -0.1 |
| UISVZ | • 075 | 0.0 | 0.00 | 0.0 | 0.0 | 0.0 |
| UISVZ | -• 075 | 1.294 | -2.30 | 4.6 | -0.2 | 60.8 |
| UISVZ | • 060 | 6.0 | 0.00 | 0.0 | 0.2 | -60.9 |
| UISVZ | -• 060 | -5.0 | 0.00 | -0.7 | -1.4 | -0.6 |
| UASVY | • 060 | -23.0 | -0.01 | -0.1 | 1.4 | 0.4 |
| UASVY | -• 060 | 23.0 | 0.01 | 0.1 | -10.7 | 3.1 |
| UASVZ | • 060 | 760. | -1.45 | 2.0 | -0.2 | -3.0 |
| UASVZ | -• 060 | -760. | 1.44 | -2.0 | 0.0 | 43.6 |
| SSVX | • 050 | -23.0 | 0.00 | 0.0 | 0.0 | -42.8 |
| SSVY | -• 050 | 23.0 | 0.01 | 0.1 | 0.0 | -0.3 |
| SSVZ | • 050 | 1.0 | 0.00 | 0.0 | -0.2 | -0.0 |
| SSVZ | -• 050 | -0.0 | 0.00 | 0.0 | -0.1 | -0.0 |
| SSVZ | • 050 | -0.0 | 0.00 | 0.0 | -0.0 | -0.0 |
| SSVZ | -• 050 | 0.0 | 0.00 | 0.0 | -0.0 | -0.0 |

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| | R | V | BETA F-3 DEG | INCL E-3 DEG | NODE E-3 DEG | PHIT E-3 DEG | FUEL LBS |
|------|---------|--------|-----------------|-----------------|-----------------|-----------------|-------------|
| FSVX | -000003 | -2.83. | -0.40 | -0.0 | -0.3 | 61.1 | 1.70. |
| FSVY | -000003 | 2.98. | 0.40 | 0.0 | 0.3 | -62.7 | -1.70. |
| FSVZ | -000003 | -2.54. | 0.22 | -0.7 | -0.0 | 7.4 | 5.5 |
| FSVZ | -000002 | 2.53. | -0.21 | 0.7 | 0.0 | -7.9 | -5.5 |
| SVX | -000003 | 0. | 0.00 | 0.0 | 0.0 | -0.1 | -0.0 |
| SVX | -000003 | -7. | 0.00 | 0.0 | 0.0 | 0.1 | 0.0 |
| SVX | -000003 | -245. | -0.36 | -0.0 | 0.0 | 57.7 | 15.1 |
| SVY | -000003 | 247. | 0.37 | -1.8 | -0.3 | -58.4 | -15.3 |
| SVY | -000003 | -253. | 0.44 | -1.2 | -0.0 | -2.9 | 4.3 |
| SVZ | -000003 | 353. | -0.42 | -1.2 | 0.0 | 2.5 | -4.4 |
| SVZ | -000003 | -5. | 0.00 | -0.0 | 0.0 | 2.4 | -0.0 |
| SVZ | -000003 | 6. | 0.00 | 0.0 | 0.6 | 0.8 | -0.0 |
| X | -000196 | 5. | -0.00 | 0.0 | -0.6 | -2.4 | -0.0 |
| X | -000196 | -5. | 0.00 | 0.0 | -0.5 | -1.0 | -0.4 |
| X | -000196 | 00573 | -25. | -0.01 | 0.5 | 1.0 | -0.1 |
| Y | -000196 | -00573 | 25. | 0.01 | 0.1 | 2.5 | 0.3 |
| Y | -000196 | 290. | -0.68 | 0.4 | -2.5 | 9.0 | 2.9 |
| Z | -000196 | -289. | 0.68 | -0.4 | -0.0 | -9.0 | -2.9 |
| SVX7 | -000834 | 0. | 0.00 | 0.0 | 0.0 | -0.1 | -0.0 |
| SVX7 | -000834 | 0. | 0.00 | 0.0 | 0.0 | 26.7 | 1.0 |
| SVXY | -000293 | 356. | 0.24 | 2.2 | 0.0 | -26.9 | -1.2 |
| SVYZ | -000293 | -357. | -0.23 | -2.7 | -0.0 | -0.1 | -0.0 |
| SVYY | -000834 | 0. | 0.00 | 0.0 | 0.0 | -0.1 | -0.0 |
| SVYY | -000834 | 0. | 0.00 | 0.0 | 0.0 | -54.6 | -16.9 |
| SVYY | -000278 | -551. | 0.80 | -2.2 | -0.3 | 54.4 | 16.7 |
| SVZY | -000278 | 552. | -0.79 | 2.2 | 0.0 | -0.1 | -0.0 |
| SVZY | -000879 | -22. | -0.00 | -0.4 | 2.3 | 2.0 | -8.7 |
| SVZY | -000879 | 22. | 0.00 | 0.1 | 4.6 | -2.1 | 0.0 |
| SVZX | -000834 | 18. | 0.01 | 0.2 | -4.6 | -2.1 | -4.4 |
| SVZX | -000834 | -36. | -0.01 | -0.2 | -3.7 | -13.0 | -0.1 |
| RSS | | | | | | 4.2 | -0.0 |
| | | | | | | 13.0 | 140.8 |
| | | | | | | 6.6 | 7.7 |
| | | | | | | 3.61 | 21.01 |

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TABLE ??
ACTUAL DEVIATIONS AT S-IVB REIGNITION
DUE TO PLATFORM ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SEC | TIMF SEC |
|-------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| GDSVX | * 100 | -184. | 158. | 0.19 | 0.22 | 0. | 0. |
| GDSVY | -0.100 | 170. | -146. | -0.17 | -0.21 | -0.20 | -0.000 |
| GDSVZ | * 075 | 914. | -781. | -0.91 | -1.10 | -2.48 | 0.000 |
| GDSVZ | * 075 | -939. | 802. | 1358. | 0.93 | 1.13 | -0.001 |
| GDSVZ | * 075 | 16582. | -12760. | 332. | -16.52 | 2.48 | -0.002 |
| GDSVZ | -0.075 | -16628. | 13776. | -332. | -16.55 | -16.28 | -0.40 |
| USSVX | * 100 | -150. | 129. | 325. | 0.15 | 0.40 | 0.001 |
| USSVY | -0.100 | 200. | -172. | -324. | -0.21 | -0.24 | 0.000 |
| USSVY | * 075 | 898. | -769. | -1235. | -0.90 | -1.08 | -0.000 |
| USSVZ | -0.075 | -726. | 672. | 1239. | 0.72 | -1.96 | 0.000 |
| USSVZ | * 100 | -19. | 17. | -0. | 0.02 | 0.02 | 0.000 |
| USSVZ | -0.100 | -2. | 0. | 0. | 0.00 | 0.00 | -0.000 |
| UISVX | * 100 | 7. | -6. | 0. | -0.01 | -0.01 | 0. |
| UISVY | -0.100 | -36. | 32. | -1. | 0.04 | 0.04 | 0.000 |
| UISVY | * 075 | -41. | 35. | -1. | 0.04 | 0.05 | 0.000 |
| UISVZ | -0.075 | -13. | 11. | -0. | 0.01 | 0.02 | 0.00 |
| UISVZ | * 075 | 18222. | -13887. | 364. | -18.03 | -17.56 | -0.44 |
| UISVZ | -0.075 | -18252. | 13985. | -364. | 18.03 | 17.60 | 0.44 |
| UASVX | * 060 | -163. | 140. | 202. | 0.17 | 0.20 | 0.00 |
| UASVY | -0.060 | 127. | -108. | -203. | -0.12 | -0.15 | 0.00 |
| UASVY | * 060 | 895. | -765. | -1261. | -0.89 | -1.08 | -2.33 |
| UASVZ | -0.060 | -880. | 751. | 1261. | 0.87 | 1.06 | 2.33 |
| UASVZ | * 060 | 12955. | -10081. | 261. | -13.16 | -13.17 | -0.32 |
| SSVX | * 050 | -12746. | 9885. | -257. | 12.92 | 12.92 | 0.31 |
| SSVY | -0.050 | 7. | -2. | 0. | -0.00 | -0.00 | 0.002 |
| SSVY | * 050 | -58. | 52. | -1. | 0.06 | 0.07 | 0.000 |
| SSVZ | -0.050 | -19. | 15. | -0. | 0.02 | 0.02 | 0.00 |
| SSVZ | * 050 | -33. | 29. | -1. | 0.04 | 0.04 | -0.000 |
| SSVZ | -0.050 | -10. | 9. | -0. | 0.01 | 0.01 | 0.00 |
| SSVZ | * 050 | -26. | 22. | -1. | 0.03 | 0.03 | -0.000 |

| | R PX FT | R PY FT | R PZ FT | V PX FT/SEC | V PY FT/SEC | V PZ FT/SEC | TIME SEC |
|--------|------------|------------|------------|----------------|----------------|----------------|-------------|
| SFSVX | -0.00003 | 17280. | -15157. | 252. | -18.62 | -21.17 | -0.44 |
| SFSVY | -0.00003 | -17618. | -15420. | -259. | 18.94 | 21.58 | -0.008 |
| SFSVZ | -0.00003 | 1959. | -2008. | 40. | -2.18 | -2.88 | 0.45 |
| SFSVZ | -0.00003 | -208. | 2111. | -42. | 2.31 | 3.03 | 0.005 |
| ABSVX | -0.00003 | -15. | 14. | -0. | 0.02 | 0.02 | -0.005 |
| ABSVX | -0.00003 | 18. | -14296. | 0. | -0.02 | -0.02 | 0. |
| ABSVX | -0.00003 | 16333. | -14296. | 222. | -17.53 | -19.95 | 0.001 |
| ABSVY | -0.00003 | -16538. | 14443. | -336. | 17.71 | 20.20 | 0.001 |
| ABSVY | -0.00003 | -1067. | 447. | -20. | 0.84 | 0.31 | 0.001 |
| ABSVZ | -0.00003 | 957. | -355. | 18. | -0.73 | -0.18 | 0.001 |
| ABSVZ | -0.00003 | 222. | -191. | -337. | -0.22 | -0.27 | 0.001 |
| CHT1X | -0.00003 | -249. | 207. | 237. | 0.24 | 0.29 | 0.047 |
| CHT1Y | -0.00003 | -119. | 103. | 234. | 0.12 | 0.15 | 0.047 |
| CHT1Y | -0.00196 | 102. | -88. | -234. | -0.10 | -0.12 | 0.047 |
| CHT1Z | -0.00196 | 925. | -715. | -1312. | -0.83 | -1.01 | 0.047 |
| CHT1Z | -0.00573 | -849. | 727. | 1312. | 0.85 | 1.02 | 0.047 |
| EPSVXZ | -0.00196 | 7820. | -6305. | -6347. | -8.12 | -8.47 | 0.047 |
| EPSVYX | -0.00196 | -7875. | -7875. | -160. | 6.17 | 8.53 | 0.047 |
| EPSVYX | -0.00834 | -17. | 14. | -16. | 0.02 | 0.02 | 0.001 |
| EPSVYX | -0.00834 | -31. | 27. | -21. | 0.03 | 0.04 | 0.001 |
| EPSVYX | -0.00293 | -15395. | 13613. | -215. | 16.63 | 19.13 | 0.001 |
| EPSVYZ | -0.00393 | 15323. | -13579. | -314. | -16.59 | -19.05 | 0.014 |
| EPSVYZ | -0.00834 | -28. | 24. | -2. | 0. | 0.03 | -0.015 |
| FPSVYX | -0.00278 | -369. | -554. | -5. | 0. | 0.00 | -0.000 |
| FPSVYX | -0.00278 | -196. | 704. | 2. | 0.26 | 1.53 | -0.006 |
| FPSVZY | -0.00879 | 601. | -518. | -1047. | -0.61 | -0.73 | 0.004 |
| FPSVZY | -0.00879 | -599. | 515. | 1047. | 0.61 | 0.72 | -0.000 |
| FPSVZX | -0.00834 | -1293. | 1109. | 1904. | 1.30 | 1.56 | -0.000 |
| FPSVZX | -0.00834 | 1228. | -1052. | -1906. | -1.23 | -1.48 | -0.000 |
| RSS | | 40883. | 32746. | 42.42 | 45.63 | 5.35 | 0.060 |

TABLE 24

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UNCERTAINTIES AT S-IVB REIGNITION
DUE TO PLATFORM ERRORS

| | ERNX FT | ERNY FT | ERNZ FT | EVNX FT/SEC | EVNY FT/SEC | EVNZ FT/SEC |
|-------|------------|------------|------------|----------------|----------------|----------------|
| GDSVX | -100 | 184. | -158. | -361. | -0.19 | -0.22 |
| GNSVY | -075 | -168. | 145. | 361. | 0.17 | 0.21 |
| GDSVZ | -075 | -924. | 789. | 1358. | 0.91 | 0.20 |
| GDSVZ | -075 | 932. | -795. | -1358. | 1.11 | 2.48 |
| USSVX | -075 | -16578. | 12757. | -332. | -0.92 | -1.12 |
| USSVZ | -075 | 16529. | -12776. | 333. | 16.54 | -7.48 |
| USSVX | -100 | 152. | -130. | -325. | -16.56 | 0.40 |
| USSVY | -100 | -199. | 171. | -0.15 | -16.34 | -0.40 |
| USSVY | -075 | -905. | 775. | 1235. | -0.18 | -0.18 |
| USSVZ | -075 | 729. | -623. | -1238. | 0.21 | 0.24 |
| USSVZ | -100 | 20. | -17. | 0. | 0.91 | 0.18 |
| UISVX | -100 | -5. | 4. | -0. | -0.02 | -0.02 |
| UISVX | -100 | -17. | 15. | -0. | 0.01 | 0.01 |
| UISVY | -100 | 38. | -33. | 1. | 0.02 | 0.02 |
| UISVY | -075 | 42. | -36. | 1. | -0.04 | -0.05 |
| UISVZ | -075 | 15. | -12. | 0. | -0.04 | -0.05 |
| UISVZ | -075 | -18221. | 13888. | -364. | 1.9.03 | -0.05 |
| UISVX | -060 | 162. | -140. | -302. | -0.16 | -0.20 |
| USSVY | -060 | -127. | 108. | 303. | 0.13 | -0.26 |
| USSVY | -060 | -893. | 763. | 1261. | 0.89 | 0.26 |
| USSVZ | -060 | 882. | -753. | -1261. | -0.88 | 2.33 |
| USSVZ | -060 | -12953. | 10078. | -261. | 1.3.16 | -1.06 |
| SSVX | -050 | -12745. | -9884. | 257. | -12.92 | -2.33 |
| SSVY | -050 | -9. | 8. | -0. | 0.01 | -0.01 |
| SSVY | -050 | 51. | -46. | 1. | -0.05 | -0.05 |
| SSVZ | -050 | 20. | -17. | 1. | -0.02 | -0.02 |
| SSVZ | -050 | 23. | -29. | 1. | -0.04 | -0.04 |
| SSVZ | -050 | 17. | -11. | 0. | -0.01 | -0.01 |
| SSVZ | -050 | 26. | -22. | 1. | -0.03 | -0.03 |

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| | ERNX FT | ERNZ FT | EVNY FT/SEC | EVNZ FT/SEC | EVNX FT/SEC | EVNY FT/SEC | EVNZ FT/SEC |
|---------|------------|------------|----------------|----------------|----------------|----------------|----------------|
| SFSVX | • 000003 | -1 7227. | 15110. | -351. | 18.57 | 21.11 | 0.44 |
| SFSVY | -• 000003 | 1 7557. | -15369. | 358. | -18.88 | -21.51 | -0.45 |
| SFSVZ | • 000003 | -1 941. | -1992. | -39. | 2.16 | 2.86 | 0.05 |
| SFSVZ | -• 000003 | 2 064. | -2098. | 42. | -2.29 | -2.01 | -0.06 |
| SFSVZ | • 000003 | 16. | -14. | 0. | -0.02 | -0.02 | -0.00 |
| ABSVX | -• 000003 | -1 6222. | -14253. | -231. | 0.02 | 0.02 | 0.00 |
| ABSVY | • 000003 | 1 6419. | -14399. | 335. | 17.85 | 19.91 | 0.41 |
| ABSVZ | -• 000003 | 1 083. | -397. | 21. | -0.84 | 0.06 | -0.02 |
| ABSVZ | • 000003 | -980. | 308. | -19. | 0.73 | -0.18 | 0.02 |
| ABSVZ | -• 000003 | -221. | 190. | 400. | 0.22 | 0.27 | 0.87 |
| ABSVZ | • 000003 | 242. | -207. | -400. | -0.24 | -0.29 | -0.87 |
| CH11X | • 001 96 | 11.9. | -103. | -233. | -0.12 | 0.14 | -0.19 |
| CH11Y | -• 001 96 | -111. | 96. | 234. | 0.11 | 0.14 | 0.19 |
| CH11Z | • 00573 | -843. | 722. | 1313. | 0.84 | 1.02 | 1.89 |
| CH11Z | -• 00573 | 850. | -729. | -1312. | -0.85 | -1.03 | -1.89 |
| EP SVXZ | • 000824 | 7815. | 6300. | -158. | 8.12 | 8.46 | 0.19 |
| EP SVXY | -• 000834 | 7872. | -6345. | 160. | -8.17 | -8.52 | -0.20 |
| EP SVYZ | • 000834 | 17. | -15. | 0. | -0.02 | -0.02 | -0.00 |
| EP SVXY | -• 000834 | 31. | -26. | 1. | -0.03 | -0.04 | -0.00 |
| EP SVYX | • 00393 | 15329. | -13557. | 314. | -16.56 | -19.05 | -0.19 |
| EP SVYX | -• 00393 | -15266. | 13527. | -312. | 16.53 | 18.98 | 0.29 |
| EP SVYZ | • 000834 | 30. | -25. | 1. | -0.02 | -0.02 | -0.00 |
| EP SVYZ | -• 000834 | 7. | -2. | 0. | -0.00 | -0.00 | -0.00 |
| EP SVYX | • 00278 | 400. | 527. | 5. | 0.05 | 1.29 | -0.00 |
| EP SVYX | -• 00278 | -224. | -683. | -2. | -0.24 | -1.50 | -0.00 |
| EP SVZY | • 00879 | -610. | 526. | 1045. | 0.62 | 0.74 | 0.86 |
| EP SVZY | -• 00879 | 598. | -515. | -1045. | -0.61 | -0.73 | -0.86 |
| EP SVZX | • 00834 | 1294. | -1109. | -1908. | -1.30 | -1.56 | -2.75 |
| EP SVZX | -• 00834 | -1227. | 1051. | 1910. | 1.23 | 1.48 | 2.75 |
| RSS | | 40782. | 33679. | 3557. | 42.50 | 45.54 | 5.41 |

TABLE 25

ACTUAL DEVIATIONS AT S-IVB REIGNITION
DUE TO PERFORMANCE ERRORS

| | R FT | V FT/SEC | BFTA E-3 DEG | INCL E-3 DEG | NODE E-2 DEG | PHIT E-3 NEG |
|--------|---------|-------------|-----------------|-----------------|-----------------|-----------------|
| FISP* | 0.416 | -99. | 0.02 | -0.1 | -0.4 | 10. |
| EDWGT1 | -0.416 | 101. | -0.02 | 0.1 | 0.4 | -24.0 |
| EDWGT1 | 0.716 | -52. | 0.02 | -0.0 | -0.7 | 7.8 |
| FM* | -0.716 | 34. | 0.00 | 0.0 | 0.2 | -6.2 |
| FM* | 0.895 | 145. | -C.C3 | 0.1 | C.6 | -34.1 |
| FFUFL1 | -0.895 | 218. | -C.C4 | 0.2 | C.8 | -56.4 |
| FFUFL1 | 0.8 | -75. | 0.02 | -0.1 | -0.0 | 0.2 |
| EWGT1 | -0.5 | 37. | -0.00 | 0.1 | 0.2 | -18.0 |
| EWGT1 | 2.846 | 84. | -0.02 | 0.1 | 0.2 | -15.6 |
| FCN | 1.00 | -81. | 0.02 | -0.0 | -0.2 | -8.2 |
| FRHQA | -1.00 | 38. | -0.01 | 0.0 | 0.2 | 7.7 |
| FRHQA | 1.00 | -36. | 0.01 | -0.0 | -0.1 | -7.2 |
| FISP2 | 1.00 | 36. | -0.00 | 0.0 | -0.2 | 6.7 |
| FISP2 | -1.00 | -34. | 0.01 | -0.0 | -0.0 | 18.8 |
| EDWGT2 | 0.427 | -101. | 0.07 | -0.1 | -0.5 | -23.4 |
| EDWGT2 | -0.427 | 106. | -0.07 | 0.1 | 0.5 | 9.9 |
| FFUFL2 | 1.034 | -52. | 0.02 | -0.1 | -0.6 | -14.7 |
| EM2 | -1.034 | 76. | -0.02 | 0.2 | 0.7 | 6.4 |
| EM2 | 0.855 | -42. | C.C2 | -C.1 | 0.1 | -10.2 |
| EM2 | -0.895 | 65. | -0.03 | 0.1 | 0.0 | 18.5 |
| FFUFL2 | 0.5 | -19. | 0.01 | 0.0 | 0.0 | -7.0 |
| EWGT2 | 2.402 | 18. | -0.01 | 0.0 | 0.0 | 8.8 |
| EWGT2 | -2.402 | 96. | -0.01 | 0.1 | 0.0 | -9.6 |
| FISP2 | 0.029 | -97. | 0.02 | -0.1 | -0.6 | 22.8 |
| FISP2 | -0.929 | -44. | 0.01 | -0.0 | -0.0 | -27.5 |
| EDWGT3 | 2.0 | 45. | -0.01 | 0.0 | 0.0 | 20.6 |
| EM2 | 2.0 | 2. | -0.01 | 0.1 | 0.0 | -0.7 |
| EM2 | -2.0 | -4. | 0.01 | -0.0 | -0.0 | 0.9 |
| | | -9. | C.C1 | 0.0 | 0.0 | -30.1 |

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| | R FT | V FT/SFC | BFTA E-2 CFG | INCL E-2 DEG | NODE E-3 DEG | PHI T E-3 NEG |
|---------|---------|-------------|-----------------|-----------------|-----------------|------------------|
| FFUJF13 | -1.0 | 0.01 | 0.0 | 0.0 | 0.7 | -25.6 |
| FHG72 | 1.926 | -0.02 | -0.0 | -0.0 | -0.5 | 19.4 |
| F40FF1 | -1.926 | C.01 | C.C | 0.0 | C.7 | -26.5 |
| F40FF2 | 0.02 | -C.C2 | -U.0 | -0.0 | -C.5 | 19.2 |
| F40FF3 | -0.02 | 50. | 0.64 | 0.9 | 0.1 | 0.4 |
| F40FF4 | 0.02 | -50. | -0.64 | -0.9 | -0.1 | -C.7 |
| FULAGE | -0.02 | 0. | 0. | 0. | 0. | 0. |
| FVFNTR | 20.0 | 0.02 | 0.29 | 0.4 | 0.0 | C.? |
| PSS | -20.0 | 3745. | -2.14 | -0.4 | -0.0 | 0.? |
| | 3755. | 2.25 | 2.13 | -0.7 | -0.4 | -93.9 |
| | | | | | | 93.9 |
| | | | | C.1 | 2.3 | 135.5 |

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TABLE 26

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ACTUAL DEVIATIONS AT S-IVB REIGNITION
DUE TO PERFORMANCE ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | Vpz FT/SEC | TIME SEC |
|--------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| FISP1 | 0.419 | -4.747 | 1.270 | -5.55 | -6.52 | -0.06 | -1.027 |
| FDWGT1 | -0.419 | 5.937 | -1.540 | 6.96 | 8.18 | 0.00 | 0.980 |
| FM1 | 0.716 | 2.040 | -1.952 | -2.26 | -2.58 | -0.02 | -0.865 |
| FWGTT1 | -0.714 | -2.622 | 2.995 | -70. | 2.14 | -0.01 | 0.915 |
| FM2 | 0.895 | -9.653 | 8.436 | -220. | 9.88 | 11.62 | 1.333 |
| FFUFL1 | -0.895 | -15.958 | 13.946 | -354. | 16.36 | 19.24 | 0.26 |
| FCN | 0.5 | 2.622 | -2.340 | 57. | -2.70 | -3.92 | 1.620 |
| FWGTT2 | -0.5 | -2.813 | 2.853 | -66. | 2.89 | 3.39 | -0.091 |
| FRHIA | 0.0 | -5.746 | 4.678 | -125. | 5.48 | 6.44 | 0.086 |
| FFUFL2 | -0.0 | -2.6846 | 4.411 | -3.877 | -6.62 | -5.22 | 0.830 |
| FCN | 1.0 | -2.315 | 2.029 | -55. | 2.37 | 2.79 | -0.858 |
| FRHIA | -1.0 | 2.176 | -1.908 | 45. | -2.23 | -2.62 | 0.382 |
| FISP2 | 0.0 | -2.041 | 1.791 | -50. | 2.10 | 2.46 | -0.382 |
| FDWGT2 | -1.0 | 1.983 | -1.554 | 39. | -1.93 | -2.27 | -0.315 |
| FM2 | 0.427 | 5.321 | -4.682 | -4.682 | -5.47 | -6.44 | -0.714 |
| FWGTT2 | -0.427 | -5.528 | 5.901 | -1.54. | 6.79 | 8.00 | 0.663 |
| FFUFL2 | 1.0 | 2.908 | -2.469 | -2.86. | -2.91 | -3.42 | 0.300 |
| FCN | -1.0 | -1.74 | -4.164 | 3.558 | -1.71 | 4.21 | -2.61 |
| FRHIA | 0.895 | 1.792 | -1.587 | 29. | -1.85 | -2.20 | -0.714 |
| FFUFL3 | -0.895 | -2.887 | 2.552 | -58. | 2.99 | 3.54 | -1.043 |
| FCN | 0.5 | 0.74 | -2.469 | -7.30. | -1.10 | -0.84 | -0.65 |
| FWGTT3 | -0.5 | -1.74 | -4.164 | 3.558 | -1.18 | 0.83 | 0.945 |
| FM3 | 0.895 | 1.792 | -1.587 | 29. | -1.85 | -2.20 | -0.923 |
| FFUFL4 | 0.5 | 0.74 | -2.469 | -7.30. | -1.10 | -0.84 | 0.673 |
| FWGTT4 | -0.5 | -1.74 | -4.164 | 3.558 | -1.18 | 0.83 | -0.670 |
| FISP3 | 0.402 | -51.71 | 53.99 | -4570. | 4.33 | 7.44 | -0.07 |
| FDWGT3 | -0.402 | -2.407 | 5.37. | -1.7. | -5.28 | -6.21 | -0.07 |
| FM4 | 0.929 | -0.929 | 2.494 | -71.90 | 5.6. | -2.0. | -0.04 |
| FWGTT5 | -0.929 | -2.725 | 2.389 | -72.5. | 6.8. | 2.80 | -0.04 |
| FFUFL5 | 0.0 | 6.910 | -5.920 | 1.81. | 6.92 | -8.09 | 0.08 |
| FCN | -2.0 | -1.079 | 9.57. | -2.67. | 10.89 | 12.74 | 0.05 |
| FRHIA | 2.0 | 5.899 | -5.032 | -50.32. | 1.52. | -6.00 | -0.150 |
| FFUFL6 | -2.0 | -8.617 | 7.350 | -214. | 8.74 | 10.22 | -0.12 |

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| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SEC | TIME SEC |
|--------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| FFUF13 | 1.0 | -7221. | 5211. | -180. | 7.41 | 8.66 | 0.577 |
| FHCF12 | -1.0 | 5297. | -4479. | 137. | -5.16 | -6.25 | -0.675 |
| FHCF11 | 1.0 | -7594. | 6441. | -186. | 7.69 | 8.98 | C. C5 |
| FLAGF1 | 0.03 | 5519. | -4672. | 137. | -5.59 | -6.52 | C. 551 |
| FAGFF2 | -0.03 | 145. | -58. | -7. | 0.62 | -C. 649 | -C. C3 |
| FAGFF3 | 0.03 | -131. | 47. | 3. | -0.64 | 0.74 | 0.874 |
| FULAGF | -0.03 | 0. | 0. | 0. | 0. | 0. | -0.877 |
| FVFNTR | 5.0 | 80. | -41. | 1. | 0.27 | -0.12 | 0.00 |
| | -5.0 | 45. | -67. | 1. | -0.40 | -0.02 | 0.056 |
| | 20.0 | -26449. | 25782. | -475. | 25.77 | 13.63 | -C. C1 |
| | -20.0 | 24388. | -25800. | 472. | -25.81 | 0.64 | -0.049 |
| PSS | | 37CC1. | 35252. | 81C. | 38.34 | 47.22 | 0.73 |
| | | | | | | | 4.238 |

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TABLE 27

**UNCERTAINTIES AT S-IVB REIGNITION
DUE TO PERFORMANCE ERRORS**

| | FVNX FT | FRNY FT | ERNZ FT | EVNX FT/SEC | FVNZ FT/SEC |
|--------|------------|------------|------------|----------------|----------------|
| FISP1 | 0.419 | -737. | 764. | -14. | 0.78 |
| FDWGT1 | -0.419 | 745. | -776. | -0.79 | -1.01 |
| FDWGT1 | 0.716 | -445. | 453. | 0.47 | -0.61 |
| FM- | -0.716 | 277. | -281. | -0.29 | -0.37 |
| FM- | 0.895 | 984. | -1034. | -1.04 | -1.36 |
| FM- | -0.895 | 1599. | -1646. | -1.68 | -2.15 |
| FFUFL1 | 0.895 | -538. | 557. | 0.58 | 0.75 |
| FWGTL1 | -0.5 | 180. | -197. | -0.19 | -0.25 |
| FWGTL1 | 2.846 | 557. | -586. | -0.59 | -0.77 |
| FCN | -2.846 | -486. | 522. | 0.51 | 0.67 |
| FCN | 10.0 | 170. | -197. | -0.18 | -0.25 |
| FRHAA | -10.0 | -236. | 249. | -0.25 | 0.32 |
| FRHAA | 10.0 | 301. | -306. | -0.32 | -0.41 |
| FRHAA | -10.0 | -251. | 262. | 0.26 | 0.34 |
| FISP2 | 0.497 | -649. | 687. | -12. | 0.69 |
| FDWGT2 | -0.497 | 654. | -698. | -13. | -0.70 |
| FDWGT2 | 1.34 | -351. | 367. | -7. | 0.37 |
| FM? | -1.34 | 679. | -680. | 12. | -0.72 |
| FM? | 0.895 | -133. | 157. | -2. | 0.14 |
| FM? | -0.895 | 419. | -433. | 9. | -0.45 |
| FFUFL2 | 0.5 | -144. | 144. | -3. | 0.15 |
| FWGTL2 | -0.5 | 13. | -34. | 0. | -0.02 |
| FWGTL2 | 2.407 | 642. | -678. | 12. | -0.69 |
| FWGTL2 | -2.407 | -716. | 744. | 0.76 | 0.97 |
| FISP2 | 0.929 | -299. | 305. | -6. | 0.20 |
| FDWGT2 | -0.929 | 218. | -244. | 4. | -0.22 |
| FDWGT2 | 2.0 | -62. | 55. | -1. | 0.06 |
| FM2 | -2.0 | 43. | -29. | 1. | -0.04 |
| FM2 | 2.0 | 5. | -10. | 0. | -0.01 |
| FM2 | -2.0 | -33. | 34. | -1. | 0.04 |

| | FVNX FT | FVNY FT | FVN7 FT | FVN7 FT/SFC | FVN7 FT/SEC |
|---------|------------|------------|------------|----------------|----------------|
| FFUEFL3 | 1.0 | 175. | -2. | 0.17 | 0.22 |
| FWGT2 | -1.0 | -230. | -4. | -0.23 | -0.11 |
| | 1.936 | -166. | -3. | 0.18 | 0.23 |
| | -1.936 | 162. | 3. | -0.17 | -0.23 |
| F4AFF1 | 0.C7 | 6. | -4. | -0.01 | -0.01 |
| F4AFF2 | 0.02 | -18. | 12. | 0.01 | 0.02 |
| | -0.02 | 0. | -0. | -0. | -0. |
| | 0.02 | 0. | 0. | -0. | -0. |
| | -0.02 | 0. | -0. | -0. | -0. |
| FULAGE | 5.0 | -19. | 16. | -0. | 0.04 |
| | -5.0 | -96. | 81. | -2. | 0.12 |
| FVFNT2 | 20.0 | 24450. | -25782. | 475. | -25.76 |
| | -20.0 | -24190. | 25800. | -473. | -25.80 |
| PSS | 24569. | 25920. | 477. | 25.93 | 33.68 |
| | | | | | 0.64 |

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TABLE 28
COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT S-IVB REIGNITION

| R | V | BETA | INCL | NODE | PHIT | FUEL |
|----------|-----------|-----------|-----------|-----------|----------|----------|
| 1.43E 03 | -0.8 | 0.6 | -0.0 | -0.0 | -0.3 | -0.1 |
| V | 1.42E 00 | -0.7 | -0.0 | -0.0 | -0.2 | 0.0 |
| BETA | -2.50E-03 | 2.58E-03 | -0.0 | -0.0 | 0.1 | -0.0 |
| INCL | -1.79E-05 | -2.52E-07 | 2.20E-03 | 1.0 | 0.0 | -0.0 |
| NODE | -3.90E-06 | -9.25E-07 | 1.76E-05 | 8.29E-03 | -0.0 | -0.0 |
| PHIT | -2.07E-02 | 1.58E-05 | 4.37E-06 | -5.55E-06 | 6.10E-07 | 0.3 |
| FUEL | 2.50E 01 | -1.23E-01 | -1.65E-02 | -4.35E-01 | 2.05E 01 | 1.29E 03 |

TABLE 29

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT S-IVB REIGNITION

| | R _{PX} | R _{PY} | R _{PZ} | V _{PX} | V _{PY} | V _{PZ} | TIME |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------|
| R _{PX} | 1.72E 04 | -1.0 | 0.3 | -1.0 | -1.0 | -0.3 | -0.2 |
| R _{PY} | -2.61E 08 | 1.53E 04 | -0.3 | 1.0 | 1.0 | 0.3 | 0.2 |
| R _{PZ} | 5.22E 06 | -4.62E 06 | 1.20E 03 | -0.3 | -0.2 | 0.8 | -0.1 |
| V _{PX} | -3.07E 05 | 2.72E 05 | -5.45E 03 | 1.79E 01 | 1.0 | 0.3 | 0.2 |
| V _{PY} | -3.49E 05 | 3.12E 05 | -6.13E 03 | 3.64E 02 | 2.05E 01 | 0.3 | 0.2 |
| V _{PZ} | -7.95E 03 | 7.02E 03 | 1.84E 03 | 8.23E 00 | 9.44E 00 | 1.80E 00 | 0.0 |
| TIME | -5.11E 03 | 4.47E 03 | -1.28E 02 | 5.32E 00 | 6.16E 00 | 2.24E-02 | 1.28E 00 |

TABLE 30

COVARIANCE MATRIX OF UNCERTAINTIES
AT S-IVB REIGNITION

| | ERNX | ERNY | ERNZ | EVNX | EVNY | EVNZ |
|------|------------|------------|------------|-----------|-----------|-----------|
| ERNX | 1.058E 04 | -1.0 | 0.2 | -1.0 | -1.0 | -0.3 |
| ERNY | -2.021E 08 | 1.041E 04 | -0.2 | 1.0 | 1.0 | 0.3 |
| ERNZ | 4.008E 06 | -3.064E 06 | 1.020E 03 | -0.2 | -0.2 | 0.9 |
| EVNX | -2.060E 05 | 2.031E 05 | -4.031E 03 | 1.065E 01 | 1.0 | 0.3 |
| EVNY | -2.093E 05 | 2.064E 05 | -4.078E 03 | 3.008E 02 | 1.088E 01 | 0.3 |
| EVNZ | -7.062E 03 | 6.073E 03 | 1.087E 03 | 7.091E 00 | 9.005E 00 | 1.081E 00 |

TABLE 2
ERRORS AT WAITING ORBIT INSERTION
DUE TO PLATFORM ERRORS

| | ER FT | FV FT/SEC | EBETA E-3 DFG | FINCL E-1 DFG | ENODE E-2 DEG |
|-------|-----------------|-----------------|------------------|------------------|------------------|
| GDSVX | • 100 -• 100 | 1341. -1347. | -15.18 15.17 | 20.00 -20.00 | -7.8 7.8 |
| GDSVY | • 075 -• 075 | -1975. 1952. | -6.71 6.63 | -25.3 24.9 | -11.9 12.0 |
| GDSVZ | • 075 -• 075 | 2518. -2555. | -32.31 23.16 | 41.7 -42.1 | -8.4 8.4 |
| USSVX | • 100 -• 100 | 98. -99. | -1.12 1.11 | -1.4 -1.4 | -14.1 -14.1 |
| USSVY | • 075 -• 075 | -56. 44. | -0.40 0.26 | -0.0 -0.1 | -0.9 -2.8 |
| USSVZ | • 100 -• 100 | -8. 10. | 0.13 -0.12 | -0.3 0.3 | 0.0 0.0 |
| UTSVX | • 100 -• 100 | 5. -4. | 0.07 -0.07 | -0.1 -0.1 | -0.1 -0.1 |
| UTSVY | • 075 -• 075 | 6. -7. | -0.05 -0.07 | 0.1 -0.1 | 0.1 -0.1 |
| UTSVZ | • 075 -• 075 | 2033. -2036. | -10.41 -10.41 | 12.9 -12.9 | -7.8 7.8 |
| UASVX | • 060 -• 060 | 22. -22. | -0.23 0.24 | 0.2 -0.2 | -0.9 0.9 |
| UASVY | • 060 -• 060 | -106. 102. | -0.53 0.53 | -0.7 0.7 | 2.3 -2.3 |
| UASVZ | • 060 -• 060 | 1081. -1097. | -6.51 6.35 | 1.0 -1.0 | -5.6 5.5 |
| SSVX | • 050 -• 050 | 4. -1. | 0.02 0.01 | -0.0 0.0 | -0.8 -0.8 |
| SSVY | • 050 -• 050 | 2. 0. | 0.01 0.01 | 0.0 -0.0 | -0.1 -0.1 |
| SSVZ | • 050 -• 050 | -3. 3. | 0.35 -0.35 | -0.1 0.1 | -0.0 0.0 |

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| | FR FT | EV FT/SEC | EFFECTA F-3 DEG | EINCL F-3 DEG | ENCLDE E-3 DEG |
|--------|-----------|--------------|--------------------|------------------|-------------------|
| SFSVX | • 000003 | -6.85 | 5.5 | -7.9 | -0.5 |
| SFSVY | -• 000003 | -6.98 | -5.6 | 8.1 | 0.5 |
| SFSVZ | -• 000003 | -0.58 | 0.6 | -1.0 | -0.2 |
| SFSVZ | • 000003 | 0.63 | -0.6 | 1.0 | 0.7 |
| ABSVX | -• 000003 | -0.00 | -0.0 | 0.1 | -0.4 |
| ABSVY | -• 000003 | -0.01 | 0.0 | -0.1 | 0.4 |
| ABSVZ | -• 000003 | -6.73 | 4.3 | -7.5 | -0.4 |
| ABSVZ | • 000003 | 5.88 | 6.80 | -4.4 | -0.5 |
| CH11X | • 000196 | -1.17 | -1.6 | 7.6 | 0.3 |
| CH11Y | -• 000196 | -1.12 | 1.5 | -0.3 | 0.5 |
| CH11Z | -• 000573 | -3.90 | 0.04 | 0.3 | 3.8 |
| EPSVXZ | -• 000003 | -2.0 | -0.02 | -0.3 | -1.0 |
| EPSVYX | -• 000003 | -0.05 | -0.05 | -0.0 | -0.4 |
| EPSVYZ | -• 000003 | -0.06 | 0.0 | 0.6 | 0.4 |
| EPSVYX | -• 000573 | -0.31 | 0.2 | 3.0 | 8.6 |
| EPSVYX | -• 000573 | -4.0 | 0.32 | -0.2 | -8.6 |
| EPSVYX | -• 000196 | 3.90 | -3.59 | 3.6 | 0.2 |
| EPSVYX | -• 000196 | -3.88 | 2.62 | -3.6 | -0.2 |
| EPSVYX | -• 000834 | 6.9 | 0.37 | 0.9 | -0.1 |
| EPSVYX | -• 000834 | -6.9 | -0.35 | -0.9 | 0.1 |
| EPSVYX | -• 000393 | 54.9 | 5.86 | -5.0 | 0.5 |
| EPSVYX | -• 000393 | -54.6 | -5.83 | 5.0 | -7.1 |
| EPSVYX | -• 000834 | -33. | 0.41 | -0.5 | -0.5 |
| EPSVYX | -• 000834 | 25. | -0.39 | 0.5 | -0.2 |
| EPSVYX | -• 000278 | -934. | 1.02 | -1.6 | -0.1 |
| EPSVYX | -• 000278 | 940. | -0.95 | 1.6 | -0.6 |
| EPSVZY | -• 000834 | 1. | -0.18 | 0.6 | 0.6 |
| EPSVZY | -• 000834 | 1. | 0.18 | -0.6 | 2.8 |
| EPSVZX | -• 000834 | -1.0 | 0.12 | -1.2 | -2.8 |
| EPSVZX | -• 000834 | 13. | -0.09 | 1.2 | -4.4 |
| RSS | | 4474. | 41.03 | 55.9 | 141.6 |

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TABLE 32

ACTUAL DEVIATIONS AT WAITING ORBIT INSERTION
DUE TO PLATFORM ERRORS

| | R FT | V FT/SEC | BETA F-2 DEG | INCL F-3 DEG | NODE F-3 DFG | P/HIT E-3 DEG | FUEL LBS |
|-------|---------|-------------|-----------------|-----------------|-----------------|------------------|-------------|
| GDSVX | -100 | 1333. | -15.17 | 20.0 | -7.8 | -7.7 | 0.5 |
| GDSVY | -100 | -1357. | 15.18 | -20.0 | 7.8 | -9.7 | 0.7 |
| GDSVZ | -075 | -1990. | -6.70 | -25.3 | -11.9 | 138.4 | 0.9 |
| GDSVZ | -075 | 1924. | 6.63 | 24.9 | 12.0 | -138.5 | 1.2 |
| GDSVZ | -075 | 2503. | -33.30 | 41.7 | -8.4 | 14.0 | 1.5 |
| GDSVZ | -075 | -2572. | 33.17 | -42.1 | -4.4 | -14.1 | -36.5 |
| USSVX | -100 | 99. | -1.12 | 1.4 | -1.4 | 0.9 | -1.1 |
| USSVY | -100 | -98. | 1.11 | -1.4 | 1.4 | -0.9 | 1.2 |
| USSVY | -075 | -77. | -0.38 | -0.1 | 2.7 | 9.6 | 2.7 |
| USSVY | -075 | 79. | 0.28 | -0.1 | -2.8 | -9.7 | -2.5 |
| USSVZ | -100 | -8. | 0.13 | -0.3 | 0.0 | -0.1 | -0.0 |
| USSVZ | -100 | 4. | -0.12 | 0.3 | -0.0 | 0.1 | -0.1 |
| UISVX | -100 | -12. | 0.08 | -0.1 | 0.1 | -0.2 | 0.3 |
| UISVY | -100 | -7. | -0.05 | 0.1 | -0.0 | 0.2 | -0.1 |
| UISVY | -075 | 5. | 0.05 | 0.1 | 0.1 | -0.6 | -0.1 |
| UISVZ | -075 | -8. | -0.02 | -0.1 | -0.1 | 0.6 | -0.1 |
| UISVZ | -075 | 2033. | -10.41 | 12.9 | -7.8 | 1.8 | 52.9 |
| UISVZ | -060 | -2035. | 10.41 | -12.9 | 7.8 | -1.8 | -53.0 |
| UISVX | -060 | -33. | 0.25 | -0.2 | 0.9 | 0.4 | -0.1 |
| UISVY | -060 | -105. | -0.53 | -0.7 | 2.3 | 15.2 | 2.7 |
| UISVZ | -060 | 104. | 0.52 | 0.7 | -2.3 | -15.2 | -2.7 |
| SSVX | -060 | 1060. | -6.49 | 6.9 | -5.6 | 0.5 | 38.7 |
| SSVY | -060 | -1133. | 6.38 | -7.2 | 5.5 | -0.8 | -38.5 |
| SSVY | -050 | -8. | 0.02 | -0.1 | 0.0 | -0.1 | -0.0 |
| SSVZ | -050 | -2. | 0.00 | 0.0 | -0.0 | 0.1 | -0.2 |
| SSVZ | -050 | 2. | 0.01 | 0.0 | -0.1 | -0.1 | -0.0 |
| SSVZ | -050 | -0.5 | -0.01 | 0.0 | 0.0 | -0.1 | -0.0 |
| SSVZ | -050 | -1. | 0.05 | -1. | 0.0 | -0.1 | -0.1 |
| SSVZ | -050 | -0.03 | 0.1 | 0.0 | 0.0 | -0.1 | -0.1 |

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| | R FT | V FT/SEC | BFTA E-3 DFG | INCL E-3 DFG | NODE E-3 DEG | PHT E-3 DEG | FUEL LBS |
|--------|---------|-------------|-----------------|-----------------|-----------------|----------------|-------------|
| SFSVX | -000003 | -262. | -7.02 | 6.1 | -7.9 | -0.6 | 46.7 |
| SFSVY | -000003 | 264. | 7.16 | -5.2 | 8.1 | 0.6 | -4.3 |
| SFSVZ | -000003 | -242. | -0.64 | 0.8 | -1.0 | -0.2 | 0.8 |
| SFSVZ | -000003 | 250. | 0.69 | -0.8 | 1.0 | 0.2 | -1.2 |
| ABSVX | -000003 | -10. | 0.01 | -0.0 | 0.1 | -0.4 | -0.1 |
| ABSVX | -000003 | 11. | 0.00 | 0.0 | -0.1 | 0.4 | 0.7 |
| ABSVX | -000003 | -608. | -6.70 | 4.2 | -7.5 | 0.2 | -0.9 |
| ABSVY | -000003 | 612. | 6.78 | -4.3 | 7.6 | -0.4 | 21.4 |
| ABSVY | -000003 | -741. | 1.27 | -1.9 | 0.3 | -0.5 | -54.9 |
| ABSVZ | -000003 | 740. | -1.23 | 1.9 | -0.3 | 0.5 | -2.5 |
| ABSVZ | -000003 | 82. | -0.03 | 0.5 | 0.9 | 2.1 | -12.7 |
| CH11X | -000003 | -81. | 0.05 | -0.5 | -0.9 | -3.6 | -12.7 |
| CH11Y | -000196 | 7. | -0.05 | 0.0 | -0.6 | -0.4 | -6.6 |
| CH11Y | -000196 | -16. | 0.07 | 0.0 | 0.6 | 0.4 | -6.5 |
| CH11Y | -000573 | -45. | -0.30 | 0.2 | 3.0 | 8.6 | -0.0 |
| CH11Z | -000196 | 40. | 0.32 | -0.2 | -3.0 | -8.6 | -0.0 |
| CH11Z | -000196 | 407. | -3.61 | 3.7 | -3.4 | 0.2 | -24.5 |
| EPSVXZ | -000196 | -403. | 2.63 | -3.7 | 3.5 | -0.2 | -0.2 |
| EPSVYX | -000834 | 178. | 0.28 | 1.2 | 0.0 | -0.1 | -24.6 |
| EPSVYX | -000834 | -175. | -0.25 | -1.2 | 0.0 | 1.0 | -8.2 |
| EPSVYX | -000393 | 312. | 6.07 | -5.8 | 7.1 | 0.6 | -8.0 |
| EPSVYZ | -000393 | -311. | -6.04 | 5.7 | -7.1 | -0.6 | -1.8 |
| EPSVYZ | -000834 | -45. | 0.47 | -0.6 | 0.0 | -0.2 | -54.2 |
| EPSVYX | -000278 | 52. | -0.41 | 0.6 | -0.0 | 0.2 | -0.0 |
| EPSVYX | -000278 | -819. | 0.92 | -1.3 | -0.1 | -0.7 | -0.0 |
| EPSVZY | -000834 | -834. | -0.85 | 1.2 | 0.2 | 0.7 | -1.7 |
| EPSVZY | -000834 | 9. | -0.19 | 0.6 | 2.8 | 2.2 | -1.1 |
| EPSVZX | -000834 | -12. | 0.19 | -0.6 | -2.8 | -2.2 | -1.3 |
| EPSVZX | -000834 | -112. | 0.21 | -1.5 | -4.4 | -12.2 | -5.3 |
| RSS | -000834 | -118. | -0.18 | 1.5 | 4.4 | 12.2 | -7.6 |
| RSS | 4466. | 41.07 | 56.1 | 24.07 | 141.6 | 127.0 | 29.1 |

TARLF 22

ACTUAL DEVIATIONS AT WAITING ORBIT INSERTION
DUE TO PLATFORM ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SFC | VPY FT/SFC | Vpz FT/SEC | TIME SFC |
|-------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| GDSVX | * 100 | -85. | 3146. | 2419. | 0.79 | 21.46 | -0.001 |
| GDSVY | * 075 | -100 | -32. | -2390. | -0.71 | -21.47 | -0.002 |
| GDSVZ | * 075 | -075 | -1698. | -1081. | -17.66 | -1.07 | -0.001 |
| USSVX | * 100 | -100 | 1582. | 1181. | 7047. | 1.755 | -0.004 |
| USSVY | * 075 | -075 | 8741. | -11835. | 193. | -20.23 | -0.004 |
| USSVZ | * 075 | -075 | -9888. | 11952. | -172. | 20.15 | -0.004 |
| UISVX | * 100 | -100 | -85. | 394. | 497. | 0.25 | -0.001 |
| UISVY | * 075 | -075 | 120. | -458. | -497. | -0.32 | -0.000 |
| UISVZ | * 075 | -075 | 419. | -1013. | -1013. | -1.72 | -0.000 |
| USSVX | * 100 | -100 | -417. | 901. | 1929. | -1.72 | -0.002 |
| USSVY | * 100 | -100 | -10. | 1. | -0. | -0.04 | -0.001 |
| USSVZ | * 100 | -100 | -9. | 29. | 2. | 0.08 | -0.000 |
| UISVX | * 100 | -100 | -9. | -9. | 3. | 0.00 | -0.000 |
| UISVY | * 075 | -075 | -17. | 49. | -0. | 0.05 | -0.001 |
| UISVZ | * 075 | -075 | -17. | 49. | 15. | 0.14 | -0.001 |
| UISVZ | * 075 | -075 | -17. | 15. | -15. | -0.06 | -0.001 |
| UISVZ | * 075 | -075 | 11263. | -17913. | 202. | -22.77 | -0.001 |
| UISVZ | * 060 | -060 | -11291. | 17921. | -202. | 22.78 | -0.001 |
| UISVZ | * 060 | -060 | -131. | 280. | 406. | 0.28 | -0.000 |
| UISVZ | * 060 | -060 | 49. | -172. | -390. | -0.15 | -0.002 |
| UISVZ | * 060 | -060 | 411. | -1060. | -2210. | -2.24 | -0.001 |
| UISVZ | * 060 | -060 | -405. | 1043. | 2210. | 2.22 | -0.000 |
| SSVX | * 050 | -050 | 7844. | -13267. | 158. | -16.86 | -0.000 |
| SSVY | * 050 | -050 | -43. | 13158. | -119. | 0.01 | -0.006 |
| SSVZ | * 050 | -050 | -43. | 81. | 2. | 0.04 | -0.004 |
| SSVY | * 050 | -050 | -9. | 21. | 2. | 0.04 | -0.002 |
| SSVZ | * 050 | -050 | -1. | 29. | -3. | 0.04 | -0.002 |
| SSVZ | * 050 | -050 | -1. | 1. | -1. | -0.02 | -0.000 |
| SSVZ | * 050 | -050 | -25. | 25. | -1. | -0.09 | -0.000 |
| | | | | | | 0.07 | 0.10 |

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| | RPX | RPY | RPZ | VPX | VPY | VPZ | TIME SEC |
|---------|-----------|-----------|----------|--------|--------|--------|----------|
| SFSVX | • 00002 | 1 043 0. | -21 377. | 112. | -25.90 | -13.82 | -0.54 |
| SFSVY | -• 00003 | -1 064 6. | 21 754. | -114. | 26.35 | 14.09 | 0.55 |
| SFSVZ | • 00002 | 1 242. | -3012. | -8. | -2.35 | -2.15 | -0.06 |
| SFSVZ | -• 00002 | -1 297. | 3140. | 2. | 3.50 | 2.22 | 0.06 |
| SFSVZ | • 00003 | -33. | -33. | 44. | 19. | 0.05 | -0.008 |
| ABSVX | -• 00003 | 40. | -55. | -20. | 0.02 | 0.11 | -0.001 |
| ABSVX | • 00003 | 91 43. | -9579. | 195. | -0.06 | -0.04 | 0.02 |
| ABSVY | -• 00003 | -92 66. | 1 9789. | -197. | -24.25 | -12.77 | -0.52 |
| ABSVY | • 00003 | -11 06. | 552. | 41. | 24.50 | 12.92 | 0.52 |
| ABSVZ | -• 00003 | 1 044. | -429. | -42. | -0.92 | 0.83 | -0.032 |
| ABSVZ | • 00003 | 335. | -487. | -708. | -0.54 | -0.30 | -0.047 |
| ABSVZ | -• 00003 | -342. | 504. | 707. | 0.56 | 0.31 | 0.015 |
| CHILX | • 001 96 | -72. | 160. | 290. | 0.17 | 0.22 | -0.015 |
| CHILY | -• 001 96 | 46. | -128. | -787. | -0.13 | -0.21 | 0.07 |
| CHILY | • 00573 | 440. | -983. | -1936. | -1.53 | -0.66 | -0.001 |
| CHILZ | -• 00573 | -458. | 1007. | 1939. | 1.56 | 0.67 | -0.001 |
| CHILZ | • 001 96 | 473 0. | -8515. | 78. | -10.62 | -4.68 | -0.24 |
| EPSSVXZ | -• 001 96 | -4 759. | 8572. | -81. | 10.69 | 4.72 | 0.24 |
| EPSSVXZ | • 00834 | 242. | -284. | -48. | 0.25 | -0.15 | -0.000 |
| EPSSVYX | -• 00834 | -366. | 326. | 47. | -0.19 | 0.18 | -0.001 |
| EPSSVYX | • 00393 | -93 99. | 19387. | -75. | 23.16 | 12.68 | -0.018 |
| EPSSVYZ | -• 00393 | 93 54. | -19339. | 73. | -23.10 | -12.64 | -0.49 |
| EPSSVYZ | • 00834 | -47. | -6. | 5. | 0.07 | -0.51 | -0.018 |
| EPSVYX | -• 00834 | 46. | 27. | -8. | -0.04 | 0.51 | 0.002 |
| EPSVYX | • 00278 | -219. | -1389. | -51. | -1.03 | -2.18 | 0.00 |
| EPSVYZ | -• 00278 | 142. | 1577. | 45. | 1.26 | 2.30 | 0.00 |
| EPSVYZ | • 00879 | 384. | -749. | -1206. | -0.88 | -0.49 | -0.011 |
| EPSVYZ | -• 00879 | -386. | 747. | 1308. | 0.88 | 0.48 | -0.002 |
| EPSVZX | • 00834 | -1 037. | 1 821. | 2856. | 2.10 | 1.16 | 0.36 |
| EPSVZX | -• 00834 | 1 006. | -1 749. | -2859. | -2.01 | -1.12 | -0.017 |
| RSS | 24222. | 44562. | 8884. | 59.17 | 42.87 | 37.75 | 0.074 |

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TABLE F 24
UNCERTAINTIES AT WAITING ORBIT INSERTION
DUE TO PLATFORM ERRORS

| | ERNX FT | ERNY FT | ERNZ FT | EVNX FT/SFC | EVNY FT/SEC | EVNZ FT/SEC |
|-------|------------|------------|------------|----------------|----------------|----------------|
| GDSVX | • 100 | -3128. | -2416. | -0.76 | -21.46 | 0.86 |
| GDSVY | -• 100 | 3120. | 2394. | 0.74 | 21.44 | -1.07 |
| GDSVZ | • 075 | 1112. | 7025. | 17.69 | 1.09 | 27.17 |
| UDSVZ | -• 075 | -1134. | -7040. | -17.50 | -1.09 | -27.27 |
| UDSVX | • 075 | 11872. | -187. | 20.27 | -26.96 | 0.47 |
| UDSVY | -• 075 | 8837. | -11895. | -20.09 | 26.92 | -0.52 |
| UDSVZ | • 100 | 88. | -395. | -0.25 | -1.78 | 0.19 |
| UDSVX | -• 100 | -110. | 447. | 496. | 0.31 | -0.19 |
| UDSVY | • 075 | -468. | 1066. | 1914. | 1.78 | 0.71 |
| UDSVZ | -• 075 | 390. | -872. | -1924. | -1.44 | -2.32 |
| UDSVX | • 100 | 11. | -3. | 0. | 0.04 | -2.36 |
| UDSVY | -• 100 | 7. | -25. | -2. | -0.08 | -0.00 |
| UDSVZ | • 100 | -6. | 25. | -0. | 0.02 | 0.00 |
| UDSVX | -• 100 | 29. | -62. | -2. | -0.06 | -0.14 |
| UDSVY | • 075 | 18. | -50. | -15. | -0.14 | -0.03 |
| UDSVZ | -• 075 | 19. | -19. | 15. | 0.06 | -0.01 |
| UDSVX | • 075 | -11261. | 17911. | -202. | 22.77 | 6.40 |
| UDSVY | -• 075 | 11292. | -17923. | 202. | -22.78 | -6.43 |
| UDSVZ | • 060 | 98. | -245. | -401. | -0.24 | -0.51 |
| UDSVX | -• 060 | -72. | 197. | 394. | 0.18 | 0.47 |
| UDSVY | • 060 | -409. | 1057. | 2210. | 2.24 | 0.71 |
| UDSVZ | -• 060 | 407. | -1046. | -2211. | -2.23 | -0.70 |
| UDSVX | • 060 | -7897. | 13325. | -149. | 16.92 | 6.42 |
| UDSVY | -• 060 | 7787. | -13053. | 136. | -16.49 | -6.26 |
| UDSVZ | • 050 | -4. | 12. | -1. | 0.01 | 0.05 |
| UDSVX | -• 050 | 31. | -68. | 0. | -0.08 | -0.08 |
| UDSVY | • 050 | 10. | -23. | -2. | -0.04 | -0.01 |
| UDSVZ | -• 050 | 21. | -40. | 3. | -0.04 | -0.03 |
| UDSVX | • 050 | 2. | -2. | 1. | 0.02 | 0.08 |
| UDSVY | -• 050 | 22. | -45. | -1. | -0.08 | -0.11 |
| UDSVZ | • 050 | - | - | - | - | -0.00 |

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| | ERNX FT | ERNY FT | ERNZ FT | EVNX FT/SEC | EVNY FT/SEC | EVNZ FT/SEC | EVN2 FT/SEC |
|---------|------------|------------|------------|----------------|----------------|----------------|----------------|
| SFSVX | • 000007 | -9926. | -184. | 25.31 | 13.51 | 0.57 | |
| SFSVY | -• 000003 | 10139. | -21193. | -25.75 | -12.78 | -0.58 | |
| SFSVZ | -• 000003 | -1061. | 2812. | 3.13 | 2.04 | 0.07 | |
| SFSVZ | • 000003 | 1137. | -2962. | -2.31 | -2.13 | -0.07 | |
| SFSVZ | -• 000003 | 9. | -18. | -15. | -0.02 | -0.01 | -0.11 |
| ABSVX | -• 000003 | -6. | 17. | 14. | 0.02 | 0.01 | 0.11 |
| ABSVX | • 000003 | -9206. | 19647. | -174. | 24.33 | 12.80 | 0.53 |
| ABSVY | -• 000003 | 9332. | -19863. | 175. | -24.58 | -12.97 | 0.54 |
| ABSVY | • 000003 | 817. | -234. | 13. | -0.73 | 0.93 | -0.02 |
| ABSVZ | -• 000003 | -749. | 102. | -13. | 0.57 | -1.01 | 0.02 |
| ABSVZ | • 000003 | -140. | 268. | 701. | 0.31 | 0.18 | 0.95 |
| CHI1X | -• 000003 | 147. | -289. | -701. | -0.34 | -0.19 | -0.95 |
| CHI1X | • 001196 | 73. | -162. | -290. | -0.17 | -0.22 | -0.07 |
| CHI1Y | -• 001196 | -60. | 143. | 289. | 0.15 | 0.21 | 0.07 |
| CHI1Y | • 000573 | -454. | 998. | 1939. | 1.55 | 0.67 | 2.03 |
| CHI1Z | -• 000573 | 459. | -1009. | -1939. | -1.56 | -0.67 | -2.03 |
| CHI1Z | • 001196 | -4686. | 8465. | -86. | 10.57 | 4.65 | 0.24 |
| EP SVXZ | -• 001196 | 4727. | -8537. | 85. | -10.65 | -4.70 | -0.75 |
| EP SVYX | • 000834 | -72. | -72. | 2. | -0.58 | -0.02 | -0.00 |
| EP SVYX | -• 000834 | 95. | -36. | -1. | 0.51 | -0.01 | -0.00 |
| EP SVYX | • 00293 | 8813. | -18738. | 162. | -22.46 | -12.33 | -0.51 |
| EP SVYZ | -• 00393 | -8764. | 18683. | -162. | 22.39 | 12.27 | 0.51 |
| EP SVYZ | • 000834 | 16. | 40. | 0. | -0.03 | 0.53 | -0.00 |
| EP SVYY | -• 000834 | 5. | -83. | -1. | -0.02 | -0.55 | -0.00 |
| EP SVYY | • 00278 | 506. | 1071. | 9. | 0.69 | 2.01 | 0.01 |
| EP SVZY | -• 00278 | -402. | -1288. | -8. | -0.95 | -2.15 | -0.07 |
| EP SVZY | • C0879 | -355. | 718. | 1297. | 0.85 | 0.48 | 0.23 |
| EP SVZX | -• 00879 | 353. | -711. | -1299. | -0.84 | -0.47 | -0.33 |
| EP SVZX | • 00834 | 772. | -1528. | -2821. | -1.79 | -1.00 | -2.96 |
| EP SVZX | -• 00834 | -740. | 1454. | 2822. | 1.70 | 0.96 | 2.96 |
| RSS | | 23754. | 44000. | 8865. | 58.67 | 42.66 | 27.76 |

TABLE 25

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**ERRORS AT WAITING POINT INSERTION
DUE TO PERFORMANCE ERRORS**

| | ER | FV | FRFTA, F-3 DFG | FINCL, F-3 DFG | ENDDE F-3 DEG |
|--------|--------|--------|-------------------|-------------------|------------------|
| | FT | FT/SEC | F-3 DFG | F-3 DFG | |
| EISP* | 0.419 | -71. | -0.27 | 0.5 | -0.4 |
| FDWGT1 | -0.419 | 79. | 0.27 | -0.5 | 0.4 |
| | 0.714 | -48. | -0.16 | 0.3 | -0.2 |
| | -0.714 | 26. | 0.10 | -0.2 | 0.1 |
| FM* | 0.895 | 1C9. | C.35 | -0.6 | -0.2 |
| | -0.895 | 148. | C.59 | -C.9 | -0.4 |
| FFUEL1 | 0.5 | -67. | -0.19 | 0.3 | -0.6 |
| | -0.5 | 21. | 0.07 | -0.3 | 0.1 |
| FWGT* | 2.946 | 63. | 0.20 | -0.2 | -0.2 |
| | -2.946 | -56. | -0.18 | 0.3 | -0.2 |
| ECD | 1.00 | 30. | 0.05 | -0.1 | -0.1 |
| | -1.00 | -26. | -0.09 | 0.2 | 0.2 |
| FRHWA | 1.00 | 33. | 0.11 | -0.2 | -0.1 |
| | -1.00 | -28. | -0.09 | 0.2 | -0.2 |
| EISP2 | 0.427 | -72. | -0.24 | 0.4 | -0.4 |
| | -0.427 | 81. | 0.24 | -0.4 | 0.4 |
| FDWGT2 | 1.024 | -36. | -0.13 | 0.2 | -0.2 |
| | -1.024 | 62. | 0.24 | -0.2 | 0.2 |
| EM? | 0.895 | -25. | -0.04 | C.1 | -0.1 |
| | -0.895 | 48. | 0.15 | -0.2 | -0.2 |
| EFUEL2 | 0.5 | -11. | -0.05 | 0.1 | -0.1 |
| | -0.5 | 15. | 0.00 | -0.0 | 0.0 |
| FWGT2 | 2.407 | 75. | 0.23 | -0.4 | -0.4 |
| | -2.407 | -73. | -0.27 | 0.5 | -0.4 |
| EISP2 | 0.929 | -58. | -0.10 | 0.1 | -0.1 |
| | -0.929 | 61. | 0.06 | -0.1 | 0.1 |
| FDWGT3 | 2.0 | -114. | 0.03 | -0.4 | 0.3 |
| | -2.0 | 139. | -0.05 | 0.7 | -1.6 |
| FM? | 2.0 | -19. | 0.00 | 0.4 | -2.1 |
| | -2.0 | 18. | -0.01 | 0.0 | -0.2 |

C.2

0.0

-0.2

-0.2

-0.2

-0.2

-0.2

0.0

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| | ER | FV | FT | FT / SEC | EBFT A | E-2 DFG | FINCL | E-3 DEG | END DEG | E-2 DEG |
|----------|--------|--------|-------|----------|--------|---------|-------|---------|---------|---------|
| FFIIFL 2 | 1.0 | -21. | -0.05 | -0.1 | -0.1 | -0.1 | -0.1 | 0.0 | 0.0 | -0.0 |
| FIGT2 | -1.0 | 27. | 0.07 | -0.1 | -C.C6 | C.C6 | 0.1 | -0.1 | -0.1 | C.C |
| FCAFF1 | -1.936 | -23. | -C.C6 | -0.1 | -0.1 | -0.1 | 0.1 | 0.1 | -0.1 | -0.0 |
| FCAFF2 | 0.02 | 23. | C.C6 | -0.1 | -0.01 | 0.01 | -0.1 | 0.1 | 0.1 | -0.0 |
| FLLAGF | -0.02 | 2. | 0.01 | -0.0 | -0.0 | -0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| F4AFF2 | 0.02 | 5. | -0.00 | 0.0 | -0.0 | -0.0 | -0.0 | -0.0 | -0.0 | 0.0 |
| FVFNTR | -C.C2 | 244. | 1.24 | 0.3 | -1.25 | -1.25 | -0.3 | 0.2 | -0.2 | 0.9 |
| FVFNTR | 5.0 | -244. | -0.05 | -0.0 | -0.07 | -0.07 | -0.0 | -0.0 | -0.0 | -0.9 |
| FVFNTR | -5.0 | -5. | -4. | -0.05 | -0.05 | -0.05 | -0.0 | -0.0 | -0.0 | 0.0 |
| RSS | 20.0 | 3469. | 8.31 | -12.1 | -8.34 | -8.34 | 12.0 | 12.5 | 12.5 | 12.5 |
| RSS | -20.0 | -3471. | -8.34 | 12.0 | -12.5 | -12.5 | -12.0 | -12.5 | -12.5 | -12.0 |
| RSS | 3491. | 6.84 | 1.2.2 | 1.2.5 | 3.1 | 3.1 | 3.1 | 3.1 | 3.1 | 3.1 |

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TABLE 16

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ACTUAL DEVIATIONS AT WAITING ORBIT INSERTION
DUE TO PERFORMANCE ERRORS

| | R FT | V FT/SFC | BETA F-3 CEG | INCL F-3 DFG | NODE F-3 DEG | PHIT E-3 DEG | FUEL LBS |
|--------|---------|-------------|-----------------|-----------------|-----------------|-----------------|-------------|
| FISP1 | 0. 419 | 22522. | -20. 27 | 71. 6 | -1. 7 | -7. 2 | 14. 0 |
| FDWGT1 | -0. 419 | -23090. | 20. 73 | -73. 6 | 2. 1 | 9. 4 | -18. 1 |
| FM1 | 0. 716 | 7910. | -7. 09 | 24. 9 | -0. 8 | -7. 9 | 5. 7 |
| FFUFL1 | -0. 716 | -9582. | 8. 58 | -30. 4 | 0. 9 | 3. 9 | -7. 2 |
| FM2 | 0. 895 | -31819. | 28. 54 | -1C1. 5 | 3. 0 | 13. 8 | -29. 4 |
| FFUFL2 | -0. 895 | -49048. | 44. 09 | -157. 0 | 4. 9 | 22. 6 | -50. 0 |
| FM3 | 0. 5 | 9350. | -9. 50 | 29. 9 | -0. 9 | -3. 1 | 88. 0 |
| FWGCT1 | -0. 5 | -10732. | 9. 56 | -34. 0 | 0. 8 | 4. 0 | -99. 1 |
| FWGCT2 | 2. 846 | -18649. | 16. 71 | -59. 4 | 1. 7 | 7. 6 | -173. 7 |
| FCO | -2. 846 | 18549. | -16. 58 | 58. 7 | -1. 4 | -6. 1 | 171. 6 |
| FRHQA | 10. 0 | -8822. | 7. 97 | -28. 0 | 0. 7 | 3. 2 | -81. 6 |
| FISP2 | -10. 0 | 8714. | -7. 80 | 27. 6 | -0. 7 | -2. 8 | 16. 5 |
| FRHQA | 10. 0 | -7217. | 6. 51 | -22. 9 | 0. 6 | 2. 6 | -15. 9 |
| FFUFL2 | -10. 0 | 7285. | -6. 54 | 23. 1 | -0. 6 | -2. 7 | 14. 4 |
| FISP2 | 0. 427 | 22590. | -20. 30 | 71. 7 | -1. 7 | -7. 2 | -80. 6 |
| FDWGT2 | -0. 427 | -22855. | 20. 48 | -72. 7 | 2. 0 | 9. 2 | -212. 7 |
| FM2 | 1. 34 | 11160. | -10. 00 | 35. 4 | -1. 0 | -4. 3 | 103. 5 |
| FFUFL2 | -1. 34 | -13868. | 12. 54 | -44. 2 | 1. 4 | 5. 9 | -60. 2 |
| FM2 | 0. 895 | 7447. | -6. 63 | 23. 6 | -0. 5 | -2. 5 | 9. 0 |
| FFUFL2 | -0. 895 | -10105. | 9. 10 | -32. 2 | 0. 9 | 3. 8 | 2. 5 |
| FM2 | -0. 5 | 2923. | -2. 62 | 9. 3 | -0. 3 | -1. 1 | -5. 8 |
| FWGCT2 | -0. 5 | -3350. | 2. 97 | -10. 6 | 0. 2 | 1. 3 | 3. 7 |
| FWGCT3 | 2. 402 | -21319. | 19. 11 | -67. 9 | 1. 9 | 8. 6 | -3. 4 |
| FISP2 | -2. 402 | 21289. | -9. 10 | 67. 4 | -1. 6 | -6. 7 | 198. 4 |
| FDWGT3 | 0. 929 | -12695. | 11. 06 | -29. 7 | -0. 8 | -3. 9 | -15. 0 |
| FM2 | -0. 929 | -2801. | 11. 17 | 40. 0 | 0. 8 | 4. 5 | 13. 6 |
| FFUFL2 | -3. 0 | -94544. | 83. 56 | -301. 5 | -1. 9 | -13. 0 | -14. 9 |
| FM2 | 2. 0 | 112746. | -99. 04 | 349. 2 | 2. 8 | 19. 7 | -871. 2 |
| FFUFL2 | -2. 0 | -7060. | 6. 21 | -22. 3 | -1. 7 | -9. 9 | 1011. 1 |
| FM2 | -2. 0 | 4850. | -4. 27 | 15. 3 | 2. 5 | 14. 3 | -63. 9 |

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| | R FT | V FT/SEC | BETA F-3 DEG | WCL F-3 DEG | NODE E-3 DEG | PHIT F-3 DEG | FUEL LBS |
|--------|---------|-------------|-----------------|----------------|-----------------|-----------------|-------------|
| FFUFL3 | 1.0 | 487. | -0.50 | 1.7 | 2.1 | 4.6 | 260.9 |
| FWGT3 | -1.0 | -1957. | 1.74 | -6.1 | -1.5 | -17.7 | -210.4 |
| | 1.936 | 489. | -0.51 | 1.7 | 2.1 | 4.7 | -2129.3 |
| F4AFF1 | -1.936 | -1956. | 1.80 | -6.3 | -1.6 | -18.3 | 2182.4 |
| | 0.01 | -360. | 0.37 | -1.1 | 0.1 | 0.2 | -3.3 |
| FEAFF? | -0.02 | 360. | -0.33 | 1.2 | -0.1 | -0.2 | 3.4 |
| | 0.02 | 244. | 1.24 | 0.3 | -0.2 | 0.9 | -0.2 |
| | -0.03 | -245. | -1.25 | -0.3 | 0.2 | -0.9 | 14.1 |
| FULAGE | 6.0 | -699. | 0.59 | -2.2 | -0.0 | 0.0 | -6.3 |
| | -5.0 | 682. | -0.66 | 2.2 | -0.0 | -0.0 | 6.6 |
| FVFNTR | 20.0 | -915. | 12.18 | -25.9 | 17.5 | 1.8 | -3.9 |
| | -20.0 | 937. | -12.23 | 25.9 | -12.5 | -1.9 | -40.5 |
| RSS | | 1337C2. | 118.65 | 418.1 | 15.0 | 43.8 | 1219.2 |
| | | | | | | | 4349.7 |

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TABLE 37

ACTUAL DEVIATIONS AT WAITING ORBIT INSERTION
DRAFT PERFORMANCE ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SEC | TIME SEC |
|--------------------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| EISP ¹ | 0.419 | 57246. | -63940. | -9703. | -68.17 | -34.39 | 1.89 |
| FDWGT ₁ | -0.419 | -58905. | 65484. | 9655. | 69.87 | 35.65 | -2.41 |
| FM1 | 0.716 | -19059. | -22388. | -9953. | -73.89 | -12.11 | -2.93 |
| FM1 | -0.716 | -24235. | 27053. | 3573. | 28.86 | 14.67 | 0.74 |
| FFUFL ¹ | 0.895 | -70593. | 78166. | 10346. | 82.60 | 42.71 | -1.01 |
| FFUFL ¹ | -0.895 | -42855. | 59079. | 20454. | 168.72 | 86.76 | -2.98 |
| FFUFL ¹ | 0.5 | 23945. | -26891. | -3606. | -28.70 | -14.56 | -5.95 |
| FWGT ¹ | -0.5 | -27175. | 30127. | 4056. | 22.12 | 16.32 | -6.77 |
| FWGT ¹ | 2.846 | -47528. | 52867. | 6997. | 56.38 | 28.76 | -1.95 |
| FCN | 10.0 | -22359. | 46935. | -52368. | -71.26. | -55.80 | -2.20 |
| FRHAA | -10.0 | 22056. | -24820. | 3145. | 26.47 | 13.44 | -0.84 |
| FISP ² | 10.0 | -19384. | -24558. | -3348. | -26.19 | -12.24 | -0.72 |
| FISP ² | -10.0 | 18478. | 20498. | 2741. | 21.89 | 11.11 | -0.66 |
| FDWGT ² | 1.34 | -20602. | -2801. | -21.98 | -21.98 | -11.11 | -0.60 |
| FDWGT ² | -1.34 | 57369. | -64037. | -9732. | -68.25 | -34.44 | -1.90 |
| EM2 | 0.895 | -58234. | 64700. | 8568. | 69.02 | 35.21 | -2.35 |
| EM2 | -0.895 | -25790. | -31562. | -4198. | -33.64 | -17.04 | -2.38 |
| FFUFL ² | 0.5 | 78293. | -35497. | 39661. | 51.65. | 42.32 | -1.11 |
| FWGT ² | 2.402 | 18810. | -20904. | -2850. | -22.28 | -11.27 | -0.50 |
| FISP ² | -2.402 | -0.895 | -25790. | 28777. | 3831. | 30.71 | -0.64 |
| FDWGT ² | 3.0 | -1.34 | -8374. | -1113. | -8.93 | -4.55 | -0.28 |
| EM1 | 2.0 | -0.5 | -8479. | 9415. | 1274. | 10.02 | -0.23 |
| EM1 | -2.0 | -0.929 | -54311. | 60354. | 7996. | 64.29 | -2.21 |
| FISP ² | 0.929 | 53904. | -60217. | -9197. | -64.20 | -22.40 | -0.77 |
| FDWGT ² | 3.0 | -2.0 | -31617. | 34581. | 5010. | 37.12 | 0.91 |
| EM1 | 2.0 | -2.0 | 31789. | -34893. | -6123. | -37.44 | -1.04 |
| EM1 | -2.0 | -12047. | -240684. | 242821. | 42843. | 28255. | -14.77 |

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TABLE 3A

**UNCERTAINTIES AT WAITING ORBIT INSERTION
DUE TO PERFORMANCE ERRORS**

| | FRNX FT | ERNY FT | ERNZ FT | FVNX FT/SEC | FVNZ FT/SEC | FVN2 FT/SFC |
|---------|------------|------------|------------|----------------|----------------|----------------|
| FISP 1 | 0.419 | -456. | 1008. | .69. | 1.09 | 0.65 |
| FDWGT1 | -0.419 | 456. | -1024. | -69. | -1.11 | -0.58 |
| FDWGT1 | 0.716 | -759. | 602. | 20. | 0.66 | -0.68 |
| FM 1 | -0.716 | 176. | -776. | -30. | -0.41 | 0.40 |
| FM 1 | 0.295 | 609. | -1355. | -93. | -1.45 | -0.75 |
| FM 1 | -0.895 | 1007. | -2156. | -143. | -2.33 | -0.91 |
| EFUFL 1 | 0.5 | -314. | 750. | 26. | -1.42 | -1.12 |
| FWGCT 1 | -0.5 | 112. | -244. | -32. | 0.82 | -1.42 |
| FWGCT 1 | 2.846 | 341. | -765. | -55. | -0.25 | -0.16 |
| FWGCT 1 | -2.846 | -298. | 674. | 56. | -0.87 | -0.51 |
| FCN | 0.0 | -108. | -256. | -28. | 0.71 | -0.51 |
| FCN | -0.0 | -147. | 325. | 27. | -0.45 | -0.37 |
| FP HPA | 1.0. C | 1.92. | -410. | -71. | 0.22 | -0.22 |
| FP HPA | -1.0. C | -1.58. | 350. | 22. | -0.28 | -0.19 |
| FISP 2 | 0.427 | -396. | 897. | 68. | 0.96 | 0.58 |
| FISP 2 | -0.427 | 414. | -925. | -70. | -0.09 | -0.62 |
| FDWGT2 | 1.0.34 | -221. | 488. | 35. | 0.52 | 0.32 |
| FM 2 | -1.0.34 | 418. | -920. | -41. | -1.02 | -0.61 |
| FM 2 | 0.895 | -84. | 201. | 23. | 0.20 | 0.14 |
| FM 2 | -0.895 | 242. | -568. | -27. | -0.62 | -0.39 |
| EFUFL 2 | 0.5 | -83. | 187. | 8. | 0.20 | 0.12 |
| FWGCT 2 | -0.5 | 14. | -47. | -17. | -0.04 | -0.04 |
| FWGCT 2 | 2.402 | 408. | -897. | -65. | 0.96 | -0.50 |
| FWGCT 2 | -2.402 | -442. | 985. | 65. | 1.07 | 0.64 |
| FISP 3 | 0.929 | -170. | 430. | -52. | 0.47 | 0.28 |
| FDWGT3 | -0.929 | 92. | -358. | 51. | -0.39 | -0.24 |
| FDWGT3 | 2.0 | 126. | 257. | -338. | 0.32 | -0.18 |
| FM 3 | -3.0 | -181. | -254. | 601. | -0.25 | -0.10 |
| FM 3 | 2.0 | 14. | 24. | -46. | 0.04 | 0.02 |
| FM 3 | -2.0 | -39. | 28. | 39. | 0.03 | C.01 |

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| | RPX FT | RPY FT | RPZ FT | VPX FT/SFC | VPY FT/SEC | Vpz FT/SFC | TIMF SEC |
|---------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| EFUFL 2 | 1.0 | 1270. | -1462. | -1992. | -1.93 | -0.59 | -2.09 |
| FWGTR | -1.0 | -4823. | 5449. | 2143. | 5.10 | 2.90 | 2.21 |
| F4AFF1 | 1.936 | 1293. | -1493. | -2065. | -1.98 | -0.60 | -3.21 |
| F4AFF2 | -1.936 | -5003. | 5609. | 2218. | 6.28 | 2.87 | 2.37 |
| FULGF | 0.02 | -91.0 | 1011. | 109. | 1.07 | 0.54 | -0.50 |
| F4AFF3 | -0.02 | -0.03 | 914. | -1039. | -1.11 | -1.10 | -0.57 |
| FVFNTR | 0.02 | 512. | -676. | -105. | 0.06 | 1.57 | 0.04 |
| FULGF | -0.02 | -615. | 678. | 106. | -0.06 | 1.57 | 0.03 |
| F4AFF4 | 5.0 | -1737. | 1907. | 298. | 2.00 | 1.02 | -0.42 |
| FVFNTR | -5.0 | 1777. | -2020. | -295. | -2.20 | 1.10 | -0.05 |
| FVFNTR | 20.0 | -24881. | 47353. | 1681. | 51.14 | 26.73 | 0.01 |
| FVFNTR | -20.0 | 24811. | -47455. | -1693. | -51.27 | -29.63 | 0.01 |
| PSS | 333401. | 373557. | 57885. | 390.58 | 198.05 | 10.45 | 18.931 |

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| | ERNX FT | ERNY FT | ERNZ FT | EVNX FT/SEC | EVNY FT/SEC | EVNZ FT/SEC | EVN2 FT/SEC |
|---------|------------|------------|------------|----------------|----------------|----------------|----------------|
| FFIUEL3 | 1.0 | -90. | 220. | 7. | 0.25 | 0.15 | 0.02 |
| FWGT2 | 1.936 | 126. | -308. | -10. | -0.34 | -0.20 | -C. C2 |
| | -1.936 | -94. | 242. | 8. | 0.26 | 0.16 | C. C2 |
| E40FF1 | 0.03 | 96. | -238. | -11. | -0.25 | -0.15 | -C. C2 |
| | -0.03 | 8. | -10. | -2. | -0.01 | -0.01 | -0.00 |
| F40FF2 | 0.03 | -60. | -17. | 20. | 0.02 | C. 01 | 0.00 |
| | -0.03 | 7. | -9. | -1. | -0.01 | -0.01 | C. 00 |
| FULLAGE | 5.0 | -6. | 5. | -5. | -0.01 | -0.00 | -C. C0 |
| | -5.0 | 3. | 15. | -4. | 0.05 | 0.01 | -C. C0 |
| FVFNT2 | 20.0 | -46. | 102. | 0. | 0.15 | 0.07 | 0. C1 |
| | -20.0 | 13855. | -25169. | 207. | -38.10 | -22.17 | -C. 87 |
| RSS | 13936. | 353326. | 35181. | -205. | 38.14 | 22.02 | C. 87 |
| | | | | | | | |
| | | | 502. | 38.32 | 23.27 | 0.98 | |

TABLE 39

COVARIANCE MATRIX OF ERRORS
AT WAITING ORBIT INSERTION

| | ER | EV | EBETA | EINCL | ENODE |
|-------|-----------|-----------|-----------|-----------|----------|
| ER | 1.88E 03 | -0.3 | 0.5 | 0.2 | -0.3 |
| EV | -9.17E 03 | 1.39E 01 | -0.8 | 0.7 | -0.3 |
| EBETA | 1.89E 01 | -2.13E-01 | 1.90E-02 | -0.4 | -0.3 |
| EINCL | 2.59E 00 | 9.52E-02 | -6.88E-05 | 9.16E-03 | -0.4 |
| ENODE | -2.39E 01 | -1.73E-01 | -3.01E-04 | -1.85E-04 | 4.71E-02 |

TABLE 40

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT WAITING ORBIT INSERTION

| | R | V | BETA | INCL | NODE | PHIT | FUEL |
|------|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| R | 3.75E 04 | -0.9 | 1.0 | -0.0 | 0.0 | 1.0 | -0.8 |
| V | -1.76E 06 | 3.61E 01 | -1.0 | 0.3 | -0.1 | -0.9 | 0.7 |
| BETA | 4.48E 03 | -4.19E 00 | 1.21E-01 | -0.1 | -0.0 | 1.0 | -0.8 |
| INCL | -8.61E 00 | 1.05E-01 | -1.04E-04 | 9.38E-03 | -0.4 | -0.1 | -0.1 |
| NODE | 1.01E 01 | -2.01E-01 | -1.94E-04 | -1.64E-04 | 4.83E-02 | 0.0 | -0.1 |
| PHIT | 1.30E 04 | -1.20E 01 | 4.18E-02 | -4.74E-04 | 3.14E-04 | 3.50E-01 | -0.7 |
| FUEL | -3.18E 07 | 2.79E 04 | -1.01E 02 | -8.55E-01 | -5.02E 00 | -2.90E 02 | 1.11E 03 |

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TABLE 41.

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT WAITING ORBIT INSERTION

| | RPX | RPY | RPZ | VPX | VPY | Vpz | TIME |
|------|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| RPX | 9.57E 04 | -1.0 | -1.0 | -1.0 | -1.0 | -0.0 | 1.0 |
| RPY | -1.02E 10 | 1.07E 05 | 1.0 | 1.0 | 1.0 | 0.0 | -0.9 |
| RPZ | -1.55E 09 | 1.72E 09 | 1.67E 04 | 1.0 | 0.9 | 0.2 | -1.0 |
| VPX | -1.09E 07 | 1.22E 07 | 1.85E 06 | 1.15E 02 | 1.0 | 0.1 | -0.9 |
| VPY | -5.52E 06 | 6.19E 06 | 9.41E 05 | 6.63E 03 | 5.95E 01 | 0.0 | -0.9 |
| Vpz | -1.17E 04 | 2.82E 04 | 3.80E 04 | 1.02E 02 | 1.44E 01 | 1.28E 01 | -0.1 |
| TIME | 5.08E 05 | -5.59E 05 | -8.88E 04 | -6.00E 02 | -3.05E 02 | -3.65E 00 | 5.52E 00 |

TABLE 42

COVARIANCE MATRIX OF UNCERTAINTIES
AT WAITING ORBIT INSERTION

| | ERNX | ERNY | ERNZ | EVNX | EVNY | EVNZ |
|------|-----------|----------|----------|----------|----------|----------|
| ERNX | 9.12E 03 | -1.0 | 0.1 | -0.9 | -0.4 | 0.0 |
| FRNY | -1.66E 08 | 1.87E 04 | 0.0 | 1.0 | 0.6 | 0.1 |
| ERNZ | 2.12E 06 | 1.76E 05 | 2.95E 03 | 0.2 | 0.1 | 0.9 |
| EVNX | -2.00E 05 | 4.20E 05 | 1.25E 04 | 2.32E 01 | 0.5 | 0.3 |
| EVNY | -6.59E 04 | 1.76E 05 | 6.61E 03 | 1.80E 02 | 1.61E 01 | 0.0 |
| EVNZ | 1.61E 03 | 1.52E 04 | 3.16E 04 | 8.68E 01 | 7.36E 00 | 1.26E 01 |

TABLE 43
ACTUAL DEVIATIONS AT FIXED TIME NO. 3
DUE TO PLATFORM ERRORS

| | EKCR FT | EKCR FT | EKUP FT | EKUK FT/SEC | EVUR FT/SEC | EVUP FT/SEC |
|-------|------------|------------|------------|----------------|----------------|----------------|
| GDSVX | .100 | 1794. | -4879. | 1723. | -3.26 | -19.23 |
| GDSVY | -.100 | -1701. | 4898. | -1720. | 3.41 | 19.20 |
| GDSVZ | .075 | -10158. | 1217. | -3282. | -36.93 | -0.83 |
| GDSVZ | -.075 | 10174. | -1204. | 3250. | 37.01 | 0.75 |
| GSSVX | .075 | 1528. | 11339. | 3279. | -4.58 | -33.34 |
| GSSVY | -.075 | -1225. | -11346. | -3330. | 4.62 | 33.24 |
| GSSVZ | .100 | 415. | -600. | 120. | -5.40 | -1.50 |
| USSVX | -.100 | -407. | 664. | -121. | 0.40 | 1.51 |
| USSVY | .075 | -1922. | 1410. | -68. | -2.14 | 0.18 |
| USSVZ | -.075 | 1992. | -1180. | 48. | 2.17 | -0.20 |
| USSVZ | .100 | 1. | 12. | -19. | 0.02 | 0.19 |
| UISVX | -.100 | 3. | -17. | 23. | -0.02 | -0.18 |
| UISVX | .075 | 100. | 10. | 34. | -9. | 0.08 |
| UISVY | -.100 | -14. | -77. | 4. | -0.08 | 0.10 |
| UISVY | .075 | 24. | -25. | 22. | 0.18 | -0.09 |
| UISVZ | .075 | -34. | -16. | -13. | -0.17 | -0.00 |
| UISVZ | -.075 | 2594. | 20318. | 2257. | -1.37 | -3.90 |
| LDSVX | .000 | 2597. | -20333. | -2278. | 1.36 | 3.88 |
| LDSVY | -.000 | 372. | -328. | 20. | 0.04 | -0.37 |
| LDSVZ | -.000 | -368. | 304. | -20. | -0.00 | 0.36 |
| USSVX | .000 | -2383. | 1398. | -159. | -3.64 | 0.21 |
| USSVY | -.000 | 2385. | -1404. | 149. | 3.64 | -0.20 |
| USSVZ | .000 | 1522. | 15172. | 1206. | -0.79 | -1.33 |
| Ssvx | .050 | -1868. | -14809. | -1215. | 0.86 | 1.30 |
| Ssvy | -.050 | 5. | 2. | -8. | 0.04 | 0.04 |
| Ssvz | .050 | -12. | -77. | 3. | -0.03 | -0.04 |
| Ssvz | -.050 | 1. | -23. | 2. | 0.02 | 0.00 |
| SSVX | .050 | -10. | -29. | 3. | -0.92 | 0.09 |
| SSVY | -.050 | -1. | -2. | -8. | 0.01 | 0.07 |
| SSVZ | .050 | -6. | -32. | 12. | -0.01 | -0.07 |

| | EKCK FT | ERDR FT | ERUP FT | EVCR FT/SEC | EVUR FT/SEC | EVUP FT/SEC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| SFSVX | .00003 | 2875. | 23167. | -415. | -0.78 | 1.05 |
| SFSVY | -.00003 | -2928. | -23519. | 415. | 0.79 | -1.70 |
| SFSVZ | -.00003 | 374. | 3143. | -278. | -0.05 | 0.53 |
| SFSVZ | -.00003 | -392. | -3205. | 309. | 0.06 | -0.24 |
| SFSVZ | .00003 | 22. | -13. | 2. | 0.11 | 0.92 |
| ABSVX | -.00003 | -22. | 21. | -3. | -0.11 | 0.02 |
| ABSVY | -.00003 | 2699. | 20659. | -941. | -0.76 | -0.02 |
| ABSVZ | -.00003 | -2730. | -20852. | 942. | 0.77 | -26.60 |
| ABSVY | .00003 | -63. | 615. | -337. | 0.17 | 26.65 |
| ABSVZ | -.00003 | 46. | -683. | 358. | -0.17 | -1.18 |
| ABSVZ | -.00003 | -708. | 249. | -33. | -0.82 | 0.13 |
| CH1X | -.00190 | 704. | -261. | 33. | 0.92 | -0.13 |
| CH1Y | -.00196 | 271. | -217. | 6. | 0.03 | -0.13 |
| CH1Y | .00573 | -273. | 219. | -3. | -0.03 | 0.14 |
| CH1Z | -.00573 | -1962. | 1348. | -37. | -1.85 | 0.14 |
| CH1Z | -.00196 | 1961. | -1388. | 27. | 1.85 | -0.19 |
| EPSVXZ | -.00196 | 1199. | 9545. | 440. | -0.45 | -0.24 |
| EPSVY | -.00196 | -1209. | -9612. | -442. | 0.45 | -11.52 |
| EPSVY | -.00834 | 3. | -91. | 82. | 0.03 | 11.61 |
| EPSVY | -.00834 | -11. | 30. | -81. | -0.02 | 0.07 |
| EPSVY | -.00393 | -2582. | -21008. | 414. | 0.67 | -0.59 |
| EPSVY | -.00393 | 2572. | 20963. | -427. | -0.67 | 25.83 |
| EPSVY | -.00834 | 8. | 101. | -34. | 0.05 | -25.76 |
| EPSVY | -.00834 | -13. | -99. | 49. | -0.05 | -0.18 |
| EPSVY | -.00278 | 98. | 1065. | -941. | 0.17 | 0.40 |
| EPSVY | -.00278 | -128. | -1247. | 963. | -0.16 | -1.63 |
| EPSVY | .00879 | -124. | 940. | 12. | -0.24 | -1.87 |
| EPSVY | -.00879 | 1225. | -900. | -4. | 0.24 | -0.94 |
| EPSVX | .00834 | 2825. | -1957. | -21. | 2.64 | 0.90 |
| EPSVX | -.00834 | -2837. | 1872. | 24. | -2.63 | 1.89 |
| RSS | | 12953. | 48406. | 5842. | 37.90 | 61.02 |

TABLE 44

UNCERTAINTIES AT FIXED TIME NO. 3
DUE TO PLATFORM ERRORS

| | ERNCK FT | ERNUK FT | ERNUP FT | EVNCR FT/SEC | EVNUK FT/SEC | EVNUP FT/SEC |
|-------|-------------|-------------|-------------|-----------------|-----------------|-----------------|
| GUSVX | .100 | -1742. | 4885. | -1722. | 3.27 | -8.57 |
| GUSVY | -.100 | 1760. | -4808. | 1728. | -3.41 | -19.20 |
| GUSVZ | .075 | 10166. | -1241. | 3273. | 36.93 | 8.54 |
| GUSVY | -.075 | -10183. | 1262. | -3232. | -37.00 | 16.90 |
| GUSVZ | .075 | -1528. | -11254. | -3254. | 4.58 | -16.74 |
| GUSVY | -.075 | 1521. | 11312. | 3308. | -4.62 | 9.64 |
| USSVX | .100 | -414. | 568. | -124. | 0.40 | -8.84 |
| USSVY | -.100 | 407. | -644. | 127. | -0.40 | -0.88 |
| USSVZ | .075 | 1955. | -1402. | 70. | 2.14 | -1.20 |
| USSVY | -.075 | -1992. | 1195. | -43. | -2.17 | -0.50 |
| USSVZ | .100 | -1. | -10. | 20. | -0.02 | -0.18 |
| U1SVX | -.100 | 100 | 3. | 42. | -0.02 | 1.90 |
| U1SVX | .100 | -10. | -33. | 9. | -0.08 | -1.53 |
| U1SVY | -.100 | 13. | 76. | -4. | 0.08 | 0.12 |
| U1SVY | .075 | -24. | 54. | -12. | -0.18 | -0.14 |
| U1SVZ | -.075 | 33. | 23. | 15. | 0.17 | 0.05 |
| U1SVZ | .075 | -2594. | -20294. | -2261. | 1.37 | 0.06 |
| U2SVX | -.075 | 2595. | 20322. | 2248. | -1.37 | -0.91 |
| U2SVX | .060 | -372. | 342. | -22. | -0.05 | 0.37 |
| U2SVZ | -.060 | 368. | -286. | 25. | -0.00 | -0.56 |
| U2SVY | -.060 | 2383. | -1410. | 154. | 3.64 | 2.33 |
| U2SVY | -.060 | -2386. | 1398. | -151. | -3.64 | -2.31 |
| U2SVZ | -.060 | -1922. | -15066. | -1177. | 0.78 | 1.76 |
| S2SVX | .050 | 1867. | 14780. | 1189. | -0.86 | -1.32 |
| S2SVY | -.050 | 12. | -15. | 3. | -0.04 | -0.03 |
| S2SVY | .050 | -1. | 78. | -3. | 0.03 | 0.10 |
| S2SVZ | -.050 | 9. | 25. | -2. | -0.02 | -0.04 |
| SSVX | .050 | 0. | 44. | 1. | 0.02 | 0.00 |
| SSVY | -.050 | 5. | -4. | 5. | -0.01 | -0.07 |
| SSVZ | -.050 | 6. | -4. | 5. | 0.01 | 0.11 |

| | EKNDR FT | EKNUP FT | EVNCR FT/SEC | EVNUK FT/SEC | EVNUP FT/SEC |
|--------|-------------|-------------|-----------------|-----------------|-----------------|
| SFSVX | •00003 | -2859. | -23026. | 444• | -1.66 |
| SFSVY | -•00003 | 2909. | 23454. | -469. | 28.64 |
| SFSVZ | .00C03 | -309• | -3040. | 310• | -29.16 |
| SFSVZ | -•00003 | 389• | 3207. | -310• | 3.72 |
| SFSVZ | •00003 | -22• | 23• | 0• | -3.92 |
| SFSVZ | -•00003 | 22• | -21• | 3• | -0.02 |
| ABSVX | -•00003 | -2089. | -21660. | 612• | 0.02 |
| ABSVY | -•00003 | 2717• | 21915• | -635• | 0.78 |
| ABSVY | •00003 | 69• | 401• | 628• | -0.79 |
| ABSVY | -•00003 | -52• | -253• | -655• | 0.17 |
| ABSVZ | •00003 | 738• | -393• | -17• | 0.87 |
| ABSVZ | -•00003 | -735• | 415• | 15• | -0.87 |
| CH11X | •00156 | -271• | 223• | -2• | -0.03 |
| CH11Y | -•00196 | 273• | -200• | 8• | 0.03 |
| CH11Y | •00573 | 1963• | -1330• | 40• | -0.13 |
| CH11Z | -•00573 | -1961• | 1349• | -39• | 1.85 |
| CH11Z | •00156 | -1198• | -9509• | -430• | -1.85 |
| EPSVXZ | -•0C196 | 1207• | 9592• | 427• | 0.45 |
| EPSVXZ | •0C834 | -4• | -26• | -120• | -0.03 |
| EPSVXZ | -•0C834 | 11• | 82• | 118• | 0.03 |
| EPSVXY | •0C393 | 2564• | 20707• | -234• | -0.69 |
| EPSVYZ | -•0C393 | -2557• | -20657• | 516• | 0.69 |
| EPSVYZ | •00834 | -8• | -75• | 43• | -0.06 |
| EPSVYZ | -•0C834 | 13• | 121• | -43• | 0.06 |
| EPSVYX | •10278 | -90• | -959• | 974• | -0.16 |
| EPSVYX | -•00278 | 119• | 1200• | -978• | 0.15 |
| EPSVYX | •00879 | 1216• | -955• | -18• | 0.21 |
| EPSVYX | -•00879 | -1219• | 948• | 18• | -0.21 |
| EPSVZX | •00834 | -2838• | 2070• | 57• | -2.67 |
| EPSVZX | -•00834 | 2849• | -1990• | -62• | 2.66 |
| RSS | | 12952• | 48664• | 5815• | 38.91 |
| | | | | | 38.91 |
| | | | | | 61.26 |

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TABLE 45

ACTUAL DEVIATIONS AT FIXED TIME NO. 3
DUE TO PERFORMANCE ERRORS

| | FRCR FT | FRDR FT | ERUP FT | EVCR FT/SEC | EVDR FT/SEC | EVUP FT/SEC |
|--------|------------|------------|------------|----------------|----------------|----------------|
| FISP1 | 0.419 | 1.357. | 17333. | 1.59 | 0.07 | -15.60 |
| EDWGT1 | -0.419 | -1.711. | -17020. | -4953. | -0.09 | 15.25 |
| EDWGT1 | 0.716 | 572. | 21029. | 6394. | 0.04 | -18.82 |
| FM1 | -0.716 | -709. | -21434. | -6630. | -0.02 | 19.10 |
| FM1 | 0.895 | -2491. | -23188. | -6730. | -0.16 | 20.90 |
| FFUFL1 | -0.895 | -4058. | -24367. | -6773. | -0.21 | 22.16 |
| FFUFL1 | 0.5 | 618. | -1914. | -918. | 0.08 | 1.48 |
| FCD | -0.5 | -711. | 3110. | 1095. | -0.00 | -2.72 |
| FWGTT1 | 2.845 | -1370. | -14654. | -4284. | -0.09 | 13.10 |
| FWGTT1 | -2.845 | 1122. | 4849. | 4374. | 0.06 | -13.22 |
| FCD | 1.0, 0 | -579. | -6409. | -1919. | -0.02 | 5.71 |
| FRHRA | -1.0, 0 | 521. | 6391. | 8890. | 0.01 | -5.74 |
| EISP2 | 0.427 | 1.344. | -5349. | -1535. | -0.02 | 4.85 |
| FRHRA | 1.0, 0 | -497. | 5285. | 1538. | 0.01 | -4.76 |
| EISP2 | -1.0, 0 | 442. | 8197. | 2209. | 0.07 | -7.48 |
| FRHGT2 | -0.427 | -1.677. | -7917. | -2112. | -0.07 | 7.24 |
| FFUFL2 | 1.34 | 787. | 68989. | 21508. | 1.00 | -61.22 |
| FM2 | -1.34 | -1103. | -71485. | -22269. | -1.36 | 63.70 |
| FM2 | 0.895 | 448. | 25904. | 8089. | -0.00 | -22.98 |
| FFUFL2 | -0.895 | -709. | -30956. | -9549. | -0.08 | 27.61 |
| EISP2 | 0.5 | 206. | -28507. | -9101. | 0.01 | 25.73 |
| FCD | -0.5 | -216. | 28550. | 9039. | -0.02 | -25.30 |
| FWGTT2 | 2.402 | 1.558. | -7518. | -2009. | -0.06 | 6.87 |
| FWGTT2 | -2.402 | 1274. | 7871. | 2083. | 0.07 | -7.22 |
| EISP2 | 0.929 | 685. | 15964. | 4843. | 0.08 | -14.22 |
| EDWGT2 | -0.929 | -763. | -15919. | -4863. | -0.09 | 14.27 |
| EDWGT2 | 2.0 | 2070. | 88763. | 27787. | 0.08 | -78.97 |
| FM2 | -2.0 | -3073. | -96185. | -30358. | -0.23 | 85.90 |
| FM2 | 2.0 | 1647. | 34499. | 1C871. | 2.39 | -3C.61 |
| FM2 | -2.0 | -2355. | -26657. | -3423. | -3.43 | 23.66 |

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| | ERCR FT | FRUP FT | EVCR FT/SEC | EVDR FT/SEC | EVUP FT/SEC |
|---------|------------|------------|----------------|----------------|----------------|
| FFUEL 3 | 1.0 | -2012. | -7775. | -7.96 | 0.07 |
| | -1.0 | 1488. | 5510. | 2.22 | -0.06 |
| FWGT 2 | 1.526 | -2090. | -2500C. | -3.07 | 0.02 |
| | -1.536 | 1541. | 26522. | 2.28 | -0.04 |
| FLUFF 1 | • 02 | -55. | -24374. | -7702. | -0.10 |
| | -• 02 | 57. | 24356. | 7677. | 0.10 |
| F4AFF7 | • 03 | -21. | 124. | 28. | -0.24 |
| | -• 02 | 21. | -124. | -28. | 0.24 |
| FULAGE | 5.0 | 1. | -827. | -776. | -0.00 |
| | -5.0 | 16. | 816. | 211. | -0.01 |
| EVENTR | 20.0 | -4610. | -34427. | 4362. | 0.98 |
| | -20.0 | 4603. | 34374. | -4430. | -0.99 |
| RSS | 8667. | 14999C. | 4585C. | 10.27 | 5.06 |

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TABLE 46

**UNCERTAINTIES AT FIXED TIME NO. 2
DUE TO PERFORMANCE ERRORS**

| | FRNCR FT | FRNDR FT | ERNUP FT | EVNCR FT/SEC | EVNDR FT/SEC | EVNUP FT/SEC |
|--------|-------------|-------------|-------------|-----------------|-----------------|-----------------|
| FISP1 | 0.416 | -105. | -1125. | 0.11 | -0.10 | 1.28 |
| EDWGT1 | -0.419 | 109. | -1145. | -0.12 | 0.11 | -1.22 |
| EDWGT1 | 0.716 | -60. | -661. | 0.04 | -0.07 | 0.78 |
| FM1 | -0.716 | 77. | 420. | -0.04 | 0.04 | -0.49 |
| FM1 | 0.695 | 144. | 1514. | -114. | -0.16 | -1.73 |
| FFUEL1 | -0.895 | 243. | 2423. | -153. | -0.25 | -2.77 |
| FFUEL1 | 0.5 | -95. | -826. | 68. | 0.06 | 0.67 |
| FWGT1 | -0.5 | 29. | 779. | -27. | -0.05 | -0.21 |
| FWGT1 | 2.846 | 80. | 854. | -66. | -0.09 | -0.98 |
| FCD | -2.846 | -66. | -752. | 59. | 0.09 | -0.07 |
| FCD | 10.0 | 23. | 286. | -32. | -0.04 | -0.85 |
| ERHRA | -10.0 | -37. | -364. | 26. | 0.04 | -0.22 |
| ERHRA | -10.0 | 46. | 456. | -31. | -0.04 | -0.54 |
| FISP2 | 0.427 | -98. | -390. | 25. | 0.04 | 0.44 |
| FISP2 | -0.427 | 1001. | -1001. | 78. | 0.11 | -1.14 |
| EDWGT2 | 1.34 | 102. | 1036. | -82. | -0.11 | -1.18 |
| EDWGT2 | -1.34 | -3. | -532. | 23. | 0.03 | 0.62 |
| FM2 | 1.34 | 58. | 1011. | -47. | -0.05 | -1.19 |
| FM2 | -0.895 | -2. | -220. | 21. | -0.02 | 0.25 |
| FFUEL2 | 0.5 | 47. | 623. | -50. | -0.04 | -0.74 |
| FFUEL2 | -0.895 | -46. | -214. | 20. | 0.03 | 0.24 |
| FWGT2 | 2.402 | 25. | 59. | -19. | -0.02 | -0.05 |
| FWGT2 | -2.402 | 100. | 1007. | -71. | -0.11 | -1.14 |
| FISP2 | 0.929 | -111. | -1099. | 73. | 0.11 | 1.26 |
| FISP2 | -0.929 | -61. | -436. | 51. | -0.05 | 0.55 |
| EDWGT3 | 2.0 | 50. | 356. | -51. | 0.06 | -0.45 |
| EDWGT3 | -2.0 | -56. | -94. | 52. | -0.07 | 0.33 |
| EM2 | 2.0 | 56. | 58. | -63. | 0.51 | -0.33 |
| EM2 | -2.0 | -6. | -2. | 7. | -C.C7 | 0.01 |
| | | | | -53. | C.C6 | -0.01 |
| | | | | -12. | C.C3 | |

| | FRNCR FT | FRNDR FT | ERNUP FT | EVNCR FT/SEC | EVNDR FT/SEC | FVNUP FT/SEC | FVNDR FT/SEC |
|---------|-------------|-------------|-------------|-----------------|-----------------|-----------------|-----------------|
| EFLUFL2 | 1.0 | -41. | -255. | 26. | 0.03 | -C.04 | C.29 |
| EWGTR2 | 1.936 | 57. | 343. | -37. | -0.02 | 0.05 | -0.39 |
| F4AFF1 | -1.936 | -42. | -269. | 27. | 0.03 | -0.04 | C.3C |
| F4AFF1 | 0.03 | 43. | 267. | -27. | -0.03 | 0.04 | -C.3C |
| FULAGF | -0.02 | -19. | 7. | 7. | 0.01 | -C.01 | -0.01 |
| F4AFF2 | -0.02 | -0.02 | 17. | -19. | -11. | -0.01 | 0.01 |
| FULAGF | -0.03 | -0. | 0. | 11. | 3. | 0.00 | -0.01 |
| FVNTR | 5.0 | -4. | -11. | 2. | 0.00 | 0.00 | -0.01 |
| FVNTR | -5.0 | -14. | -111. | 11. | 0.00 | 0.01 | 0.05 |
| FVNTR | 20.0 | 4608. | 38073. | 9. | 0.01 | 0.00 | C.16 |
| FVNTR | -20.0 | -4610. | -38030. | -3270. | -0.99 | 4.71 | -44.67 |
| RSS | | 4625. | 3825C. | 3281. | 1.17 | 4.77 | 44.87 |

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TABLE 47

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT FIXED TIME NO. 3

| | EKUR | EKUR | EKUP | EVUR | EVUK | EVUP |
|------|-----------|-----------|-----------|-----------|-----------|----------|
| EKUR | 4.92E 03 | 0.4 | 0.3 | 0.7 | -0.1 | -0.4 |
| EKUR | 1.05E 08 | 5.00E 04 | 0.9 | 0.1 | -0.0 | -1.0 |
| EKUP | 2.10E 07 | 6.47E 08 | 1.45E 04 | 0.2 | -0.1 | -0.8 |
| EKUR | 4.58E 04 | 6.30E 04 | 3.085E 04 | 1.029E 01 | 0.2 | 0.0 |
| EVUR | -6.33E 03 | -1.07E 04 | -1.91E 04 | 2.70E 01 | 1.31E 01 | -0.0 |
| EVUK | -8.92E 04 | -2.35E 06 | -5.04E 05 | 1.19E 01 | -8.96E 00 | 4.76E 01 |

TABLE 48

COVARIANCE MATRIX OF UNCERTAINTIES
AT FIXED TIME NO. 3

| ERNUK | ERNDR | ERNUP | EVNCR | EVNDR | EVNUP |
|-----------|-----------|-----------|----------|-----------|----------|
| 4.57E 03 | 0.5 | 0.3 | 0.7 | -0.1 | -0.3 |
| 4.74E 07 | 2.05E 04 | -0.2 | -0.1 | -0.0 | -1.0 |
| 3.43E 06 | -7.75E 06 | 2.21E 03 | 0.4 | -0.7 | 0.3 |
| 4.12E 04 | -2.55E 04 | 1.12E 04 | 1.26E 01 | 0.2 | 0.3 |
| -6.55E 03 | -1.02E 04 | -1.89E 04 | 2.67E 01 | 1.31E 01 | -0.0 |
| -3.83E 04 | -5.04E 05 | 1.72E 04 | 9.07E 01 | -9.39E 00 | 2.52E 01 |

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TABLE 49
ACTUAL DEVIATIONS
IN SPACECRAFT DELTA-V
DUE TO PLATIFORM ERRORS

| | | DEL V1 FT/SEC | DEL V2 FT/SEC |
|-------|-------|------------------|------------------|
| GDSVX | .100 | 18.02 | -0.02 |
| GDSVY | -.100 | -17.95 | 0.03 |
| GDSVY | .075 | 14.46 | -0.01 |
| GDSVZ | -.075 | -14.24 | 0.32 |
| GDSVZ | .075 | 40.21 | -0.02 |
| USSVX | -.075 | -39.61 | 0.01 |
| USSVX | .100 | 1.34 | 0.00 |
| USSVY | -.100 | -1.32 | 0.01 |
| USSVY | .075 | 0.61 | -0.00 |
| USSVZ | -.075 | -0.40 | 0.01 |
| USSVZ | .100 | -0.14 | 0.01 |
| UISVX | -.100 | 0.12 | 0. |
| UISVX | .100 | -0.08 | 0.01 |
| UISVY | -.100 | 0.06 | 0.01 |
| UISVY | .075 | -0.09 | 0.01 |
| UISVZ | -.075 | 0.06 | 0.01 |
| UISVZ | .075 | 11.51 | 0.01 |
| USSVX | .060 | 0.28 | 0.00 |
| USSVX | -.060 | -0.30 | 0.01 |
| USSVY | .060 | 0.94 | -0.00 |
| USSVY | -.060 | -0.93 | 0.01 |
| USSVZ | .060 | 7.53 | -0.03 |
| USSVZ | -.060 | -7.20 | -0.02 |
| SSSVX | .050 | -0.03 | 0.00 |
| SSSVX | -.050 | -0.00 | 0. |
| SSSVY | .050 | -0.02 | -0.00 |
| SSSVY | -.050 | -0.02 | 0. |
| SSSVZ | .050 | -0.05 | -0.00 |
| SSSVZ | -.050 | 0.02 | 0.01 |

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| | DELV1 FT/SEC | DELV2 FT/SEC |
|---------|-----------------|-----------------|
| SFSVX | • 00003 | 9.46 |
| SFSVY | -• 00003 | -9.62 |
| SFSVZ | • 00003 | 1.03 |
| -SFSVZ | -• 00003 | -1.19 |
| ABSVX | • 00003 | 0.00 |
| ABSVY | -• 00003 | -0.02 |
| ABSVZ | • 00003 | -0.02 |
| ABSVZ | -• 00003 | -0.02 |
| ABSVY | • 00003 | -9.61 |
| ABSVY | -• 00003 | -0.95 |
| ABSVZ | • 00003 | 0.89 |
| ABSVZ | -• 00003 | -0.09 |
| CH1X | • 00196 | 0.07 |
| CH1Y | -• 00196 | -0.09 |
| CH1Y | • 00573 | 0.45 |
| CH1Z | -• 00573 | -0.46 |
| CH1Z | • 00156 | 4.36 |
| EPCSVX | -• 00196 | -4.39 |
| EPCSVXZ | • 00834 | -0.79 |
| EPCSVY | -• 00834 | 0.67 |
| EPCSVY | • 00393 | -8.15 |
| EPCSVY | -• 00393 | 8.19 |
| EPCSVYZ | • 00834 | -0.49 |
| EPCSVY | -• 00834 | 0.46 |
| EPCSVYX | • 00278 | -0.47 |
| EPCSVY | -• 00278 | 0.37 |
| EPCSVZ | • 00879 | 0.18 |
| EPCSVZ | -• 00879 | -0.16 |
| EPCSVZ | • 00834 | -0.00 |
| EPCSVZ | -• 00834 | -0.04 |
| RSS | 21.16 | 0.07 |

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TABLE 50

ACTUAL DEVIATIONS
IN SPACECRAFT DELTA-V
DUE TO PERFORMANCE ERRORS

| | DELV1 FT/SEC | DELV2 FT/SEC |
|--------------------|-----------------|-----------------|
| F TSP ¹ | 0. 41 9 | 0. 87 |
| EDWGT ¹ | -0. 41 9 | -0. 89 |
| EDWGT ¹ | 0. 71 6 | 0. 41 |
| EDWGT ¹ | -0. 71 6 | -0. 35 |
| FM ² | 0. 80 6 | -0. 98 |
| FM ² | -0. 80 6 | -1. 97 |
| FFUFL ¹ | 0. 5 | 0. 49 |
| FFUFL ¹ | -0. 5 | -0. 23 |
| FWG ¹ | 2. 84 6 | -0. 68 |
| FWG ¹ | -2. 84 6 | 0. 65 |
| FCF | 10. 0 | -0. 28 |
| FRHQA | -10. 0 | 0. 31 |
| FRHQA | 10. 0 | -0. 32 |
| FISP ¹ | -10. 0 | 0. 29 |
| FISP ¹ | 0. 42 7 | 0. 82 |
| FDWG ² | -0. 42 7 | -0. 84 |
| FDWG ² | 1. 34 | 0. 42 |
| FM ² | -1. 34 | -0. 65 |
| FM ² | 0. 89 5 | 0. 23 |
| FM ² | -0. 89 5 | -0. 44 |
| FFUFL ² | 0. 5 | 0. 12 |
| FWG ² | -0. 5 | -0. 08 |
| FWG ² | 2. 40 7 | -0. 79 |
| FISP ² | 0. 93 9 | 0. 84 |
| FISP ² | -0. 93 9 | -0. 09 |
| EDWGT ² | 2. 0 | 0. 13 |
| EM ² | -2. 0 | -1. 88 |
| EM ² | 2. 0 | 2. 1 9 |
| EM ² | -2. 0 | -0. 12 |

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DELV?
 FT/SEC
 DELV?
 FT/SEC

| | | | |
|---------------------|--------|--------|-------|
| FFI/FL ² | 1.0 | 0.09 | 0.00 |
| FHG12 | -1.0 | -0.15 | 0.01 |
| FHG12 | 1.93e | C.C5 | -C.C0 |
| FHG12 | -1.93e | -0.13 | C.C1 |
| FCFFF1 | * C3 | -0.02 | -0.00 |
| FCFFF1 | -0.02 | 0.01 | 0.00 |
| FCFFF2 | * 02 | -2.03 | 0.01 |
| FCFFF2 | -* C3 | 2.04 | -0.01 |
| FILAGF | 5.0 | 0.03 | -0.00 |
| FILAGF | -5.0 | 0.09 | -0.00 |
| FVENTR | 20.0 | -13.26 | -0.00 |
| FVENTR | -?C.C | 13.40 | 0.01 |
| RSS | | 14.C1 | C.C7 |

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TABLE 31

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
IN SPACECRAFT DELTA-V

DELV1

DELV1 1.76E+01 -0.2

DELV2 -1.04E-01 3.11E-02

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TABLE 52

ACTUAL DEVIATIONS AT RE-ENTRY
WITHOUT SPACECRAFT BURNS
DUE TO PLATFORM ERRORS

| | LAT DEG | LEN DEG | V FT/SEC | BETA E-3 DEG | ALFA E-3 DEG | CRNM NM | DRNM NM |
|-------|------------|------------|-------------|-----------------|-----------------|------------|------------|
| GDSVX | .100 | -0.110 | 0.072 | -13.44 | -40.9 | -93.7 | -1.27 |
| GDSVY | -.100 | 0.110 | -0.075 | 13.43 | 40.9 | 94.0 | 1.45 |
| GDSVZ | -.075 | -0.024 | 0.292 | -8.10 | 24.2 | -5.7 | -14.57 |
| GSSVX | -.075 | 0.025 | -0.290 | 7.98 | -23.8 | 6.0 | 14.51 |
| GSSVZ | -.075 | -0.212 | 0.219 | -29.85 | -88.4 | -198.5 | -6.54 |
| USSVX | -.075 | 0.210 | -0.228 | 29.67 | 89.1 | 190.2 | 7.20 |
| USSVY | -.100 | -0.009 | 0.006 | -0.99 | -2.9 | -6.4 | -0.09 |
| USSVZ | -.100 | 0.009 | -0.005 | 0.98 | 2.9 | 6.4 | 0.08 |
| UISVX | -.075 | -0.002 | 0.010 | -0.43 | -0.7 | -5.7 | -0.46 |
| UISVY | -.075 | 0.002 | -0.007 | 0.29 | 0.7 | 5.7 | 0.30 |
| UISVZ | -.100 | 0.001 | 0.000 | 0.12 | 0.7 | 1.3 | -0.06 |
| U0SVX | -.100 | -0.001 | -0.001 | -0.11 | -0.7 | -1.3 | 0.07 |
| U0SVY | -.100 | 0.001 | -0.000 | 0.06 | 0.2 | 0.6 | -0.00 |
| U0SVZ | -.100 | -0.001 | -0.000 | -0.05 | -0.2 | -0.5 | 0.01 |
| U1SVX | -.100 | -0.001 | -0.000 | 0.05 | -0.1 | 0.0 | -0.08 |
| U1SVY | -.075 | 0.000 | -0.002 | 0.05 | -0.1 | 0.1 | -0.07 |
| U1SVZ | -.075 | -0.001 | 0.001 | -0.03 | 0.2 | -0.1 | -4.99 |
| U2SVX | -.075 | 0.000 | -0.001 | 0.014 | -8.27 | -19.5 | -0.74 |
| U2SVY | -.075 | 0.042 | -0.115 | 8.27 | 19.6 | 29.0 | -0.73 |
| U2SVZ | -.060 | -0.002 | 0.001 | -0.20 | -0.4 | -0.5 | -0.06 |
| U3SVX | -.060 | 0.002 | -0.002 | 0.21 | 0.4 | 0.6 | -0.06 |
| U3SVY | -.060 | -0.003 | 0.014 | -0.59 | 0.1 | -6.0 | -0.10 |
| U3SVZ | -.060 | 0.003 | -0.017 | 0.59 | -0.1 | 6.0 | 0.10 |
| U4SVX | -.050 | 0.002 | -0.001 | -5.33 | -11.6 | -14.1 | 0.51 |
| U4SVY | -.050 | -0.023 | 0.017 | -0.81 | 5.16 | 11.5 | -6.49 |
| U4SVZ | -.050 | 0.000 | -0.017 | 0.00 | 0.2 | 6.0 | -0.00 |
| U5SVX | -.050 | 0.000 | -0.000 | -0.00 | -0.1 | -0.1 | 0.02 |
| U5SVY | -.050 | 0.000 | -0.000 | 0.01 | 0.1 | 0.0 | -0.00 |
| U5SVZ | -.050 | 0.000 | -0.000 | 0.05 | 0.3 | -0.05 | -0.02 |
| U6SVX | -.050 | 0.000 | -0.001 | -0.03 | -0.2 | 0.0 | 0.02 |
| U6SVY | -.050 | 0.000 | -0.000 | 0.01 | 0.1 | 0.0 | -0.00 |
| U6SVZ | -.050 | 0.000 | -0.001 | -0.03 | -0.5 | 0.0 | 0.04 |

| | LAT DEG | LON DEG | V FT/SEC | BETA E-3 DEG | AL FA E-3 DEG | CRNM NM | DR NM NM |
|--------|------------|------------|-------------|-----------------|------------------|------------|-------------|
| SFSVX | * 000003 | -0. 027 | 0. 118 | -6. 96 | -18. 9 | -14. 5 | -5. 54 |
| SFSVY | - 000003 | 0. 028 | -0. 121 | 7. 09 | 19. 4 | 14. 5 | 5. 57 |
| SFSVZ | * 000003 | -0. 004 | 0. 012 | -0. 82 | -3. 5 | -2. 4 | -0. 53 |
| SFSVZ | - 000003 | 0. 004 | -0. 013 | 0. 88 | 3. 6 | 2. 6 | 0. 57 |
| ABSVX | * 000003 | 0. 000 | -0. 000 | -0. 00 | 0. 0 | -0. 0 | -0. 00 |
| ABSVX | - 000003 | -0. 000 | -0. 000 | 0. 01 | 0. 0 | -0. 00 | 0. 00 |
| ABSVX | * 000002 | -0. 026 | 0. 121 | -6. 95 | -17. 6 | -13. 6 | -5. 71 |
| ABSVX | - 000003 | 0. 026 | -0. 123 | 7. 02 | 17. 8 | 13. 8 | 5. 80 |
| ABSVY | * 000003 | 0. 003 | -0. 007 | 0. 59 | -0. 0 | 2. 6 | -0. 04 |
| ABSVY | - 000003 | -0. 003 | 0. 007 | -0. 55 | 0. 2 | -2. 5 | 0. 03 |
| ABSVZ | * 000003 | -0. 001 | -0. 001 | 0. 04 | -0. 4 | -2. 0 | -0. 05 |
| ABSVZ | - 000003 | 0. 001 | 0. 001 | -0. 02 | 0. 4 | 2. 1 | 0. 05 |
| CHI1X | * 001 96 | -0. 001 | 0. 000 | -0. 04 | 0. 0 | 0. 3 | 0. 04 |
| CHI1Y | * 005 73 | -0. 002 | 0. 006 | 0. 05 | 0. 0 | -0. 3 | -0. 04 |
| CHI1Y | - 005 72 | 0. 002 | -0. 007 | -0. 33 | -0. 9 | -5. 8 | -0. 16 |
| CHI1Z | * 001 96 | -0. 013 | 0. 051 | -3. 12 | -7. 3 | -7. 5 | 0. 16 |
| CHI1Z | - 001 95 | 0. 013 | -0. 052 | 3. 14 | 7. 4 | 7. 5 | 0. 31 |
| EPSVXZ | * 008 34 | -0. 000 | -0. 011 | 0. 42 | -0. 7 | -0. 4 | -0. 30 |
| EPSVXZ | - 008 34 | 0. 000 | 0. 011 | -0. 39 | 0. 7 | 5. 9 | 0. 30 |
| EPSVXY | * 003 93 | 0. 025 | -0. 102 | 6. 09 | 17. 8 | 13. 3 | -0. 01 |
| EPSVXY | - 003 93 | -0. 025 | 0. 101 | -6. 06 | -17. 6 | -13. 2 | -0. 57 |
| EPSVYZ | * 008 34 | 0. 003 | -0. 002 | 0. 36 | 1. 1 | 2. 6 | 4. 75 |
| EPSVYZ | - 008 34 | -0. 003 | 0. 002 | -0. 35 | -1. 1 | -2. 6 | -0. 03 |
| EPSVYX | * 002 78 | 0. 001 | -0. 002 | 0. 19 | -2. 0 | 1. 3 | -0. 00 |
| EPSVYX | - 002 78 | -0. 001 | 0. 001 | -0. 11 | 2. 2 | -1. 1 | -0. 01 |
| EPSVZY | * 008 79 | -0. 000 | 0. 000 | -0. 17 | -1. 2 | -4. 3 | -0. 02 |
| EPSVZY | - 008 79 | 0. 000 | -0. 000 | 0. 17 | 1. 2 | 4. 3 | -0. 01 |
| FPSVZX | * 008 34 | 0. 003 | 0. 001 | 0. 10 | 2. 1 | 9. 0 | 0. 01 |
| FPSVZX | - 008 34 | -0. 003 | -0. 002 | -0. 07 | -2. 1 | -8. 9 | -0. 13 |
| RSS | | 0. 250 | | 0. 455 | 37. 20 | 108. 7 | 216. 8 |
| | | | | | | 2. 67 | 20. 14 |

TABLE 53

ACTUAL DEVIATIONS AT RE-ENTRY
WITHOUT SPACECRAFT BURNS
DUE TO PLATFORM ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SEC | TIME SEC |
|-------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| GDSVX | • 100 | -99874• | -9503• | -3.92 | 128.24 | 14.08 | -80.654 |
| GDSVY | -100 | 99498• | 9007• | 3.44 | -127.74 | -13.86 | 81.177 |
| GDSVY | • 075 | 29476• | 325• | -11.81 | -25.55 | -30.27 | -46.326 |
| GDSVZ | -075 | -29075• | -348• | -19817• | 25.21 | 30.26 | 45.898 |
| GDSVZ | • 075 | -197178• | -18951• | 12741• | -11.89 | 249.10 | -178.178 |
| USSVX | -075 | 196503• | 17067• | -12929• | 1.9.89 | -247.82 | -25.98 |
| USSVX | • 100 | -7434• | -719• | 830• | -0.25 | 9.50 | 1.28 |
| USSVY | -100 | 7401• | 713• | -823• | 0.24 | -9.57 | -1.26 |
| USSVY | • 075 | -536• | -104• | 542• | -0.56 | 0.80 | -2.98 |
| USSVZ | -075 | 428• | 95• | -540• | 0.43 | -0.65 | 3.06 |
| USSVZ | • 100 | 1342• | 121• | -74• | -0.00 | -1.65 | -0.16 |
| UISVX | -100 | -1288• | -116• | 71• | 0.01 | 1.58 | 0.15 |
| UISVX | • 100 | 519• | 52• | -76• | 0.01 | -0.67 | -0.02 |
| UISVY | -100 | -450• | -46• | 70• | -0.00 | 0.59 | 0.01 |
| UISVY | • 075 | -110• | 2• | -109• | 0.07 | 0.09 | 0.11 |
| UISVY | -075 | 198• | 6• | 98• | -0.05 | -0.19 | -0.13 |
| UISVZ | • 075 | -35548• | -3453• | 3893• | -4.90 | 42.99 | -6.91 |
| UISVZ | -075 | 35507• | 3290• | -3906• | 4.85 | -42.92 | -6.89 |
| USSVX | • 060 | -1444• | -146• | 225• | -0.03 | 1.91 | 0.62 |
| USSVY | -060 | 1446• | 149• | -254• | 0.04 | -1.91 | -0.60 |
| USSVY | • 060 | 595• | -94• | 1340• | -0.87 | -0.25 | -4.24 |
| USSVZ | -060 | -591• | 95• | -1339• | 0.87 | 0.24 | 4.24 |
| USSVZ | • 060 | -18854• | -1859• | 2391• | -3.55 | 22.15 | 4.21 |
| SSVX | -060 | 18590• | 1822• | -2407• | 3.40 | -21.82 | -4.07 |
| SSVX | • 050 | 191• | 20• | -31• | 0.01 | -0.25 | -0.00 |
| SSVX | -050 | -110• | -12• | 23• | 0.01 | 0.16 | -0.01 |
| SSVY | • 050 | 22• | 4• | -14• | 0.01 | -0.03 | 0.01 |
| SSVY | -050 | 78• | 7• | 3• | 0.01 | -0.08 | 0.02 |
| SSVZ | • 050 | 535• | 49• | -30• | -0.00 | -0.55 | -0.07 |
| SSVZ | -050 | -459• | -41• | 22• | 0.02 | 0.56 | 0.05 |

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SEC | TIME SEC |
|---------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| SFSVX | • 00003 | -21531• | -21531• | -5.12 | 22.15 | 5.21 | -41.687 |
| SFSVY | -• 00003 | 21996• | 21777• | -5.20 | -22.62 | -5.43 | 42.631 |
| SFSVZ | • 00003 | -3366• | -326• | -0.56 | 3.15 | 0.73 | -4.958 |
| SFSVZ | -• 00003 | 3551• | 345• | -4.06• | 0.60 | -3.37 | 5.280 |
| ABSVX | • 00003 | -14• | 5• | -64• | 0.00 | 0.01 | -0.008 |
| ABSVY | -• 00003 | 57• | -2• | 63• | 0.00 | -0.07 | -0.062 |
| ABSVZ | • 00003 | -20219• | -2023• | 2834• | -5.21 | 20.95 | -41.484 |
| ABSVX | -• 00003 | 20486• | 2030• | -2874• | 5.25 | -21.21 | -5.06 |
| ABSVY | • 00003 | 2767• | 264• | -279• | 0.27 | -4.23 | -0.44 |
| ABSVZ | -• 00003 | -2616• | -249• | 260• | -0.24 | 4.07 | 0.41 |
| ABSVZ | • 00003 | -149• | -37• | 229• | -0.02 | 0.15 | -1.13 |
| CH11X | -• 00003 | 211• | 42• | -233• | 0.03 | -0.22 | 1.11 |
| CH11Y | • 00196 | -300• | -39• | -130• | 0.01 | 0.43 | 0.25 |
| CH11Y | -• 00196 | 336• | 43• | -132• | -0.00 | -0.48 | -0.36 |
| CH11Z | • 00573 | -770• | -102• | 341• | -0.44 | 1.00 | -2.82 |
| CH11Z | -• 00573 | 803• | 105• | -343• | 0.44 | -1.04 | 2.83 |
| EP SVXZ | • 00196 | -10405• | -1033• | 1402• | -2.17 | 11.74 | 2.42 |
| EP SVXZ | -• 00196 | 10483• | 1036• | -1414• | 2.18 | -11.82 | -2.44 |
| EP SVYX | • 00834 | -385• | -32• | 1• | 0.43 | 0.17 | 0.01 |
| EP SVYX | -• 00834 | 458• | 40• | -9• | -0.41 | -0.25 | -0.03 |
| EP SVYX | • 00393 | 19656• | 1942• | -2692• | 4.42 | -19.95 | -4.77 |
| EP SVYX | -• 00293 | -19515• | -1946• | 2674• | -4.41 | 19.80 | 4.75 |
| EP SVYZ | • 00834 | 2658• | 241• | -154• | 0.11 | -3.40 | -0.33 |
| EP SVYZ | -• 00834 | -2577• | -234• | 147• | -0.10 | 3.30 | 0.31 |
| EP SVYX | • 00278 | 1091• | 105• | -115• | -0.01 | -2.79 | -0.11 |
| EP SVYX | -• 00278 | -821• | -78• | 82• | 0.06 | 2.50 | 0.05 |
| EP SVZY | • 00879 | -1389• | -74• | -396• | -0.14 | 1.54 | -1.25 |
| EP SVZY | -• 00879 | 1401• | 76• | 397• | 0.14 | -1.55 | 1.25 |
| EP SVZX | • 00834 | 1682• | 196• | -497• | 0.23 | -1.82 | 4.05 |
| EP SVZX | -• 00834 | -1569• | -185• | 485• | -0.20 | 1.69 | -0.48 |
| RSS | | 229862. | 21907. | 25931. | 20.34 | 288.34 | 44.89 |
| | | | | | | 273.797 | |

TABLE 54

ACTUAL DEVIATIONS AT RE-ENTRY
WITHOUT SPACECRAFT BURNS
DUE TO PERFORMANCE ERRORS

| | LAT DEG | LBN DEG | V FT/SFC | BETA F-3 DEG | ALFA F-3 DEG | CRNM NM | DRNM NM |
|--------------------|------------|------------|-------------|-----------------|-----------------|------------|------------|
| FISP ¹ | 0.419 | -0.001 | 0.005 | -0.33 | -1.7 | 1.6 | -0.73 |
| | -0.419 | 0.001 | -0.005 | 0.34 | 1.7 | -2.5 | 0.24 |
| EDWGT ¹ | 0.716 | -0.001 | 0.005 | -0.9 | -0.9 | 0.5 | -0.25 |
| | -0.716 | 0.000 | -0.004 | 0.12 | 0.6 | -1.2 | 0.20 |
| FM ¹ | 0.895 | C. C01 | -C. 006 | C.45 | 2.4 | -3.9 | C.30 |
| | -0.895 | C. C01 | -C. CC8 | 0.72 | 3.7 | -6.5 | C.41 |
| FFUEL ¹ | 0.5 | -0.001 | 0.002 | -0.24 | -1.1 | 0.4 | -0.05 |
| | -0.5 | 0.000 | 0.000 | 0.09 | 0.5 | -1.2 | -0.01 |
| FWGT ¹ | 2.846 | 0.000 | -0.004 | 0.26 | 1.4 | -2.1 | -0.10 |
| | -2.846 | -0.001 | 0.003 | -0.23 | -1.3 | 1.4 | 0.19 |
| FCD | 10.0 | 0.000 | -0.001 | 0.09 | 0.5 | -0.9 | -0.06 |
| | -10.0 | -0.000 | 0.002 | -0.11 | -0.6 | 0.7 | -0.08 |
| FRHPA | 10.0 | 0.000 | -0.002 | 0.14 | 0.6 | -0.6 | 0.10 |
| | -10.0 | -0.000 | 0.002 | -0.12 | -0.5 | 0.5 | -0.07 |
| FISP ² | 0.427 | -0.001 | 0.003 | -0.30 | -1.6 | 1.7 | 0.06 |
| | -0.427 | 0.000 | -0.002 | 0.21 | 1.6 | -2.6 | -0.12 |
| EDWGT ² | 1.24 | -0.000 | 0.011 | -0.16 | -0.8 | 1.1 | -0.57 |
| | -1.24 | 0.001 | -0.013 | 0.30 | 1.2 | -1.4 | 0.57 |
| FM ² | 0.895 | -C. C0C | 0.004 | -0.07 | -0.4 | 0.7 | -0.20 |
| | -0.895 | C. C01 | -0.006 | 0.19 | 0.9 | -C. 9 | 0.31 |
| FFUEL ² | 0.5 | -0.000 | -0.004 | -0.06 | -0.2 | 0.2 | 0.20 |
| | -0.5 | -0.000 | 0.004 | 0.02 | 0.2 | -0.4 | -0.23 |
| FWGT ² | 2.402 | 0.001 | -0.003 | 0.29 | 1.5 | -2.3 | -0.12 |
| | -2.402 | -0.001 | 0.004 | -0.33 | -1.6 | 1.4 | 0.16 |
| FISP ³ | 0.939 | 0.000 | 0.004 | -0.13 | -0.5 | 1.4 | -0.22 |
| | -0.939 | -0.001 | -0.004 | 0.11 | 0.4 | -1.8 | 0.20 |
| EDWGT ³ | 2.0 | 0.005 | 0.016 | -0.01 | 1.0 | 7.4 | -0.67 |
| | -2.0 | -0.008 | -0.018 | 0.01 | -1.4 | -1.0 | -0.14 |
| FM ³ | 2.0 | C. CC2 | C. CC5 | -0.01 | 0.1 | 4.6 | C.10 |
| | -2.0 | -C. CC3 | -C. CC3 | C.01 | -0.1 | -6.5 | -C. 13 |

| | LAT DEG | LON DEG | V FT/SEC | BETA E-3 DFG | ALFA E-3 DFG | CRNM NM | DRNM NM |
|--------|------------|------------|-------------|-----------------|-----------------|------------|------------|
| EFUFL3 | 1.0 | -0.003 | -0.007 | -0.4 | -5.9 | -C.17 | 0.16 |
| | -1.0 | 0.002 | 0.002 | 0.5 | 4.6 | C.C8 | -0.15 |
| FWGTR2 | 1.936 | -0.003 | -0.002 | -0.4 | -6.1 | -C.12 | C.17 |
| | -1.936 | 0.003 | 0.002 | 0.4 | 4.7 | C.C8 | -C.18 |
| F40FF1 | 0.02 | -0.000 | -0.004 | 0.01 | 0.0 | -0.01 | 0.19 |
| | -0.02 | 0.000 | 0.004 | -0.00 | 0.0 | C.C1 | -0.19 |
| F40FF2 | 0.03 | 0.006 | -0.017 | 1.40 | 2.2 | 6.1 | -0.23 |
| | -0.03 | -0.006 | 0.018 | -1.40 | -2.2 | -6.1 | 0.78 |
| EULAGF | 5.0 | 0.000 | 0.001 | -0.02 | 0.0 | 0.0 | -0.03 |
| | -5.0 | -0.000 | 0.001 | -0.05 | -0.1 | -0.1 | 0.06 |
| FVFNTR | 20.0 | 0.065 | -0.130 | 10.93 | 50.6 | 42.8 | 5.20 |
| | -20.0 | -0.065 | 0.129 | -10.95 | -50.4 | -43.6 | -5.25 |
| RSS | | 0.C66 | C.134 | 11.10 | 51.0 | 47.7 | 1.21 |
| | | | | | | | 5.58 |

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TABLE 55

ACTUAL DEVIATIONS AT RE-ENTRY
WITHOUT SPACECRAFT BURNS
DUE TO PERFORMANCE ERRORS

| | RPX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | Vpz FT/SEC | TIME SEC |
|--------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| FISP1 | 0.419 | -2068. | -140. | -0.05 | 1.94 | 2.39 | -2.594 |
| | -0.419 | 2092. | 122. | 0.02 | -1.98 | -3.01 | 2.679 |
| FDWGT1 | 0.716 | -1.067. | -79. | -0.07 | 1.02 | 1.02 | -1.915 |
| | -0.716 | 735. | 29. | 0.00 | -0.65 | -1.22 | 1.677 |
| FM1 | 0.895 | 2852. | 156. | 0.00 | -2.49 | -4.38 | 3.482 |
| | -0.895 | 4476. | 237. | 0.01 | -3.91 | -7.12 | 5.158 |
| FFUEL1 | 0.5 | -1307. | -101. | -0.09 | 1.25 | 1.10 | -1.372 |
| | -0.5 | 676. | 21. | 0.02 | -0.59 | -1.24 | 0.429 |
| FWGT1 | 2.846 | 1657. | 95. | 0.01 | -1.46 | -2.41 | 2.029 |
| | -2.846 | -1605. | -101. | -0.01 | 1.47 | 1.59 | -1.914 |
| FCN | 10.0 | 627. | 33. | 1.82. | -0.02 | -0.56 | -1.01 |
| | -10.0 | -714. | -46. | -1.35. | -0.02 | 0.67 | 0.734 |
| FRHQA | 10.0 | 730. | 50. | 1.14. | 0.04 | -0.69 | -0.890 |
| | -10.0 | -722. | -51. | -0.95. | -0.02 | 0.70 | 1.004 |
| FISP2 | 0.427 | -1935. | -127. | -345. | -0.03 | 1.79 | -0.877 |
| | -0.427 | 1970. | 111. | 513. | 0.01 | -1.76 | -2.027 |
| FDWGT2 | 1.26 | -1.007. | -61. | -224. | -0.01 | 0.92 | -2.024 |
| | -1.34 | 1584. | 103. | 285. | 0.08 | -1.43 | -2.024 |
| FM2 | 0.895 | -523. | -31. | -132. | 0.02 | 0.48 | -1.303 |
| | -0.895 | 1046. | 70. | 173. | 0.04 | -0.96 | 2.192 |
| FFLFL2 | 0.5 | -324. | -22. | -49. | -0.01 | 0.28 | -3.363 |
| | -0.5 | 207. | 8. | 85. | -0.02 | -0.16 | 4.246 |
| FGCT2 | 2.402 | 1898. | 110. | 468. | 0.01 | -1.71 | -2.023 |
| | -2.402 | -2008. | -138. | -298. | -0.06 | 1.89 | -2.221 |
| FISP3 | 0.920 | -446. | -4. | -212. | -0.04 | 0.27 | -0.901 |
| | -0.920 | 343. | -11. | 371. | 0.01 | -0.14 | 1.341 |
| FDWGT3 | 2.0 | 305. | 1701. | -1494. | 0.02 | -2.51 | -1.193 |
| | -3.0 | -2397. | -437. | 2170. | -0.07 | 2.57 | -3.136 |
| FM3 | 2.0 | 91. | 98. | -842. | 0.13 | -0.44 | -1.276 |
| | -2.0 | -132. | 1212. | -112. | -0.21 | 0.51 | 0.981 |

| | R PY FT | R PT FT | V PY FT/SFC | V PT FT/SFC | V PZ FT/SFC | V PY FT/SFC | V PT FT/SFC | TIME SFC |
|--------|------------|------------|----------------|----------------|----------------|----------------|----------------|-------------|
| FFUFL2 | 1.0 | -145. | 1067. | -0.23 | 0.78 | -2.44 | 0.442 | |
| FWGT2 | -1.0 | 489. | 130. | 0.19 | -0.80 | 2.52 | -0.343 | |
| F4OFF1 | 1.936 | -388. | -153. | -0.24 | 0.83 | -3.57 | 0.442 | |
| F4OFF2 | -1.936 | 442. | 128. | 0.18 | -0.78 | 2.61 | -0.479 | |
| EULAGF | 0.02 | 51. | 25. | -0.00 | -0.05 | -0.10 | 0.84 | |
| EVENTR | -0.02 | -17. | -24. | 0.01 | 0.00 | 0.10 | -0.853 | |
| | -0.02 | 6397. | 553. | -122. | 0.75 | -1.07 | 8.225 | |
| | -0.02 | -6420. | -556. | 122. | -0.75 | 1.07 | -8.359 | |
| | -0.02 | 13. | 7. | -0.02 | -0.02 | 0.00 | -0.125 | |
| | -5.0 | -109. | 18. | -0.04 | -0.04 | 0.02 | -0.229 | |
| | -5.0 | 55629. | 5227. | -5580. | 6.36 | -10.65 | 66.090 | |
| | -20.0 | -55570. | -5549. | -55367. | -5.48 | -10.68 | -65.846 | |
| RSS | | 56435. | 5433. | 6.53 | 57.01 | 16.69 | 67.319 | |

TABLE 56

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT RE-ENTRY WITHOUT SM BURNS

| LAT | LON | V | BETA | ALFA | CRNM | DRNM |
|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| 8.60E-02 | -0.7 | 1.0 | 0.9 | 1.0 | -0.8 | 0.6 |
| -9.59E-03 | 1.56E-01 | -0.8 | -0.6 | -0.6 | 0.9 | -1.0 |
| 1.09E 00 | -1.69E 00 | 1.29E 01 | 0.9 | 0.9 | -0.9 | 0.7 |
| 3.18E-03 | -3.53E-03 | 4.63E-01 | 3.98E-02 | 0.9 | -0.8 | 0.4 |
| 6.25E-03 | -7.25E-03 | 8.95E-01 | 2.69E-03 | 7.33E-02 | -0.8 | 0.5 |
| -7.03E-02 | 1.41E-01 | -1.16E 01 | -2.93E-02 | -5.43E-02 | 9.65E-01 | -0.9 |
| 3.33E-01 | -1.05E 00 | 6.35E 01 | 1.12E-01 | 2.36E-01 | -5.74E 00 | 6.87E 00 |

TABLE 57

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT RE-ENTRY WITHOUT SM BURNS

| | RPX | RPY | RPZ | VPX | VPY | VPZ | TIME |
|------|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| RPX | 7.89E 04 | 1.0 | -0.5 | 0.7 | -1.0 | -0.8 | 0.9 |
| RPY | 5.88E 08 | 7.51E 03 | -0.6 | 0.7 | -1.0 | -0.7 | 1.0 |
| RPZ | -3.77E 08 | -4.17E 07 | 8.81E 03 | -0.9 | 0.6 | -0.0 | -0.8 |
| VPX | 3.69E 05 | 3.88E 04 | -5.84E 04 | 7.10E 00 | -0.7 | -0.2 | 0.9 |
| VPY | -7.70E 06 | -7.32E 05 | 4.89E 05 | -4.62E 02 | 9.79E 01 | 0.8 | -0.9 |
| VPZ | -9.76E 05 | -8.49E 04 | -4.59E 03 | -2.21E 01 | 1.17E 03 | 1.57E 01 | -0.6 |
| TIME | 5.63E 06 | 5.54E 05 | -5.35E 05 | 4.90E 02 | -7.00E 03 | -7.01E 02 | 7.72E 01 |

TABLE 58

ACTUAL DEVIATIONS AT RE-ENTRY
WITH SPACECRAFT BURNS
DUE TO PLATFORM ERRORS

| | LAT DEG | LON DEG | V FT/SEC | BETA E-3 DEG | ALFA E-3 DEG | CRNM NM | DRNM NM |
|-------|------------|------------|-------------|-----------------|-----------------|------------|------------|
| GUSSX | .100 | -U.010 | -0.020 | -0.01 | -4.9 | 0.45 | 1.39 |
| GUSSY | -.100 | U.017 | U.020 | 0.2 | 5.2 | -0.46 | -1.39 |
| GUSSY | .075 | -0.024 | 0.079 | -0.02 | -11.9 | 0.51 | -3.48 |
| GUSSZ | -.075 | U.030 | -U.078 | 0.03 | 12.3 | -0.51 | 3.42 |
| GUSSZ | .075 | -0.006 | U.013 | -0.00 | 6.4 | 0.49 | -0.53 |
| GUSSZ | -.075 | U.007 | -0.012 | U.01 | -5.8 | -0.49 | 0.47 |
| USSSX | .100 | -U.002 | -U.002 | 0.00 | 0.1 | 0.09 | 0.14 |
| USSSY | -.100 | U.002 | U.002 | 0.01 | -0.0 | -0.08 | -0.14 |
| USSSY | .075 | U.000 | U.005 | 0.00 | -3.5 | -0.18 | -0.26 |
| USSSY | -.075 | -U.000 | -U.004 | 0.00 | 4.0 | 0.18 | 0.20 |
| USSSZ | .100 | U.000 | U.000 | 0.00 | -0.0 | -0.00 | -0.02 |
| USSSZ | -.100 | -U.000 | -U.000 | 0.00 | 0.1 | 0.00 | 0.02 |
| USSSZ | .075 | U.000 | U.000 | 0.00 | -0.1 | -0.00 | -0.01 |
| USSSZ | -.075 | -U.000 | -U.000 | 0.00 | 0.1 | -0.00 | 0.02 |
| USSSY | -.100 | U.000 | -U.001 | U.00 | -0.0 | -0.00 | -0.01 |
| USSSY | .075 | -U.000 | U.000 | U.01 | 0.0 | -0.00 | -0.01 |
| USSSZ | .100 | U.000 | U.000 | U.01 | 19.7 | 0.47 | -2.26 |
| USSSZ | -.100 | -U.000 | -U.000 | U.01 | -19.6 | -0.47 | 2.26 |
| USSSY | .075 | -U.000 | -U.001 | U.00 | 0.6 | 0.05 | 0.05 |
| USSSY | -.075 | U.000 | U.000 | U.01 | -0.6 | -0.06 | -0.04 |
| USSSZ | .100 | U.000 | U.000 | U.01 | -4.4 | -0.16 | -0.35 |
| USSSZ | -.100 | -U.000 | -U.000 | U.01 | 4.4 | 0.16 | 0.34 |
| USSSY | .060 | U.000 | -U.001 | U.00 | 16.4 | 0.34 | -1.40 |
| USSSY | -.060 | -U.000 | U.001 | U.00 | -15.4 | -0.33 | 1.85 |
| USSSZ | .060 | -U.000 | U.000 | U.01 | 0.0 | -0.00 | -0.00 |
| USSSY | -.060 | U.000 | -U.001 | U.00 | 0.0 | -0.1 | 0.01 |
| USSSY | .050 | -U.000 | U.000 | U.00 | 0.0 | -0.0 | 0.00 |
| USSSY | -.050 | U.000 | -U.000 | U.00 | 0.0 | -0.0 | -0.01 |
| USSSZ | .050 | -U.000 | U.000 | U.00 | 0.0 | -0.0 | 0.02 |
| USSSY | -.050 | U.000 | -U.000 | U.00 | 0.0 | -0.0 | -0.00 |

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| | LAT DEG | LUN DEG | V FT/SEC | BETA E-3 DEG | ALFA E-3 DEG | CRNM NM | UKNM NM |
|--------|------------|------------|-------------|-----------------|-----------------|------------|------------|
| SFSVX | • 00003 | 0.018 | 0.064 | 0.02 | 29.8 | 0.48 | -3.72 |
| SFSVY | -• 00003 | -0.018 | -0.065 | -0.01 | -30.2 | -0.49 | 3.78 |
| SFSVZ | • 00003 | 0.013 | 0.009 | 0.01 | 4.4 | 0.06 | -0.55 |
| ABSVX | -• 00003 | -0.003 | -0.010 | -0.00 | -4.0 | -0.06 | 0.57 |
| ABSVY | • 00003 | 0.000 | -0.000 | 0.00 | 0.1 | -0.00 | 0.00 |
| ABSVZ | -• 00003 | 0.000 | 0.000 | 0.00 | -0.1 | 0.00 | -0.00 |
| ABSVY | • 00003 | 0.017 | 0.063 | 0.02 | 28.9 | 0.45 | -3.64 |
| ABSVZ | -• 00003 | -0.018 | -0.063 | -0.01 | -29.1 | -0.46 | 3.67 |
| CHIX | • 00196 | 0.001 | 0.003 | 0.00 | 0.9 | -0.02 | -0.10 |
| CHIY | -• 00196 | -0.001 | -0.003 | -0.00 | -1.1 | 0.02 | 0.18 |
| CHIZ | • 00573 | 0.001 | 0.001 | 0.00 | -1.7 | -0.06 | -0.03 |
| EPSSVX | • 00834 | 0.001 | 0.001 | 0.00 | 0.0 | -0.06 | 0.03 |
| EPSSVY | -• 00834 | -0.010 | -0.023 | 0.01 | -0.5 | -0.06 | -0.03 |
| EPSSVZ | • 00393 | 0.006 | -0.006 | -0.00 | -3.7 | -0.19 | -0.22 |
| EPSSVY | -• 00393 | -0.001 | 0.004 | 0.00 | 1.7 | 0.06 | 0.04 |
| EPSSVZ | • 00834 | 0.001 | -0.004 | -0.00 | 0.5 | 0.04 | 0.03 |
| EPSSVY | -• 00834 | -0.001 | 0.002 | 0.00 | -0.5 | -0.04 | -0.03 |
| EPSSVX | • 00278 | 0.016 | 0.057 | 0.00 | -3.7 | -0.19 | -0.22 |
| EPSSVY | -• 00879 | -0.002 | -0.002 | 0.01 | 1.0 | 0.21 | -1.31 |
| EPSSVZ | • 00834 | 0.000 | 0.004 | 0.00 | -1.1 | -0.21 | 1.32 |
| RSS | | v.048 | 0.148 | 0.06 | 0.5 | 60.2 | 1.40 |
| | | v.048 | 0.148 | 0.06 | 0.5 | 60.2 | 1.40 |

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TABLE 59
ACTUAL DEVIATIONS AT RE-ENTRY
WITH SPACECRAFT BURNS
DUE TO PLATFORM ERRORS

| | KPX FT | KPY FT | KPZ FT | VPX FT/SEC | VPY FT/SEC | Vpz FT/SEC | TIME SEC |
|-------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| GUSVX | .100 | -7858. | -817. | 3656. | 0.94 | 13.50 | 1.85 |
| GUSVY | -.100 | 7942. | 827. | -3746. | -0.94 | -13.04 | -1.74 |
| GUSVZ | .075 | 24106. | -776. | 19450. | -4.40 | -35.81 | -35.29 |
| GUSVZ | -.075 | -23066. | 765. | -19548. | 4.35 | 35.17 | 1.40 |
| GUSVZ | .075 | 4456. | -169. | 3864. | -0.53 | -7.16 | -1.09 |
| GUSVZ | -.075 | -3873. | 294. | -3911. | 0.47 | 6.18 | -0.91 |
| USSVX | .100 | -747. | -98. | 543. | 0.11 | 1.26 | 0.42 |
| USSVX | -.100 | 774. | 99. | -538. | -0.10 | -1.32 | -0.42 |
| USSVY | .075 | 1664. | 50. | 380. | -0.38 | -2.43 | -3.74 |
| USSVY | -.075 | -1309. | -29. | -399. | 0.34 | 1.80 | 3.73 |
| USSVZ | .100 | 116. | 8. | -19. | -0.91 | -0.19 | -0.01 |
| USSVZ | -.100 | -125. | -9. | 19. | 0.02 | 0.22 | 0.01 |
| UISVX | .100 | 42. | 8. | -54. | 0.00 | -0.08 | 0.05 |
| UISVX | -.100 | -104. | -11. | 55. | 0.01 | 0.18 | -0.04 |
| UISVY | .075 | -157. | 3. | -105. | 0.03 | 0.25 | 0.15 |
| UISVY | -.075 | 92. | -6. | 101. | -0.01 | -0.12 | -0.14 |
| UISVZ | .075 | 14165. | 586. | 1094. | -1.50 | -24.03 | -0.02 |
| UISVZ | -.075 | -14091. | -291. | -1699. | 1.48 | 23.90 | 0.00 |
| UUSVX | .060 | -306. | -37. | 184. | 0.06 | 0.47 | 0.52 |
| UUSVX | -.060 | 235. | 35. | -210. | -0.05 | -0.37 | -0.48 |
| UUSVY | .060 | 231. | 1. | 1180. | -0.52 | -3.01 | -5.13 |
| UUSVY | -.060 | -2298. | 0. | -1180. | 0.52 | 3.28 | 5.13 |
| UUSVZ | .060 | 12174. | 551. | 1014. | -1.30 | -20.65 | -0.19 |
| UUSVZ | -.060 | -11334. | -505. | -1075. | 1.20 | 19.24 | 0.15 |
| SSVX | .050 | 25. | 4. | -24. | -0.00 | -0.04 | 0.02 |
| SSVY | -.050 | -75. | -7. | 21. | 0.01 | 0.13 | -0.02 |
| SSVY | .050 | -31. | -1. | -11. | 0.00 | 0.06 | 0.02 |
| SSVZ | -.050 | -5. | 6. | -8. | 0.00 | 0.02 | -0.02 |
| SSVZ | .050 | 40. | 3. | -5. | -0.01 | -0.07 | -0.03 |
| | -.050 | -88. | 6. | 0.02 | 0.02 | 0.15 | 0.01 |

| | KPX FT | KPY FT | KPZ FT | VPX FT/SEC | VPY FT/SEC | Vpz FT/SEC | TIME SEC |
|--------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| SFSVX | .00003 | 4343. | 1151. | 989. | -2.54 | -39.63 | 0.193 |
| | -.00003 | -23070. | -1193. | -1011. | 2.54 | 40.19 | 0.96 |
| SFSVY | .00003 | 3517. | 183. | 72. | -0.38 | -2.96 | -0.18 |
| | -.00003 | -3669. | -192. | -79. | 0.46 | 6.25 | 0.19 |
| SFSVZ | .00003 | 0. | 7. | -65. | 0.00 | -0.02 | 0.08 |
| | -.00003 | 17. | -6. | 64. | -0.01 | -0.01 | -0.08 |
| ABSVX | .00003 | 22901. | 1137. | 900. | -2.49 | -38.87 | -1.09 |
| | -.00003 | -23049. | -1169. | -916. | 2.48 | 39.13 | 1.08 |
| ABSVY | .00003 | 948. | 73. | -203. | -0.11 | -1.03 | -0.15 |
| | -.00003 | -1104. | -81. | 198. | 0.13 | 1.89 | 0.16 |
| ABSVZ | .00003 | 214. | -9. | 190. | -0.09 | -0.21 | -1.31 |
| | -.00003 | -228. | 8. | -191. | 0.10 | 0.24 | 1.31 |
| CH11X | .00196 | -162. | -23. | 132. | 0.04 | 0.27 | 0.37 |
| | -.00196 | 146. | 22. | -131. | -0.04 | -0.22 | -0.37 |
| CH11Y | .00573 | 1418. | 58. | 182. | -0.34 | -2.02 | -3.55 |
| | -.00573 | -1436. | -59. | -182. | 0.35 | 2.04 | 3.55 |
| CH11Z | .00196 | 8386. | 395. | 565. | -0.90 | -14.22 | -0.23 |
| | -.00196 | -8431. | -400. | -570. | 0.90 | 14.33 | 0.23 |
| EPSVXL | .00834 | -834. | -48. | 23. | 0.10 | 1.42 | 0.16 |
| | -.00834 | 758. | 44. | -25. | -0.08 | -1.27 | -0.16 |
| EPSVXY | .00393 | -20903. | -1055. | -869. | 2.23 | 35.48 | 0.84 |
| | -.00393 | 21201. | 1052. | 849. | -2.31 | -36.01 | -0.90 |
| EPSVYZ | .00834 | 170. | 14. | -43. | -0.01 | -0.28 | 0.01 |
| | -.00834 | -190. | -15. | 41. | 0.03 | 0.35 | -0.01 |
| EPSVYX | .00278 | 2968. | 183. | -207. | -0.33 | -5.96 | -0.31 |
| | -.00278 | -3178. | -194. | 195. | 0.36 | 5.43 | 0.32 |
| EPSVZY | .00879 | 697. | 94. | -522. | -0.16 | -1.02 | -1.71 |
| | -.00879 | -640. | -91. | 521. | 0.17 | 0.95 | 1.71 |
| EPSVZX | .00834 | -1282. | -40. | -278. | 0.41 | 1.06 | 4.97 |
| | -.00834 | 1190. | 35. | 275. | -0.39 | -1.48 | -4.97 |
| | | | | | | | -0.024 |
| | | | | | | | 1.549 |
| RSS | 51610. | 2480. | 20515. | 6.70 | 85.29 | 36.55 | |

TABLE 50

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ACTUAL DEVIATIONS AT RE-ENTRY
WITH SPACECRAFT BURNS
DUE TO PERFORMANCE ERRORS

| | LAT DEG | LAN DEG | V FT/SEC | BETA E-2 DEG | ALFA F-2 DFG | CRNM NM | DRNM NM |
|--------------------|------------|------------|-------------|-----------------|-----------------|------------|------------|
| EISP ¹ | 0.419 | 0.003 | 0.006 | 0.01 | 5.5 | -0.19 | -0.40 |
| | -0.416 | -0.003 | -0.006 | 0.00 | -6.5 | -0.14 | 0.40 |
| EDWGT1 | 0.716 | 0.001 | 0.005 | 0.01 | 2.5 | 0.05 | -0.20 |
| | -0.716 | -0.001 | -0.004 | 0.00 | -2.6 | -0.05 | 0.25 |
| FM1 | 0.895 | -0.005 | -0.004 | -0.00 | -9.4 | -0.20 | 0.55 |
| | -0.895 | 0.012 | -0.00 | -0.1 | -15.1 | -0.33 | 0.76 |
| FFUEL ¹ | 0.5 | 0.001 | 0.002 | 0.01 | 2.8 | 0.06 | -0.15 |
| | -0.5 | -0.001 | -0.001 | 0.00 | -2.6 | -0.06 | 0.06 |
| FWGT ¹ | 2.846 | -0.003 | -0.005 | -0.00 | -5.2 | -0.11 | 0.32 |
| | -2.846 | 0.002 | 0.005 | 0.1 | 4.5 | -0.05 | -0.21 |
| ECD | 10.0 | -0.001 | -0.002 | 0.00 | -2.1 | -0.05 | 0.13 |
| | -10.0 | 0.001 | 0.002 | 0.00 | 2.0 | 0.04 | -0.14 |
| ERHOA | 10.0 | -0.001 | -0.002 | 0.00 | -2.0 | -0.04 | 0.14 |
| | -10.0 | 0.001 | 0.002 | 0.01 | 1.8 | 0.04 | -0.17 |
| EISP2 | 0.427 | 0.003 | 0.005 | 0.01 | 5.4 | 0.12 | -0.21 |
| | -0.427 | -0.003 | -0.005 | -0.00 | -6.4 | -0.14 | 0.31 |
| EDWGT2 | 1.34 | 0.002 | 0.002 | 0.00 | 3.0 | 0.05 | -0.65 |
| | -1.34 | -0.002 | -0.004 | -0.00 | -4.5 | -0.08 | 0.76 |
| FM2 | 0.895 | 0.011 | 0.005 | 0.00 | 1.6 | 0.03 | -0.26 |
| | -0.895 | -0.011 | -0.007 | 0.00 | -2.8 | -0.06 | 0.37 |
| EFUFL2 | 0.5 | 0.000 | -0.003 | 0.01 | 0.9 | 0.02 | 0.17 |
| | -0.5 | -0.000 | 0.004 | 0.01 | -0.8 | -0.02 | -0.19 |
| FWGT2 | 2.402 | -0.003 | -0.004 | 0.00 | -5.9 | -0.13 | 0.29 |
| | -2.402 | 0.003 | 0.005 | 0.00 | 5.2 | 0.11 | -0.31 |
| EISP ² | 0.929 | 0.001 | 0.002 | 0.00 | 2.0 | 0.05 | -0.15 |
| | -0.929 | -0.001 | -0.002 | 0.00 | -2.1 | -0.05 | 0.14 |
| EDWGT3 | 3.0 | 0.001 | 0.006 | 0.00 | 3.1 | 0.10 | -0.34 |
| | -3.0 | -0.002 | -0.006 | 0.00 | -5.7 | -0.16 | 0.36 |
| FM3 | 2.0 | 0.002 | 0.004 | 0.00 | 4.4 | 0.11 | -0.24 |
| | -2.0 | -0.003 | -0.006 | -0.00 | -6.4 | -0.16 | 0.19 |

| | LAT DEG | LONG DEG | V FT/SFC | BFTA F-3 DFG | ALFA F-3 DEG | CRNM NM | DRNM NM |
|---------|------------|-------------|-------------|-----------------|-----------------|------------|------------|
| FFUFL2 | 1.0 | -0.002 | 0.00 | -0.0 | -5.2 | -C.14 | 0.14 |
| FAGT2 | -1.0 | 0.001 | 0.002 | 0.0 | 3.7 | C.10 | -0.12 |
| FAGT2 | 1.0 | 0.346 | -C. CC2 | -C. CC2 | -5.5 | -C.14 | C.15 |
| FAGT2 | -1.0 | 0.346 | C. CC2 | C. CC2 | 3.9 | C.10 | -0.15 |
| FLAGFE1 | 0.2 | -0.000 | -0.004 | 0.0 | -0.7 | C.00 | 0.5 |
| FLAGFE1 | -0.2 | 0.000 | 0.004 | 0.0 | 0.2 | -C.00 | -0.10 |
| F40FF2 | 0.2 | -0.001 | -0.001 | 0.0 | -0.8 | 0.01 | 0.08 |
| F40FF2 | -0.2 | 0.001 | 0.001 | 0.0 | 0.8 | -0.01 | 0.0 |
| FULAGE | 5.0 | 0.000 | -0.000 | 0.0 | C.8 | -0.08 | -0.08 |
| FULAGE | -5.0 | 0.000 | 0.000 | 0.0 | 0.0 | 0.00 | 0.00 |
| FVFNTR | 20.0 | -0.032 | -0.110 | -0.03 | -51.1 | C.00 | -0.03 |
| FVFNTR | -20.0 | 0.032 | 0.110 | 0.03 | 51.2 | -C.74 | 5.42 |
| RSS | | C.034 | C.112 | C.4 | 56.5 | 0.94 | 6.60 |

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TABLE 61

ACTUAL DEVIATIONS AT RE-ENTRY
WITH SPACECRAFT BURNS
DUF T0 PERFORMANCE ERRORS

| | RPX FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SFC | TIME SEC |
|--------|-----------|-----------|---------------|---------------|---------------|-------------|
| FISP1 | 0.419 | 1937. | -470. | -0.07 | 2.12 | -0.426 |
| | -0.419 | -1886. | -171. | 0.05 | -2.80 | 0.298 |
| FDWCT1 | 0.716 | 930. | 70. | -0.05 | -1.66 | -0.641 |
| | -0.716 | -719. | -68. | 0.02 | 1.39 | 0.640 |
| FM1 | 0.895 | -2593. | -244. | 0.05 | 4.95 | -4.13 |
| | -0.895 | -4049. | -388. | 0.06 | -6.75 | 0.550 |
| EFUEL1 | 0.5 | 1151. | 82. | -0.07 | -2.06 | 0.88 |
| | -0.5 | -632. | -64. | 0.01 | 1.23 | -1.17 |
| EWGT1 | 2.846 | -1504. | -138. | 0.04 | 2.88 | -4.13 |
| | -2.846 | 1416. | 122. | -0.04 | -2.61 | 0.443 |
| ECD | 10.0 | -574. | -55. | 0.01 | 1.11 | -0.157 |
| | -10.0 | 507. | 52. | -0.02 | -1.14 | 0.157 |
| ERHOA | 10.0 | -691. | 165. | 0.04 | 1.28 | -0.166 |
| | -10.0 | 583. | 47. | -0.02 | -1.08 | 0.166 |
| FISP2 | 0.427 | 1749. | 145. | -0.06 | -3.22 | -0.106 |
| | -0.427 | -1793. | -166. | 0.05 | 3.41 | 0.079 |
| FDWGT2 | 1.24 | 902. | 80. | -0.02 | -1.67 | -2.320 |
| | -1.24 | -1521. | -125. | 0.07 | 2.80 | 2.352 |
| FM2 | 0.895 | 435. | 41. | -0.00 | -0.83 | -0.106 |
| | -0.895 | -935. | -77. | 0.04 | 1.76 | 0.079 |
| FFUFL2 | 0.5 | 304. | 25. | -0.01 | -0.55 | 0.32 |
| | -0.5 | -186. | -20. | 0.01 | 0.38 | -0.37 |
| EWGT2 | 3.402 | -1660. | 588. | 0.04 | 3.17 | -2.56 |
| | -3.402 | 1756. | -142. | -0.08 | -3.24 | 1.03 |
| FISP3 | 0.929 | 80. | 97. | 0.07 | -0.29 | -1.025 |
| | -0.929 | -929. | -153. | -0.07 | 0.24 | 0.085 |
| FDWGT2 | 2.0 | -2.402 | -435. | 0.56 | 4.72 | -0.624 |
| | -2.402 | 3172. | -313. | -0.08 | -4.52 | -6.89 |
| FM2 | 2.0 | -0.929 | -262. | -0.07 | 0.70 | 3.929 |
| | -2.0 | -221. | -40. | -0.07 | 0.20 | -1.242 |
| | -2.0 | 174. | -207. | 0.56 | -4.74 | 0.61 |
| | -2.0 | -110. | -2815. | -0.27 | -4.52 | -4.61 |
| | | | -1799. | -0.70 | -0.01 | |
| | | | -775. | 0.20 | 3.23 | |
| | | | -1127. | -0.27 | 0.27 | |

| | RDX FT | RPY FT | RPZ FT | VPX FT/SEC | VPY FT/SEC | VPZ FT/SFC | TIMF SFC |
|---------|-----------|-----------|-----------|---------------|---------------|---------------|-------------|
| FFUFL 3 | 1.0 | 794. | 973. | -0.24 | -0.00 | -2.07 | 0.947 |
| FHGTR | -1.0 | -491. | -730. | 0.22 | C.47 | 3.00 | -0.937 |
| | | 358. | -88. | -C.26 | -C.10 | -4.14 | C.896 |
| | | -392. | 58. | -749. | 0.21 | C.30 | -C.961 |
| F4OFFF1 | 0.3 | -15. | -4. | 25. | -0.00 | 3.C8 | |
| | | | 1. | -22. | 0.01 | 0.06 | |
| F4OFFF2 | 0.2 | -620. | -55. | 190. | 0.07 | 1.17 | -0.10 |
| | | | 624. | -190. | -0.06 | -0.01 | 0.941 |
| FULAGE | 5.0 | 23. | 1. | -1. | -1.08 | C.11 | |
| | | | 5. | 2. | -0.00 | -0.04 | -0.857 |
| FVFNTR | 20.0 | -2119. | -1237. | 4.25 | 69.08 | C.26 | -0.079 |
| | | 2047. | 1232. | -4.48 | -69.23 | 1.C6 | -0.622 |
| RSS | 41247. | 2193. | 3542. | 4.56 | 70.28 | -1.99 | 0.665 |
| | | | | | | | |
| | | | | | | | 5.4C1 |

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TABLE 02

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT RE-ENTRY WITH 5M BURNS

| | LAT | LEN | V | BETA | ALFA | CRNM | DRNM |
|------|-----------|-----------|-----------|-----------|-----------|-----------|----------|
| LAT | 1.92E-02 | 0.5 | 0.9 | 1.0 | 0.9 | 0.3 | -0.0 |
| LEN | 6.12E-04 | 6.17E-02 | 0.0 | 0.5 | 0.8 | 0.0 | -1.0 |
| V | 3.17E-04 | 6.68E-04 | 1.87E-02 | 0.9 | 0.8 | 0.4 | -0.6 |
| BETA | 3.18E-06 | 5.91E-06 | 3.00E-06 | 1.75E-04 | 0.8 | 0.4 | -0.6 |
| ALFA | 4.44E-04 | 1.33E-03 | 4.18E-04 | 3.97E-06 | 2.68E-02 | 0.8 | -0.9 |
| CRNM | 3.60E-03 | 2.69E-02 | 4.40E-03 | 3.57E-05 | 1.12E-02 | 5.45E-01 | -0.8 |
| DRNM | -3.99E-02 | -2.12E-01 | -4.16E-02 | -3.77E-04 | -7.89E-02 | -1.48E-06 | 3.44E-06 |

TABLE 03

COVARIANCE MATRIX OF ACTUAL DEVIATIONS
AT KEY-ENTRY WITH SM BURNS

| KPX | KPY | KPL | VPX | VPY | VPL | TIME |
|------------|------------|------------|------------|------------|------------|-----------|
| 2.19E .34 | 0.0 | 0.5 | -1.0 | -1.0 | -0.4 | 0.2 |
| 1.89E .37 | 1.09E .03 | -0.2 | -0.6 | -0.8 | 0.2 | 0.0 |
| 6.79E .07 | -1.35E .06 | 0.86E .03 | -0.6 | -0.4 | -0.9 | 0.3 |
| -5.66E .04 | -1.86E .03 | -1.15E .04 | 2.00E .00 | 1.0 | 0.6 | -0.3 |
| -7.98E .05 | -3.25E .04 | -1.04E .05 | 9.34E .01 | 3.65E .01 | 0.4 | -0.2 |
| -1.16E .05 | 2.31E .03 | -8.04E .04 | 2.09E .01 | 1.74E .02 | 1.27E .01 | -0.4 |
| 8.72E .03 | 3.43E .01 | 4.13E .03 | -1.40E .00 | -1.36E .01 | -8.86E .00 | 1.78E .00 |

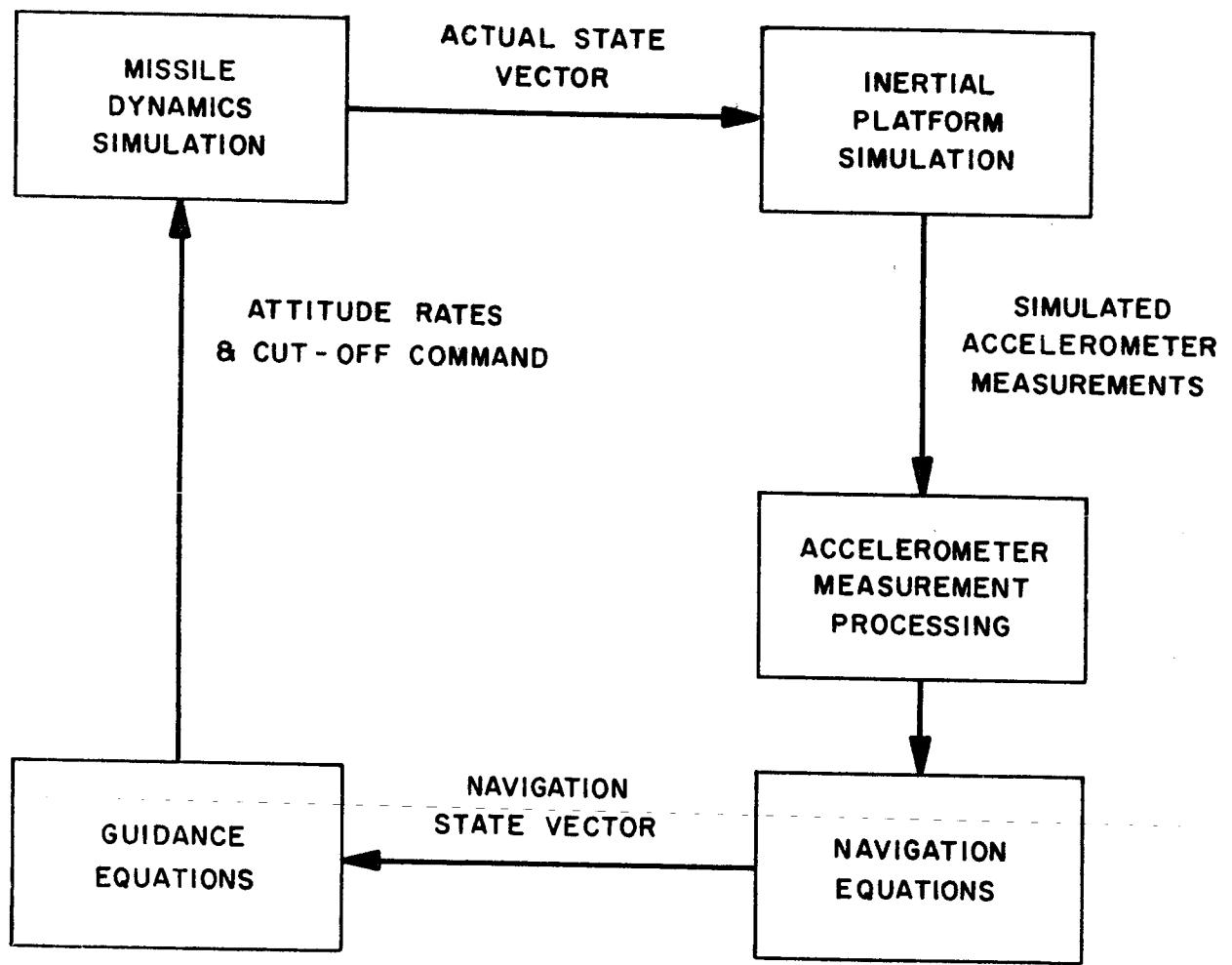


FIGURE 1
CLOSED LOOP SIMULATION

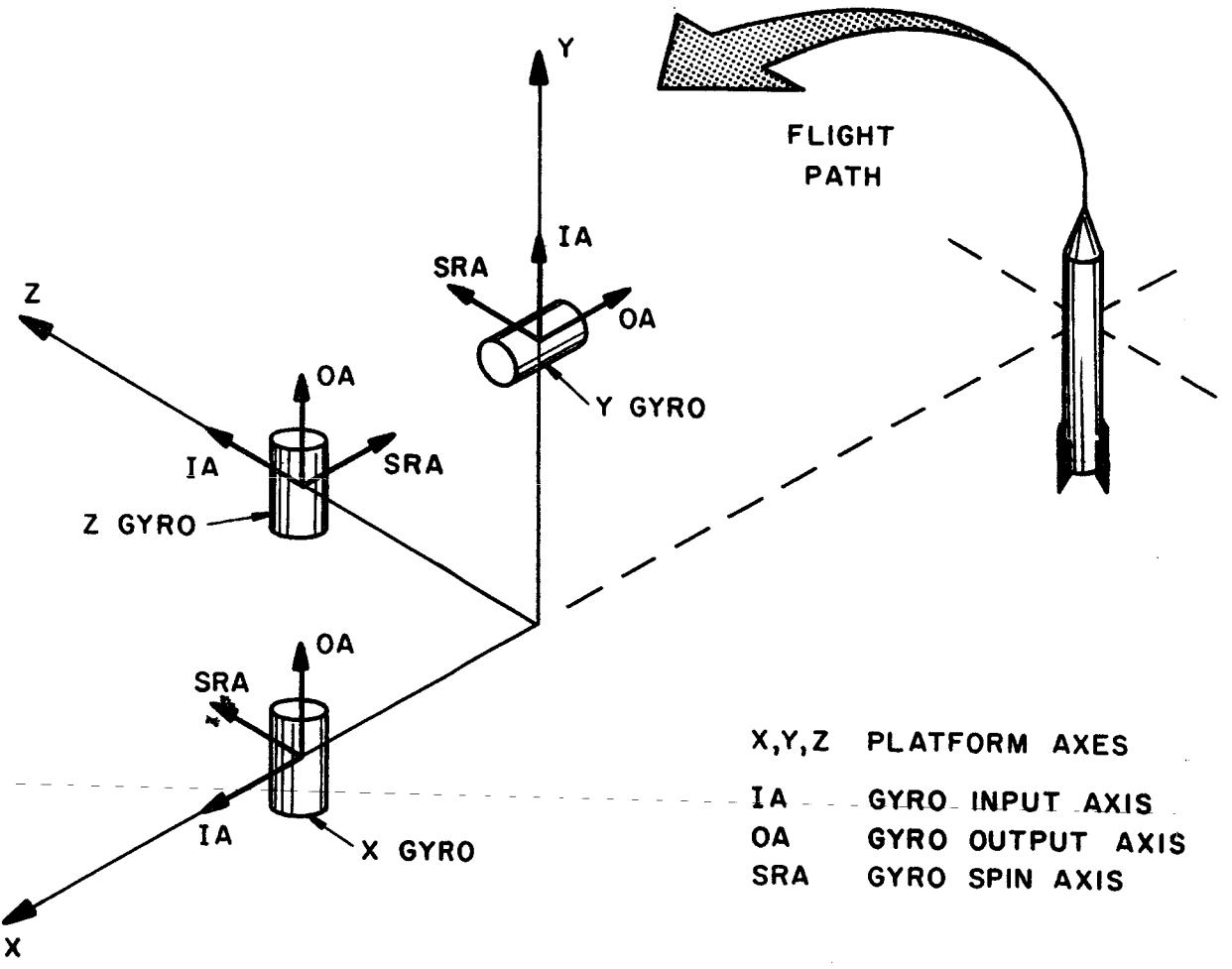


FIGURE 2
PLATFORM CONFIGURATION

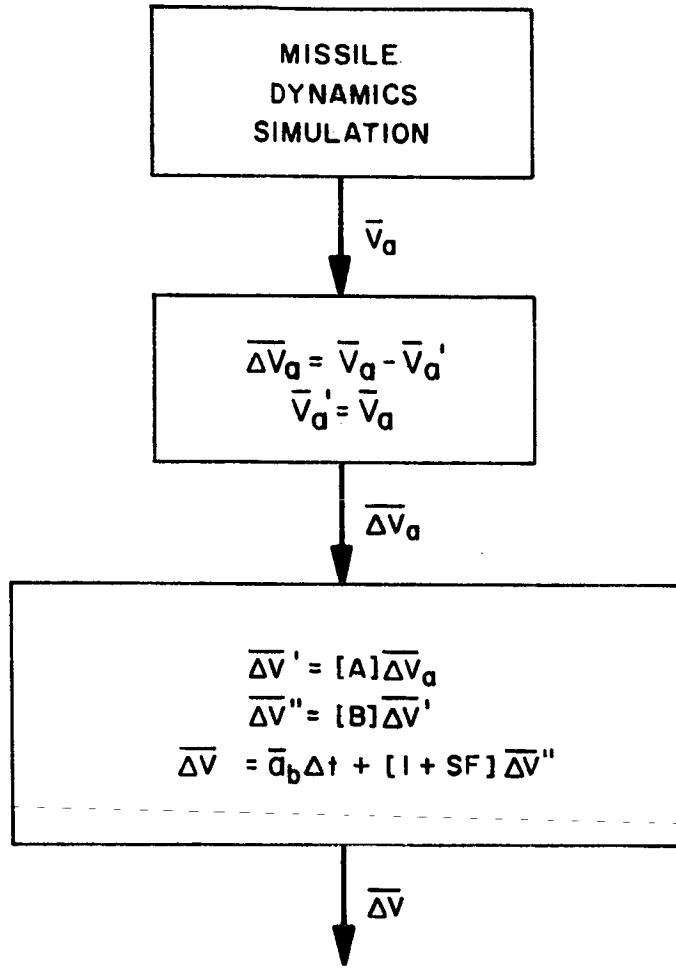


FIGURE 3
INERTIAL PLATFORM SIMULATION

ACCELEROMETER MISALIGNMENT

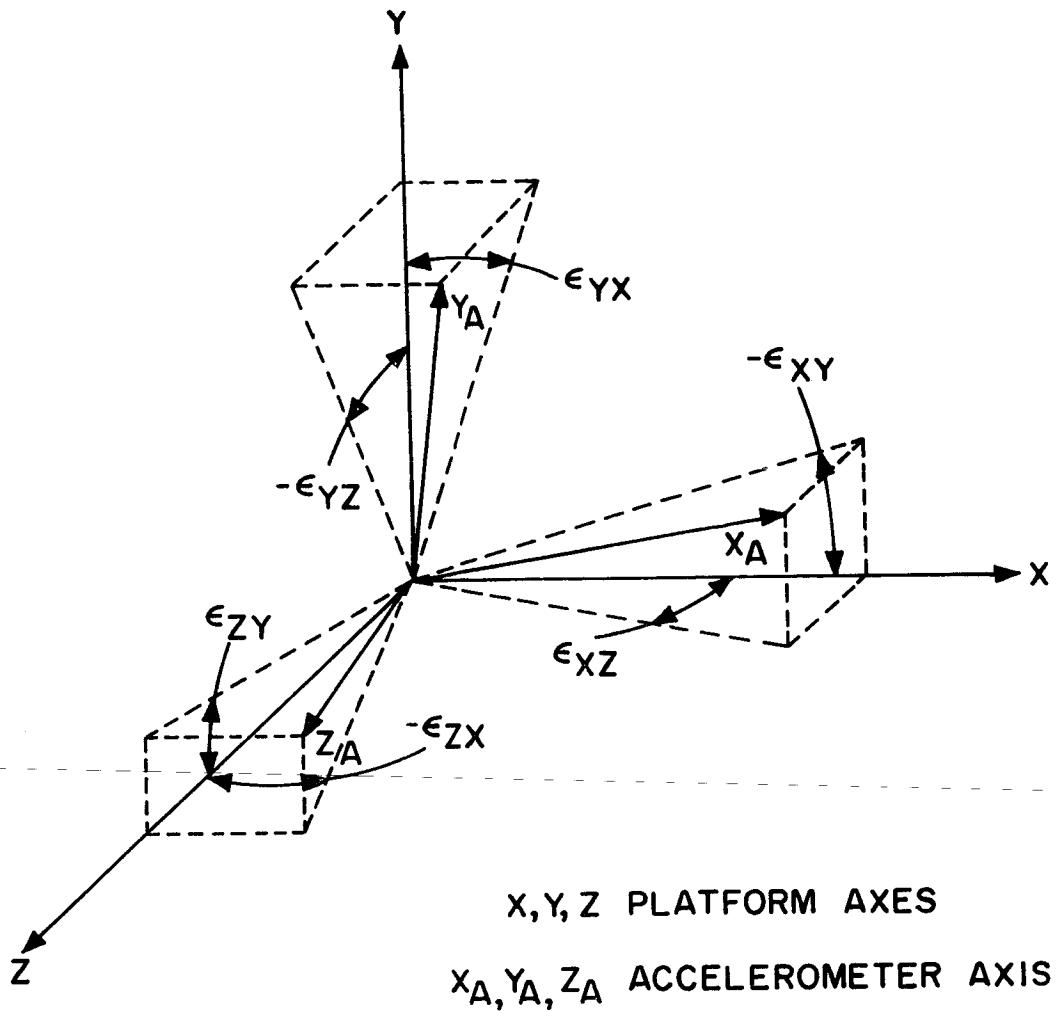


FIGURE 4

FUEL DIFFERENCE AT PARKING ORBIT INSERTION
VS DEVIATION IN S-IC MIXTURE RATIO

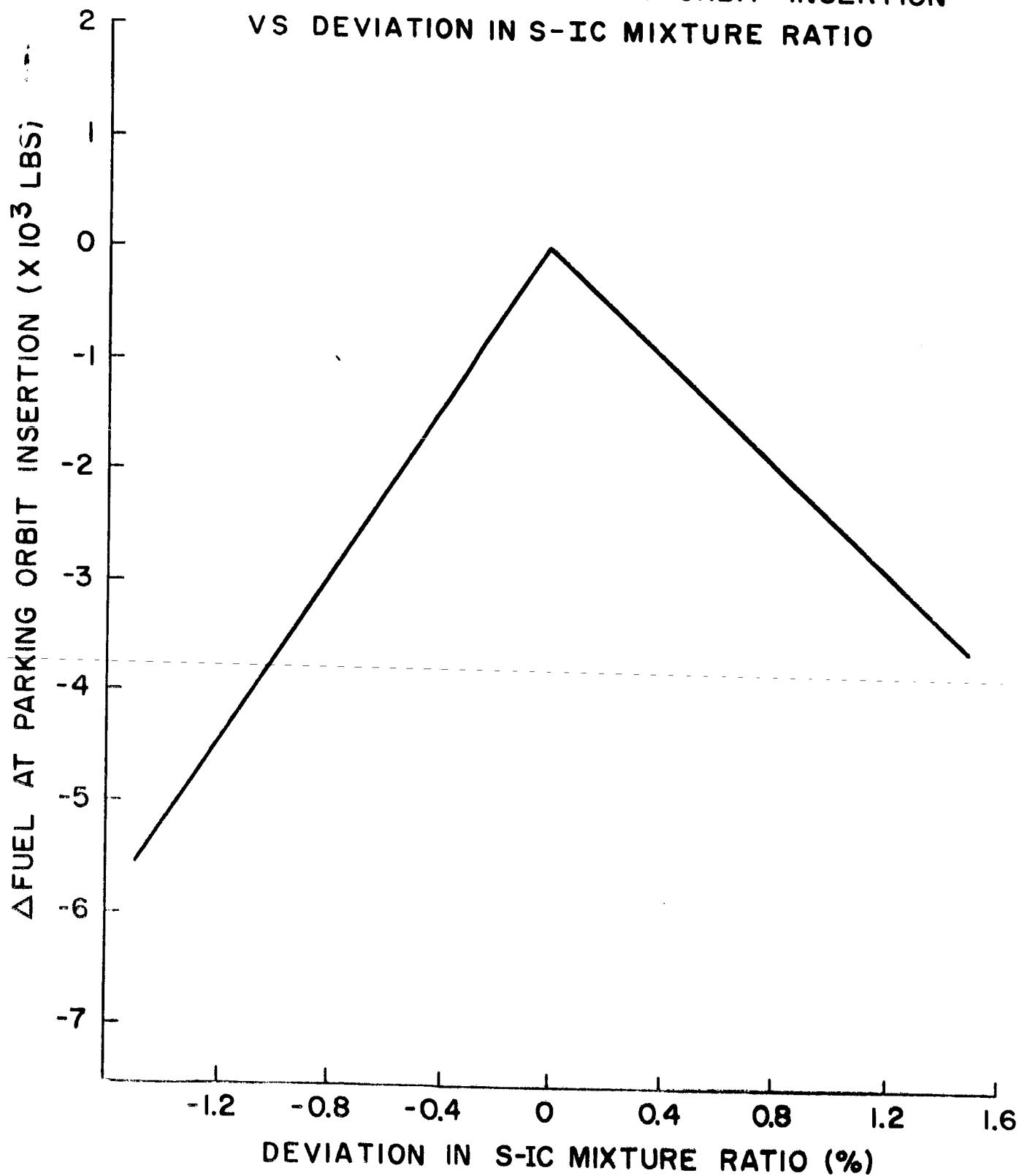


FIGURE 5

FUEL DIFFERENCE AT PARKING ORBIT INSERTION
VS DEVIATION IN S-II MIXTURE RATIO

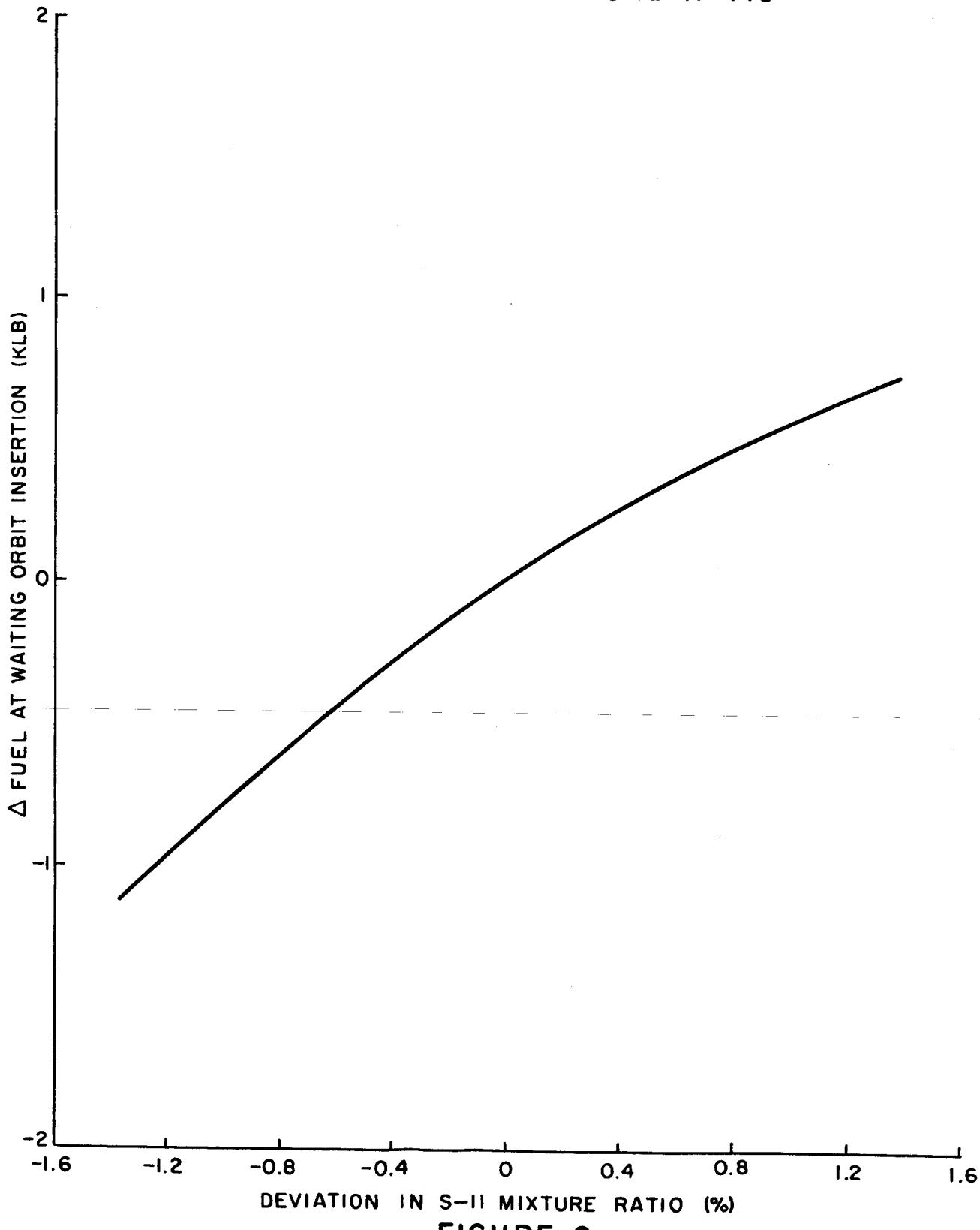


FIGURE 6

FUEL DIFFERENCE AT WAITING ORBIT INSERTION
VS DEVIATION IN S-IVB MIXTURE RATIO

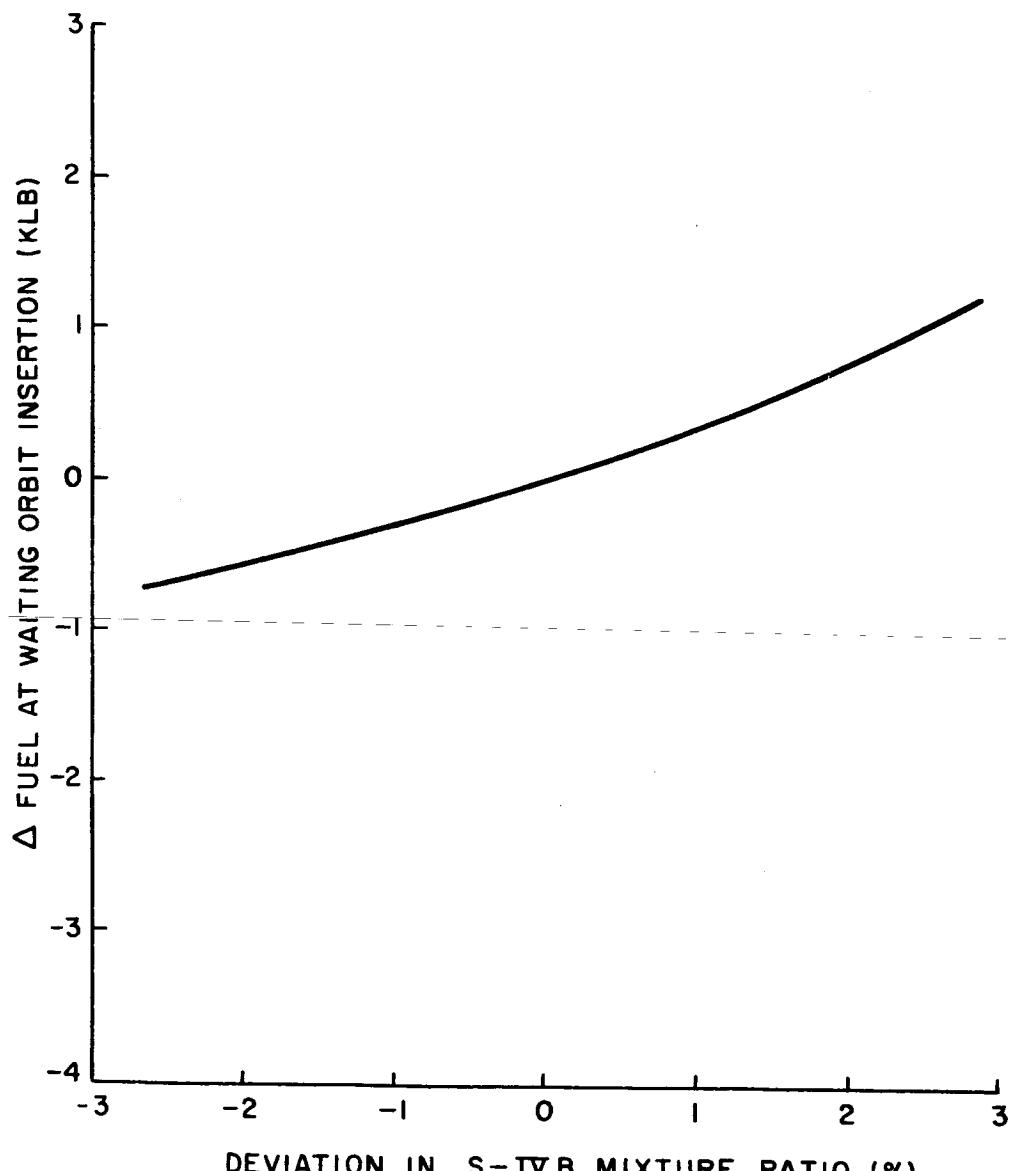


FIGURE 7

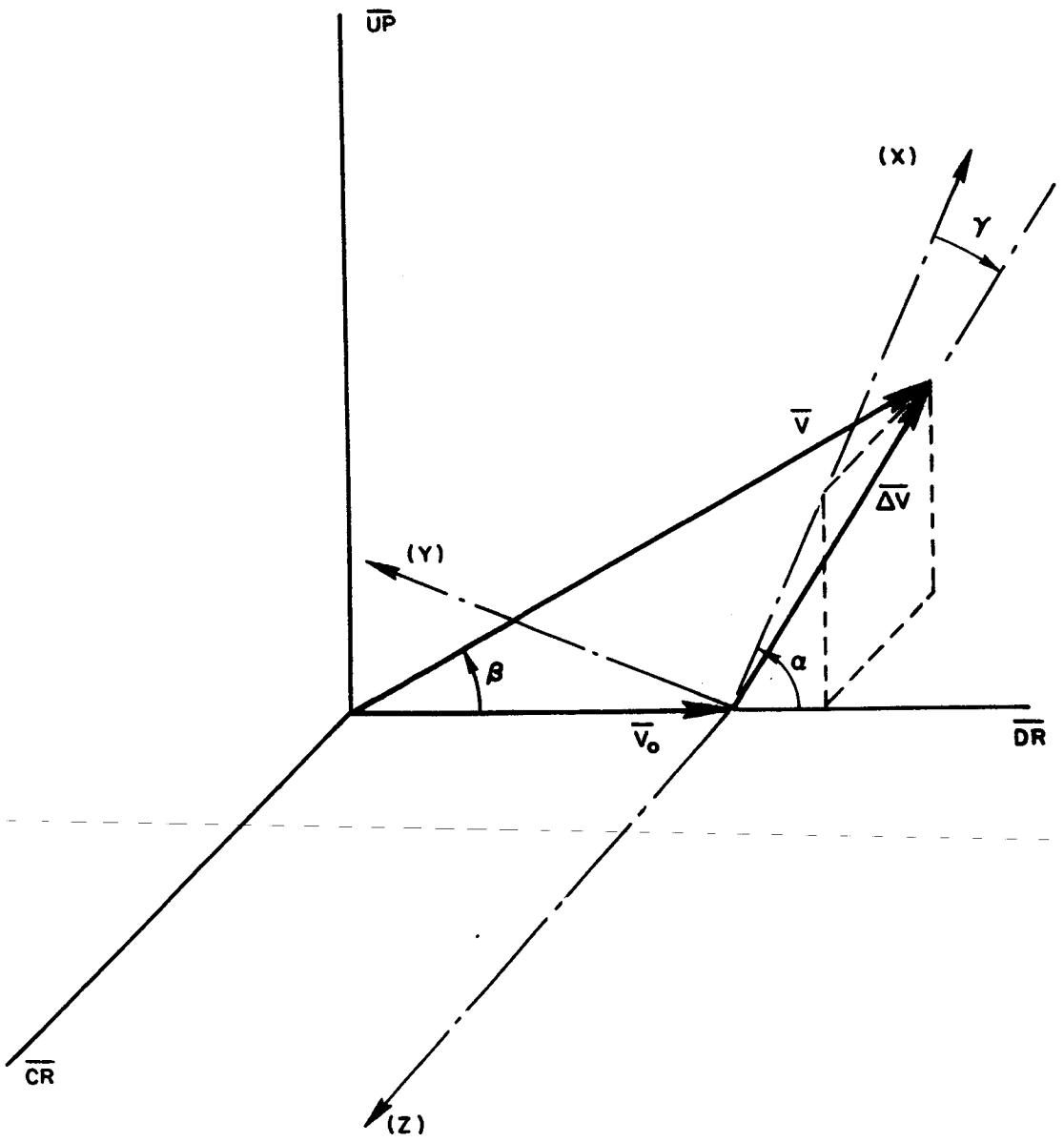


FIGURE 8
MODEL FOR WAITING ORBIT
INJECTION BURN

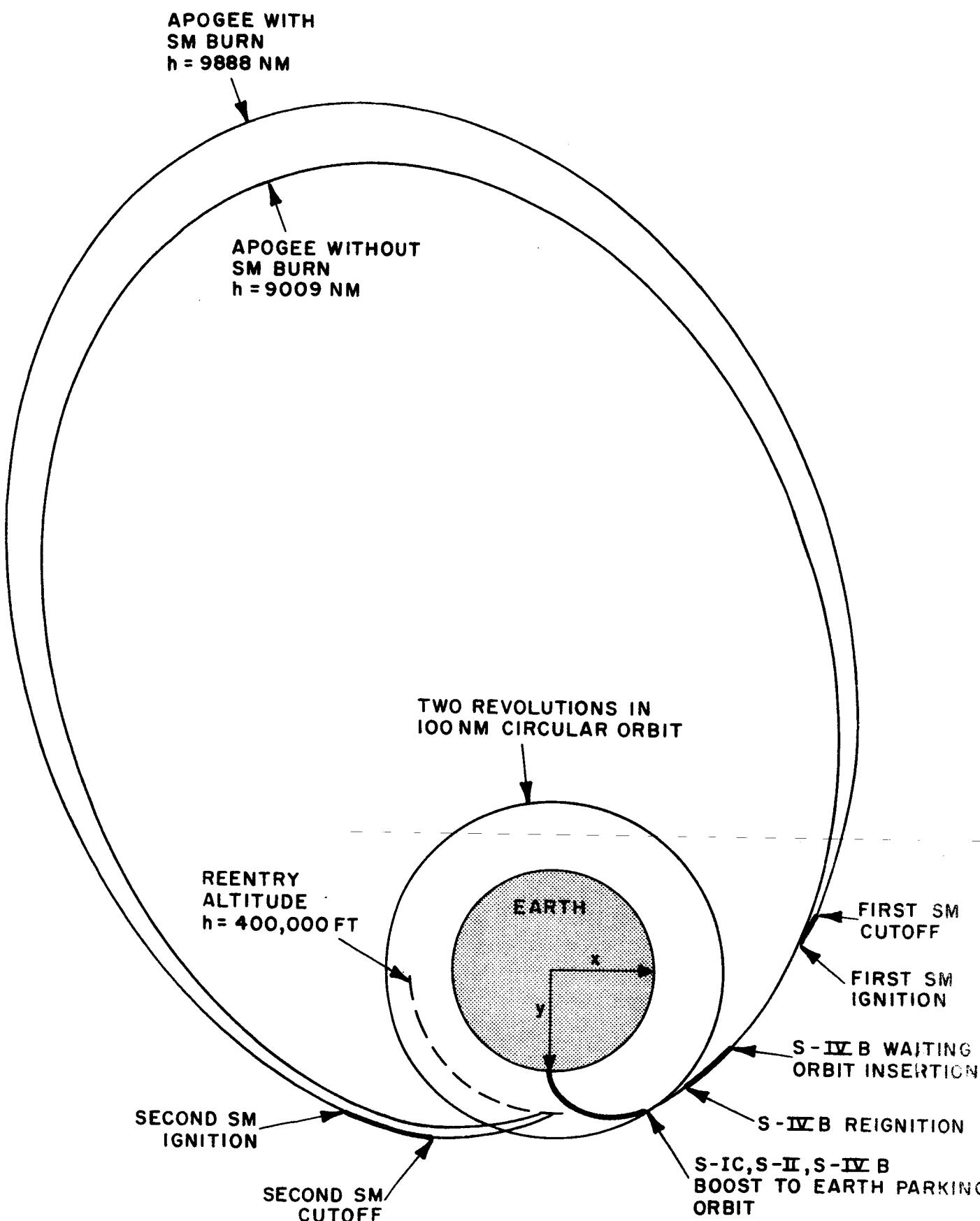


FIGURE 9
APOLLO - SATURN 501 MISSION PROFILE